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STATIC STABILITY AND AXIAL FORCE COEFFICIENTS FOR THE 0.125 SCALE MODEL MARK 82 LOW DRAG BOMB WITH CLOSED SNAKEYE I FINS AT SUBSONIC AND TRANSONIC SPEEDS

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STATIC STABILITY AND AXIAL FORCE COEFFICIENTS
FOR THE 0.125 SCALE MODEL MARK 82 LOW DRAG BOMB
WITH CLOSED SNAKEYE I FINS AT SUBSONIC AND TRANSONIC SPEEDS

Prepared by: V. L. Schermerhorn

ABSTRACT: Static stability and axial force coefficients are presented as a function of angle of attack for the Mk 82 Low Drag Bomb with Snakeye Fins in the closed position. These data were obtained for a Mach number range from 0.6 to 1.1; an angle-of-attack range from -6 to +20 degrees; and, a roll-angle range from 0 to 225 degrees in the NOL Supersonic Tunnel No. 1, using a subsonic nozzle.

U. S. NAVAL ORDNANCE LABORATORY WHITE OAK, MARYLAND

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The purpose of the test was to furnish static stability and drag data. These tests were conducted at the request of NWL under task number NOL-795/NWL.

GEORGE G. BALL Captain, USN Commander

L. H. SCHINDEL

By direction

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INTRODUCTION

This report gives the results of static wind-tunnel tests on the Navy Mk 82 Low Drag Bomb using the Snakeye I Fins, in the unretarded mode (closed position) as stabilizers.

LIST OF SYMBOLS

A	reference area, 7 d2/4
CA	axial force coefficient, FA/qA
CA _O	axial force coefficient at zero angle of attack
CAf	axial force coefficient, with base drag removed
CŁ	rolling moment coefficient, M _X /qAd
C _m	pitching moment coefficient, My/qAd
C _{m/Y}	static stability index
CN	normal force coefficient, FN/qA
$c_{n_{\sigma}}$	normal force coefficient derivative
c_n	yawing moment coefficient, Mz/qAd
C _y	side force coefficient, Fy/qA
c.g.	moment reference center (6.025 inches from model base)
d	maximum body diameter
$\mathbf{F}_{\mathbf{A}}$	axial force
F _N	normal force
Fy	side force
M	Mach number
$M_{\mathbf{X}}$	rolling moment
My	pitching moment

¥z	yawing moment
Pip	base pressure
$P_{\mathbf{S}}$	free-stream static pressure
P_0	stagnation pressure
q	dynamic pressure, $\rho^{V^2/2}$
Re	Reynolds' number/ft
V	free-stream velocity
x,y,z	body axes
α	angle of attack
8	fin opening angle
ρ	free-stream density
•	roll angle

MODEL, DATA ACQUISITION AND DATA REDUCTION

Mode 1

A 0.125-scale model of the Mk 82 Bomb with Snakeye I fins in the closed position (unretarded mode) was tested; a sketch of the model configuration is shown on Figure 1. The scaled model was 11.180 inches long and had a maximum body diameter of 1.347 inches. To accommodate the sting balance, half of the inner shaft and 1.30 inches of the tail fin length, at the rear of the model, between the panel stiffeners, was removed. A sketch of the full-scale bomb is presented on Figure 2, for comparison purposes.

Balance

The NOL 6-14 balance, an internal strain-gage axial balance, was used to obtain the experimental data, which was collected and stored in digital form on magnetic tape.

Test Conditions

The model was tested at an angle-of-attack range from -6 to +20 degrees; for roll angles of 0, 1.33 (a case where the model moved), 6, 12, 18, 22.5, 45, 90, 180, 186, 202.5 and 225 degrees; and at Mach numbers ranging from 0.6 to 1.1. These tests were conducted in the NOL Supersonic Tunnel Number 1, using the subsonic nozzle. Observations of the flow field, made while the test was being conducted, indicated that a shock reflection on the tail of the model occurred at M = 1.1. As a consequence of this condition, no further tests at this Mach number were conducted. For the remainder of the test program, a free-stream Mach Number of 1.05 was selected as an upper limit value.

Data Reduction

The experimental data were reduced to aerodynamic coefficients, using a center-of-gravity position 6.025 inches ahead of the fin base as a moment reference center. Figures 3 to 166 are plots of the various coefficients as a function of angle of attack. For these figures, the angle of attack has been corrected for elastic deflection of the sting balance due to aerodynamic loading. Since an internal strain-gage balance was used here, no correction has been applied to the data for base pressure even though the base pressure was measured and is included here on Figure 167, as a function of Mach number and for zero angle of attack.

Correction to the axial force coefficient, for base pressure, could be made by means of the following expression:

$$C_{Af} = C_A + A_b (P_b - P_s)/qA$$
,

wherein $A_b = 0.3207$ in.² (inner shaft area). This expression would yield a maximum change in axial force coefficient, $C_{A_f} = C_A = 0.015$ since the difference $(P_b = P_s)$ is very small (see Fig. 167).

As a definition of roll-angle orientation it has been assumed that when the juncture of two fin panels was in the vertical plane, the roll was zero. During this investigation, tests were conducted at roll angles of 0, 6, 12, 18, 22.5, and 45 degrees to see if any significant (induced) rolling moment would be imparted to the model by the fin-panel stiffeners. Tests also were conducted at roll angles of 90, 180, 186, 202.5 and 225 degrees to determine the effect on the coefficients due to the fin misalinement.

Table 1 is a listing of the average tunnel conditions which were used in the data reduction program. It should be understood that these conditions vary to some small degree since they are dependent upon the barometric pressure and temperature of the day. For reference purposes, the actual Mach number associated with each individual run is listed on the appropriate data figure.

RESULTS

Normal force and pitching moment coefficients, as functions of angle of attack, are presented on Figures 3 through 84. Side force, yawing moment, rolling moment and axial force coefficients are similarly presented on Figures 85 through 166. For an angle of attack near 15 degrees, and at a Mach number of 0.75 and greater, the fins were noted to vibrate. This action is reflected in all of the data, but is most visible in the pitching moment results obtained for this region of the tests (see Fig. 4). When vibration occurs, the fins would hit the balance (Fig. 4 at 16 degrees). For the remainder of the figures (Fig. 5 to 166), data is only presented up to the point where vibration starts. As a high balance sensitivity was needed to measure the small axial force loads, the balance was sensitive to tunnel and model vibrations. This accounts for the scatter seen in the axial force data (Figs. 84 to 166)

The static margin, in calibers, $C_{m_{\gamma'}}/C_{N_{\gamma'}}$, obtained at zero $\pm 1^{\circ}$ and $7^{\circ}\pm 1^{\circ}$ degrees angle of attack, and plotted as a function of Mach number, is given on Figure 168. The axial force at zero angle of attack versus Mach number is shown on Figure 169.

CONCLUSIONS

The bomb has essentially neutral static stability in the angle-of-attack range from -4 to +4 degrees. An increase in stability in the region of -4 to +4 degrees angle of attack could probably be obtained by increasing the fin span. No significant induced rolling moments, which could be attributed to the fin panel stiffeners, were ascertained. Comparison of the data at 0, 90 and 180 degrees indicates that the trim angle noted in the figures is due to fin misalinement.

Table 1

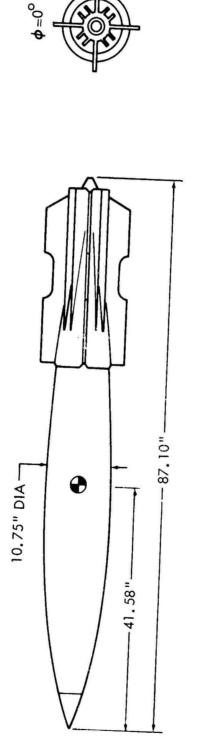
WIND TUNNEL TEST CONDITIONS

Average Supply Temperature = 22 Degrees Centigrade

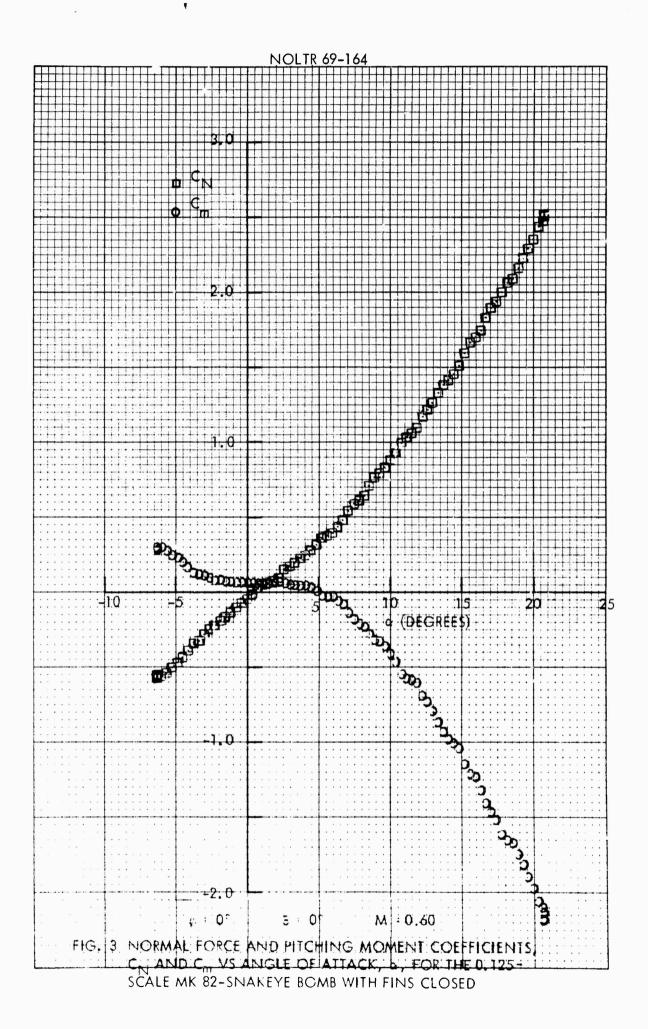
Average Mach Number	Average Supply Pressure P _O mm Hg	Reynolds Number/ft (Re/ft.)x 10 ⁻⁶
0.6	745	3.40
0.7	742	3.80
0.75	741	3.90
0.8	740	4.00
0.85	739	4.15
0.9	738	4.25
0.95	738	4.35
0.99	738	4.40
1.05	737	4.50
1.10	737	4.55

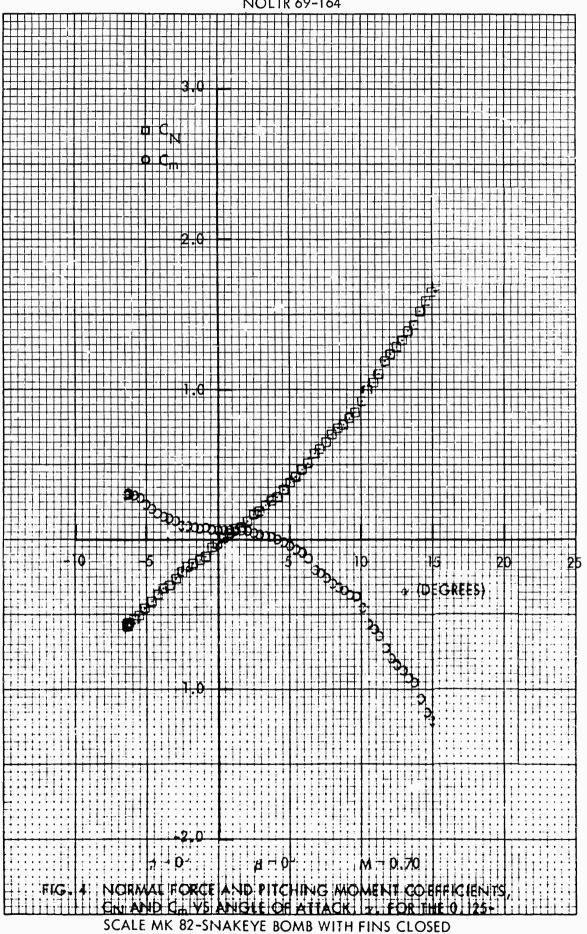


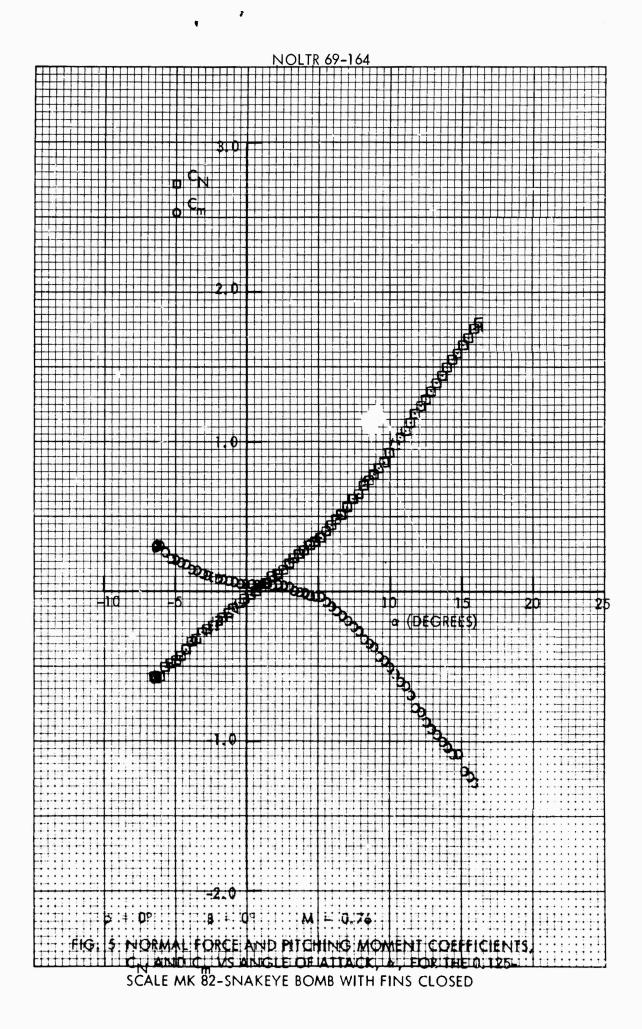
FIG. 1 MK 82 LOW-DRAG BOMB WITH SNAKEYE FINS (0.125 SCALE MODEL WITH FINS CLOSED (UNRETARDED MODE))



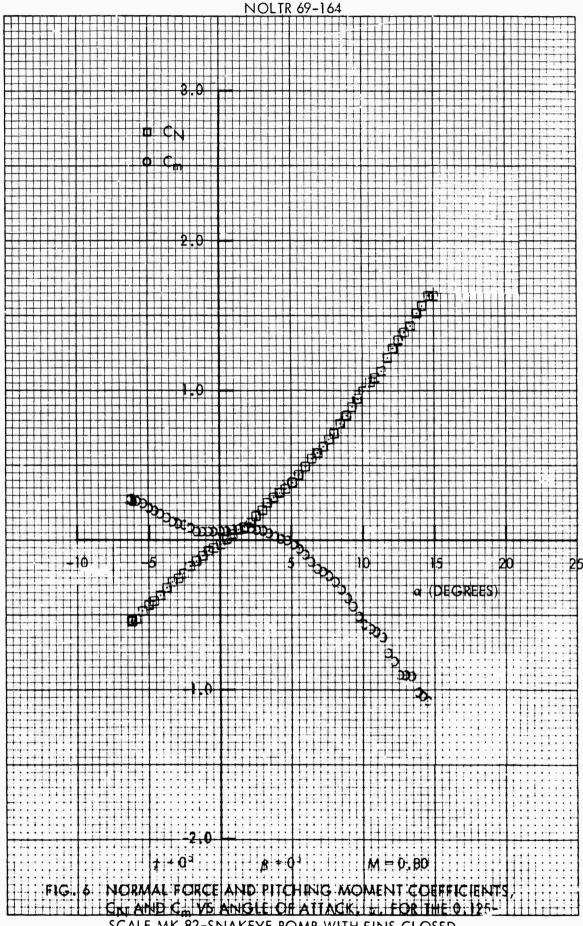
MK 82 LOW DRAG BOMB WITH SNAKEYE I FINS (FULL SCALE WITH FINS CLOSED (UNRETARDED MODE)) FIG. 2



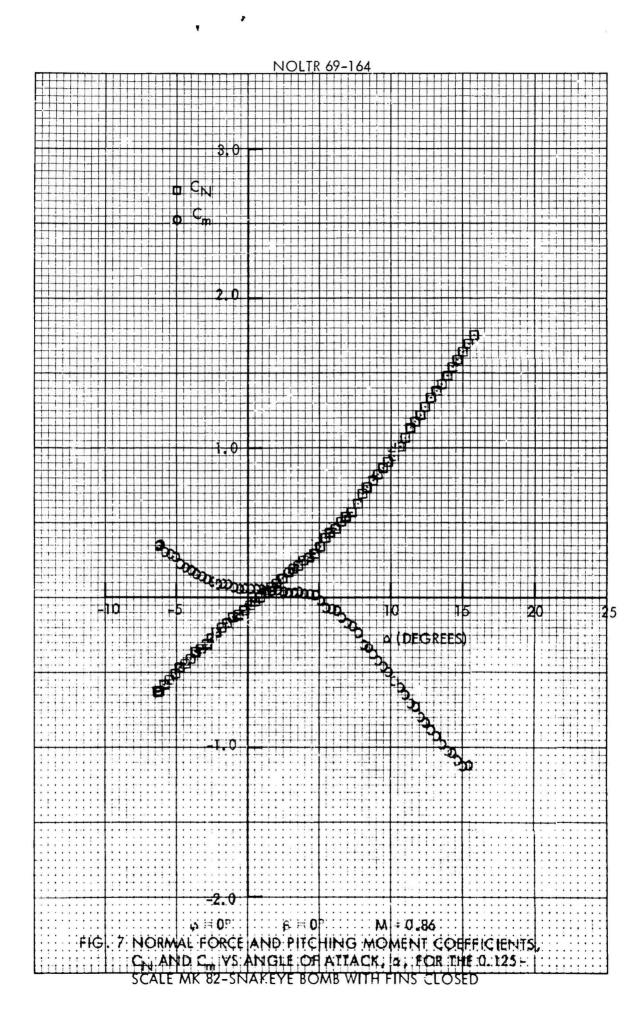


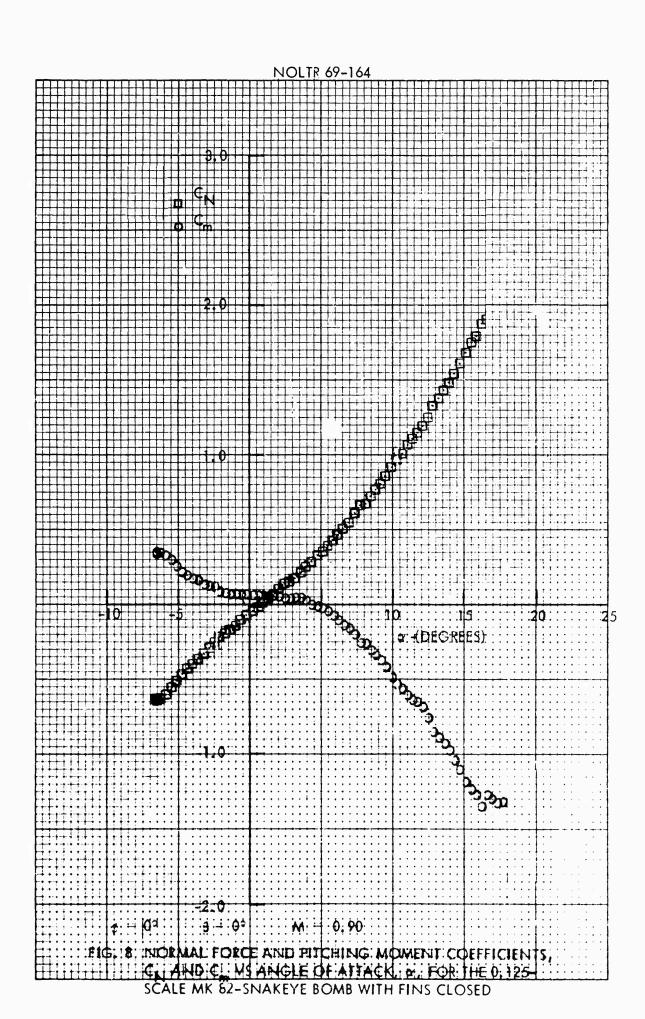


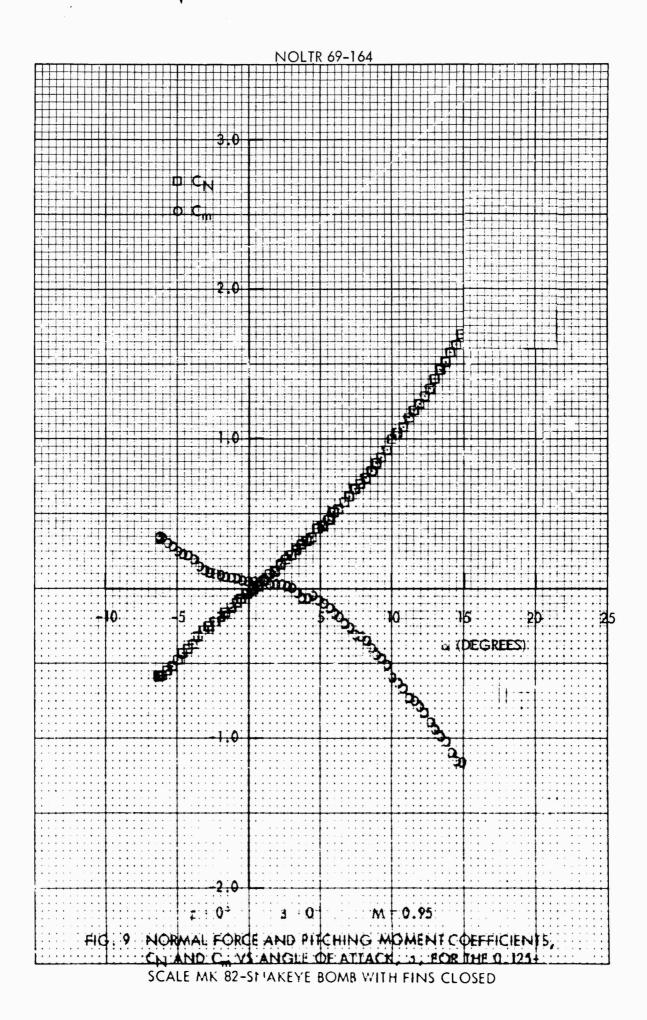


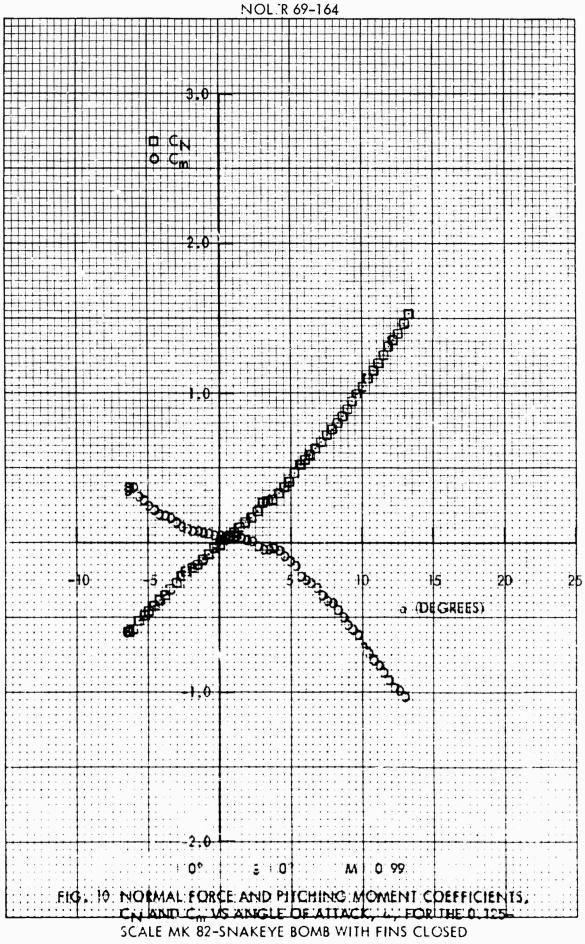


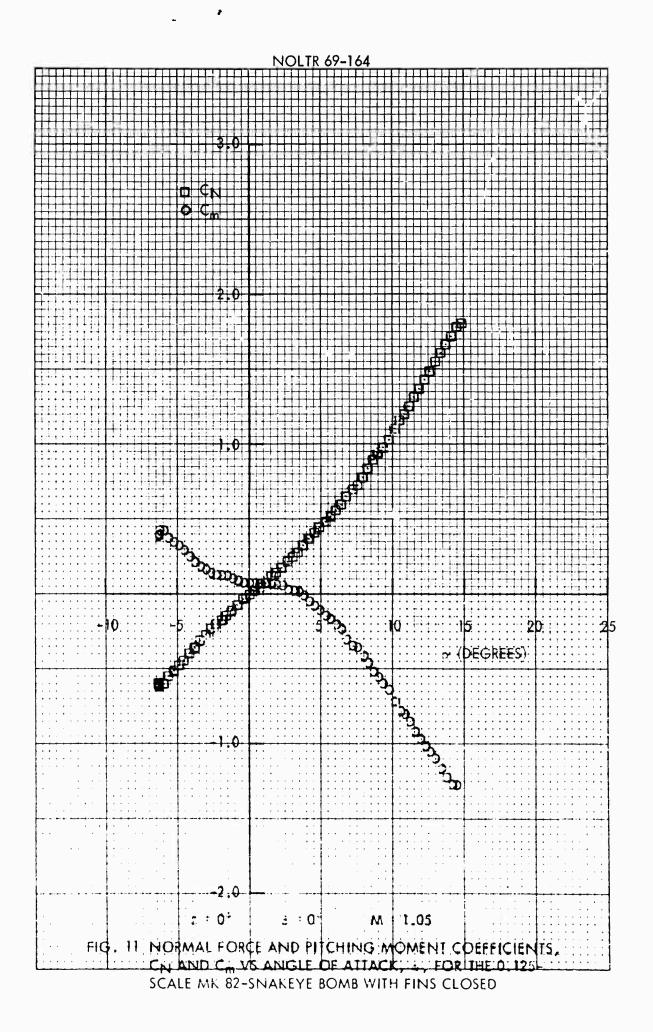
SCALE MK 82-SNAKEYE BOMB WITH FINS CLOSED

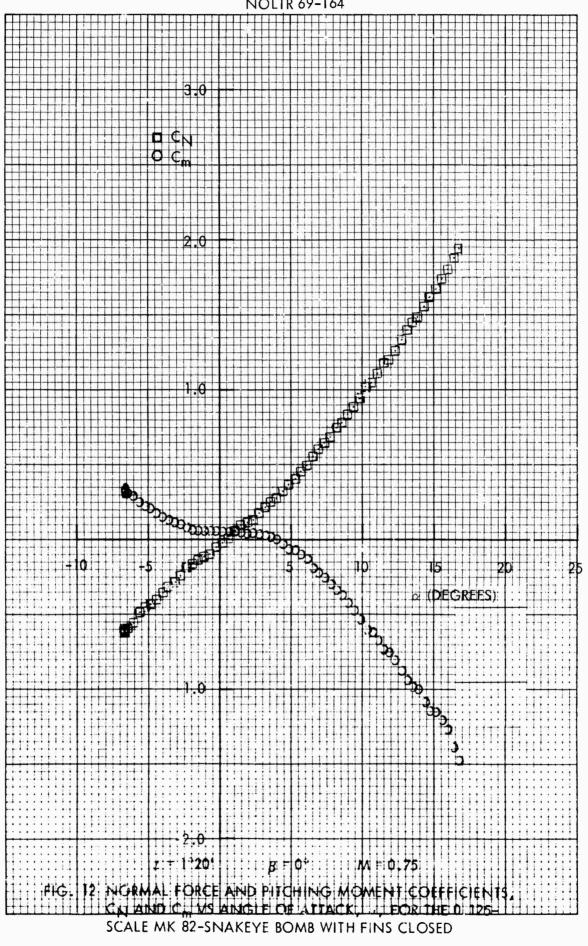




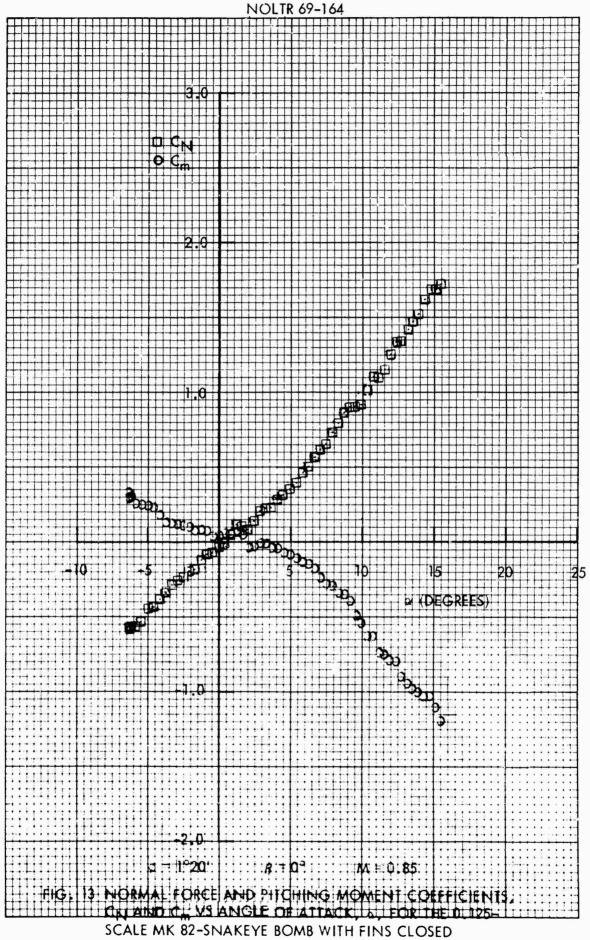


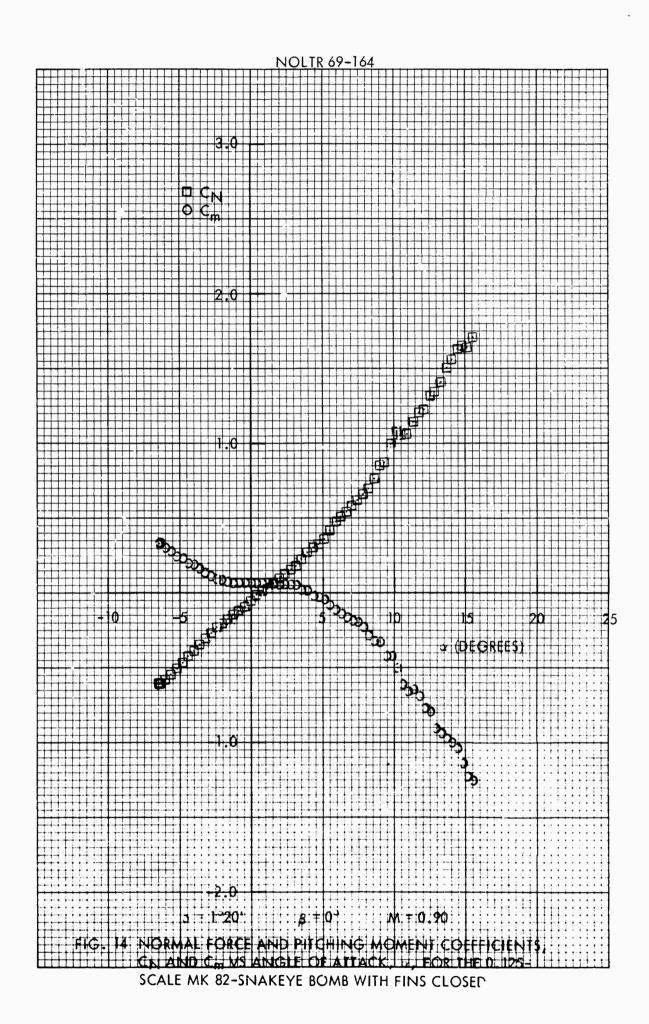


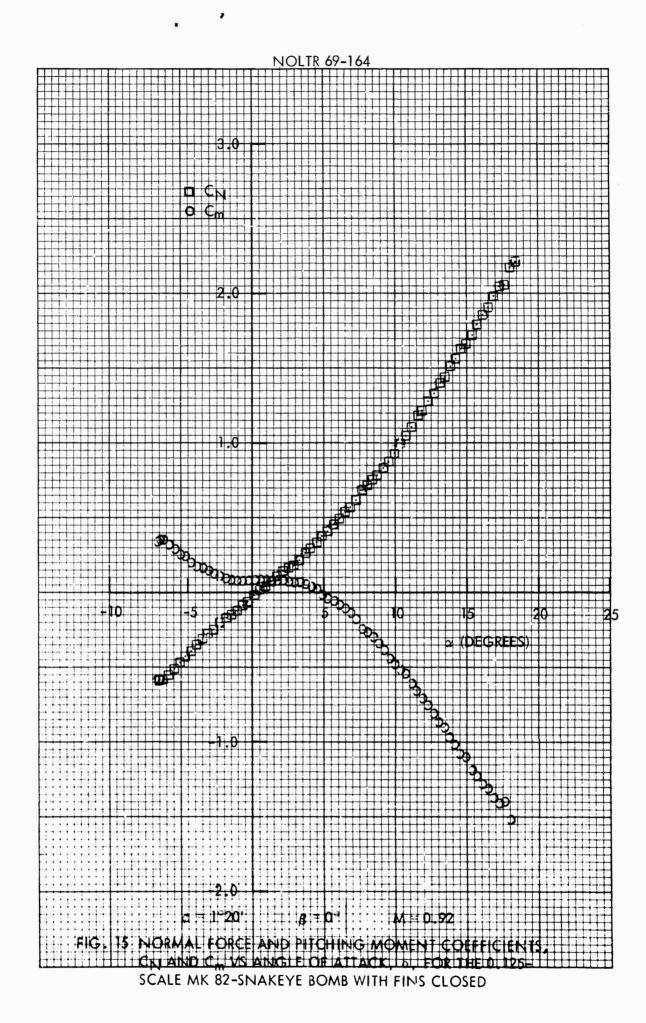


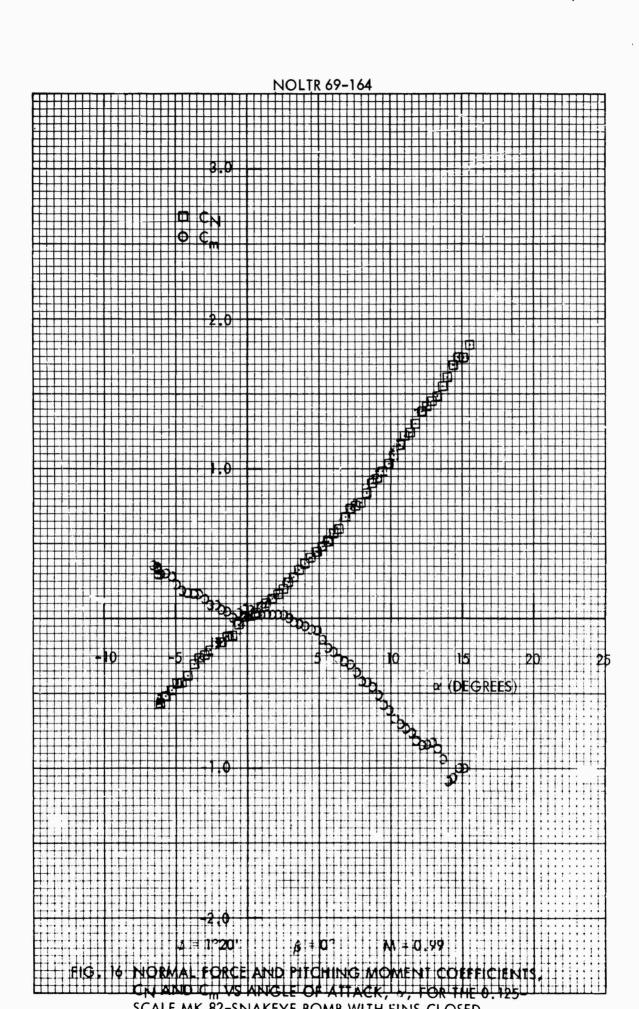




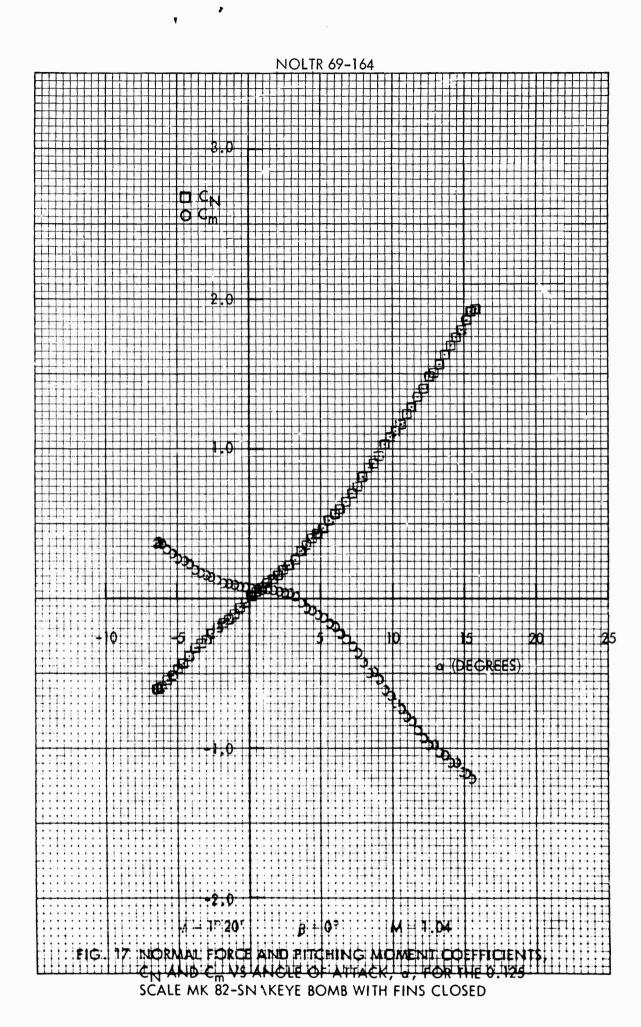


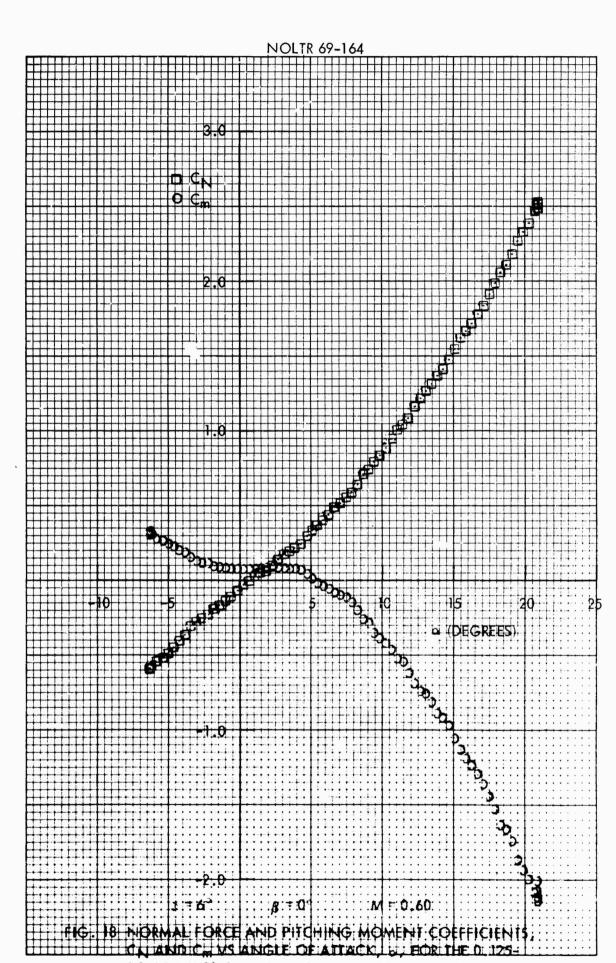




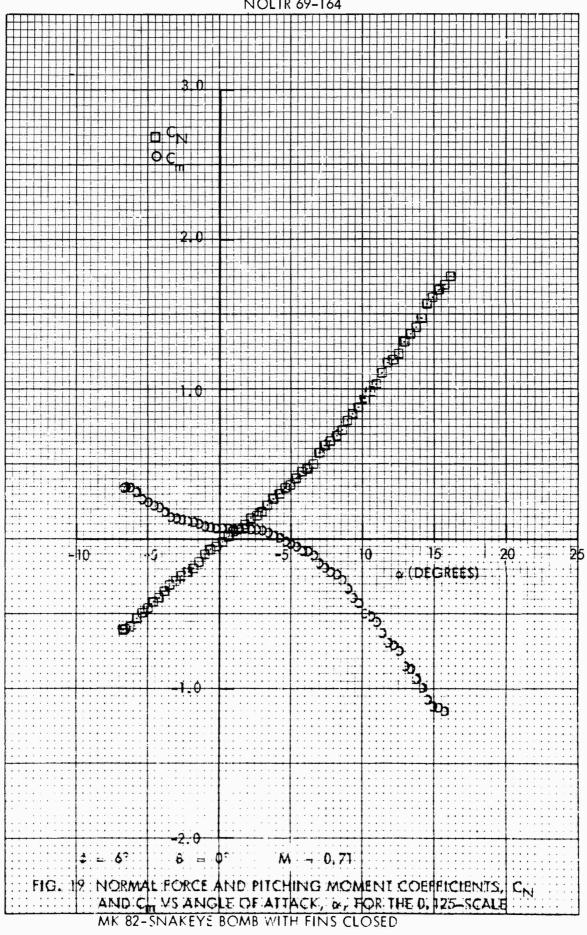


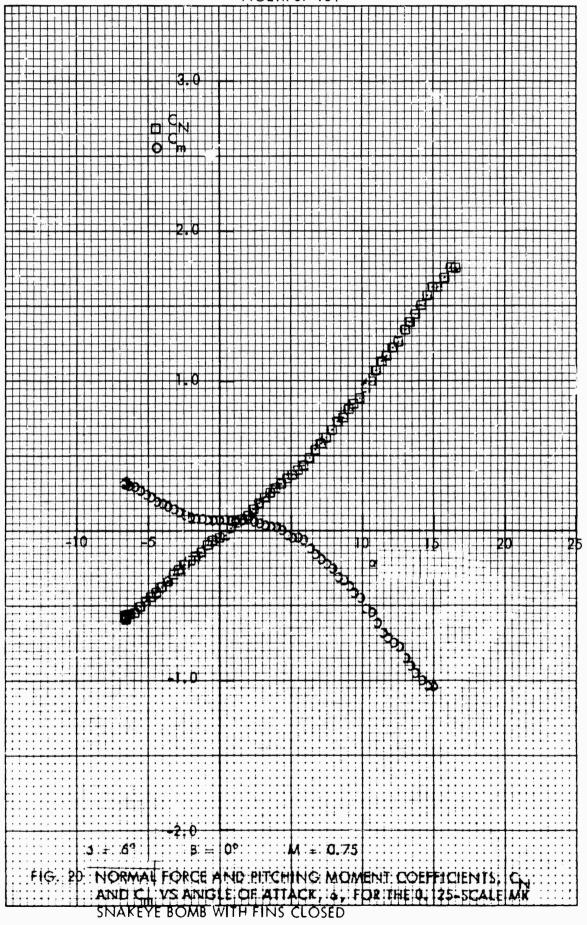
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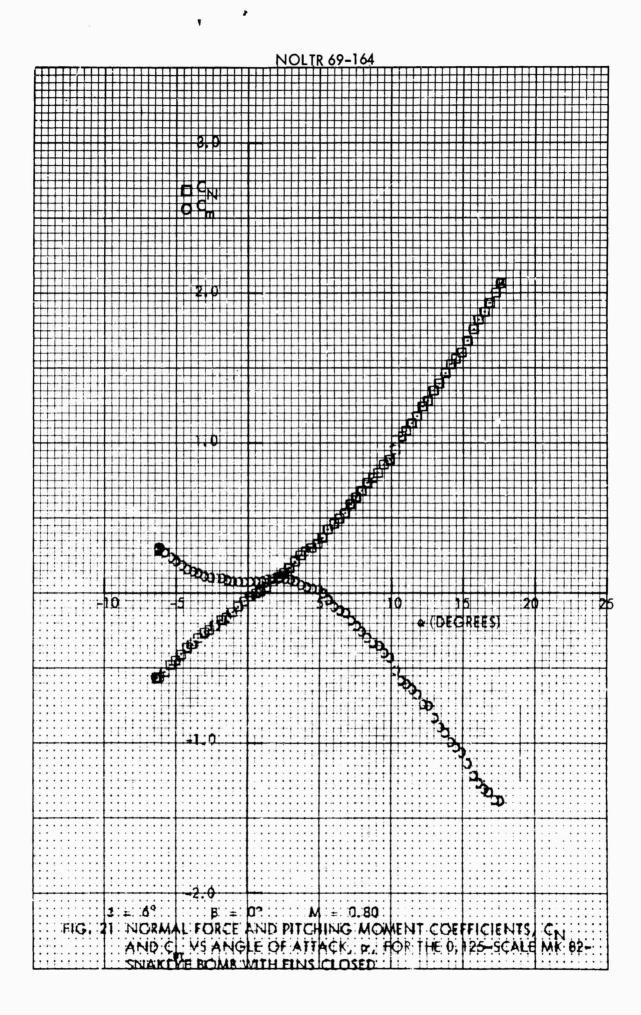


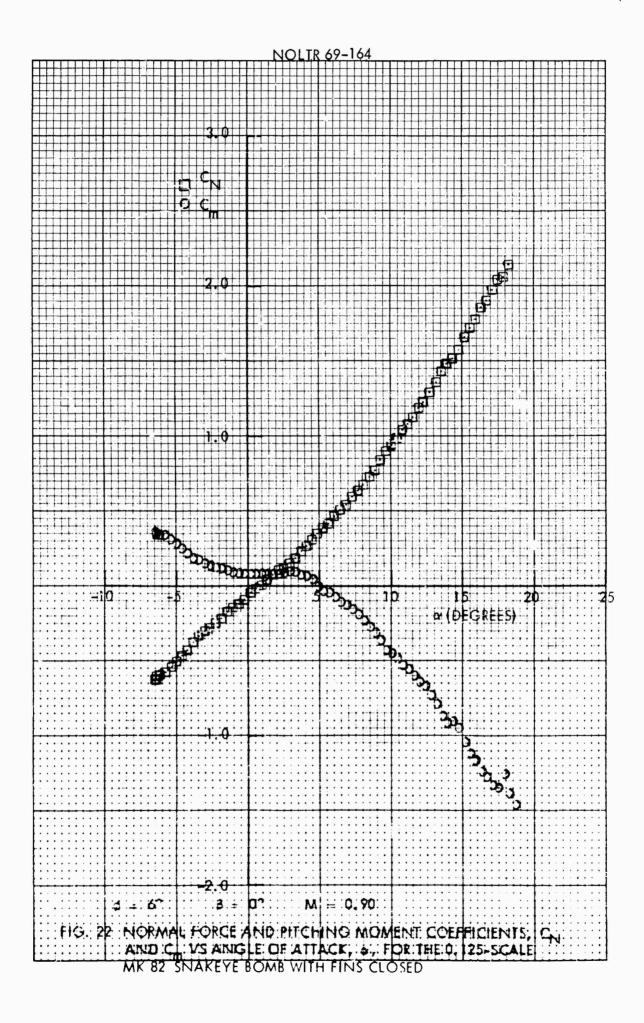


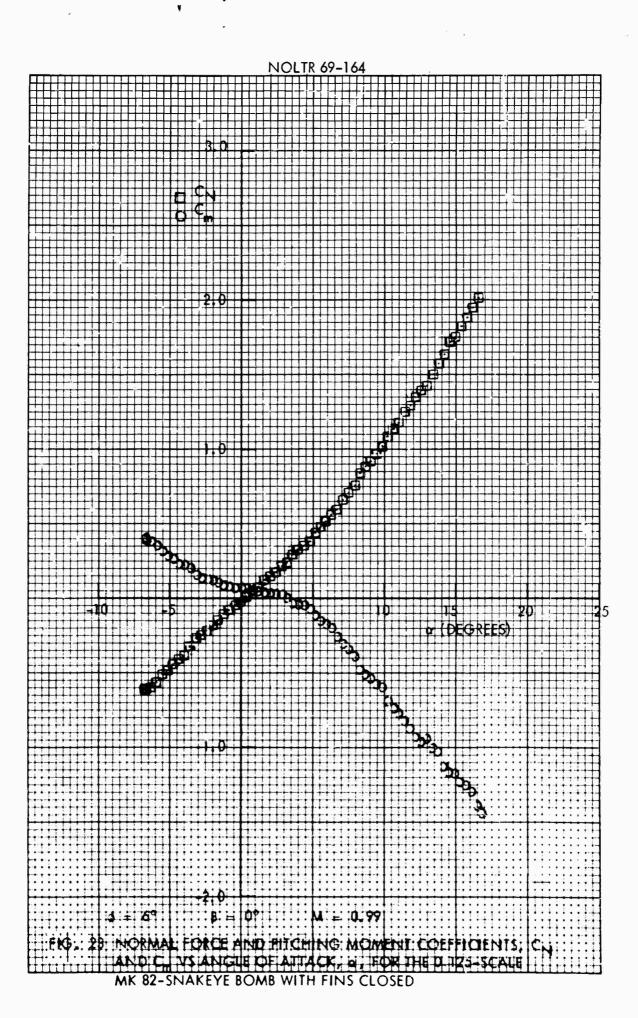
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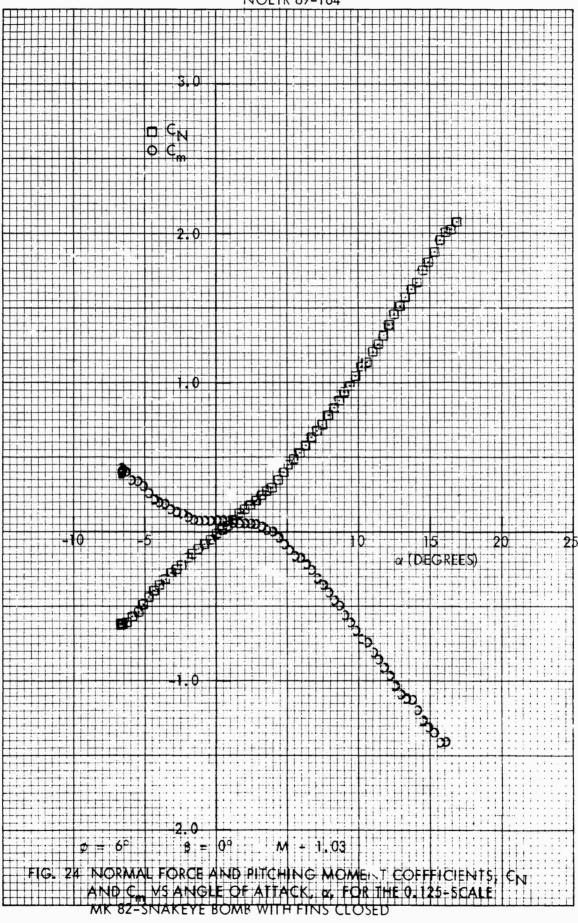


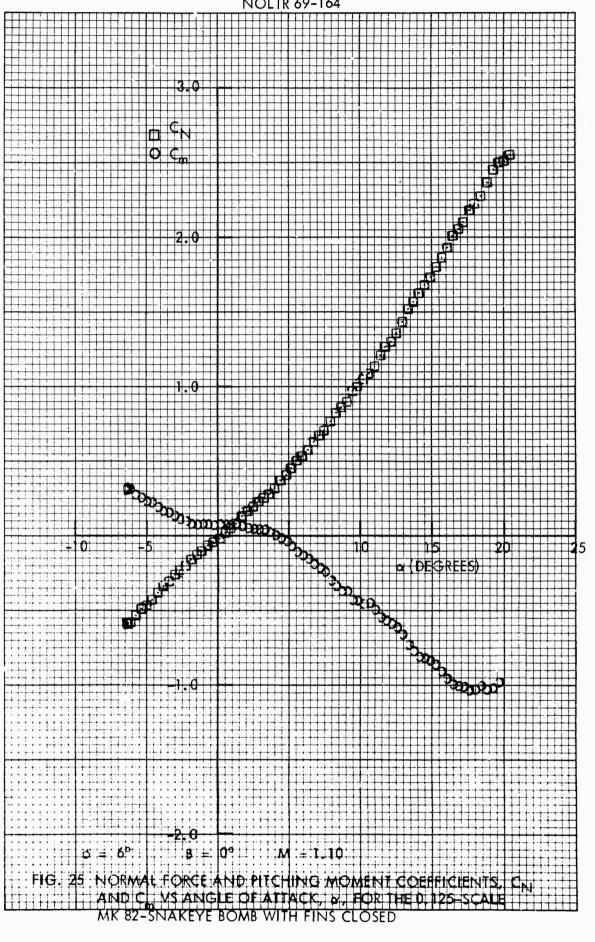


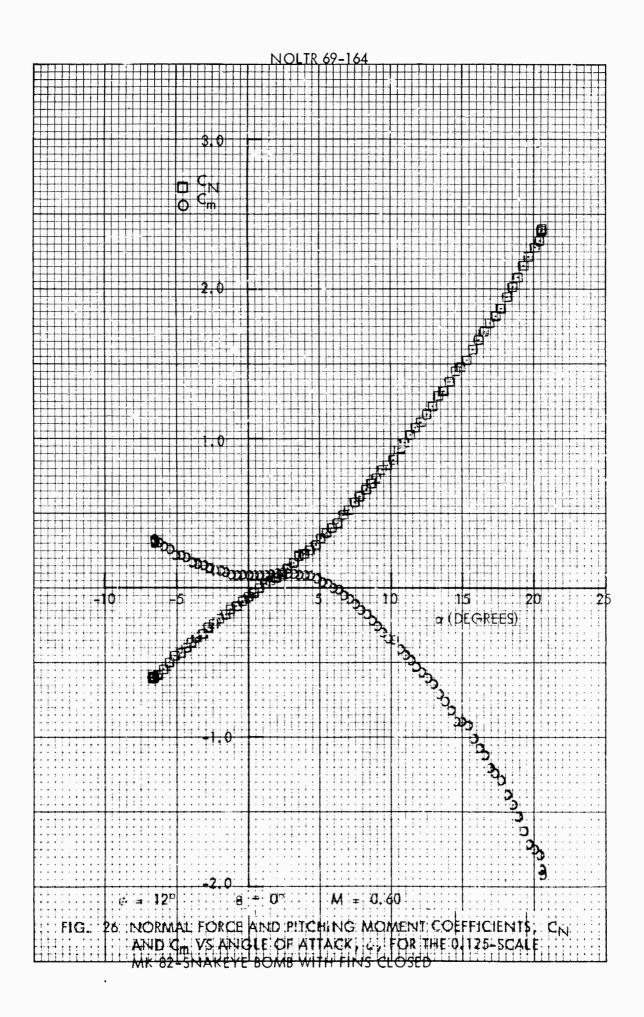


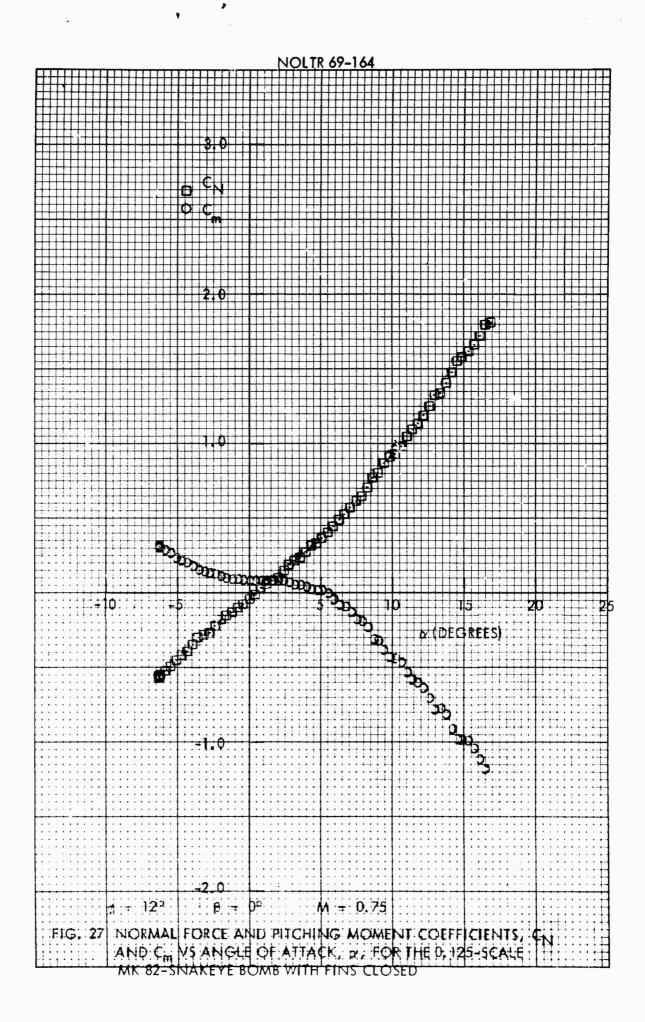


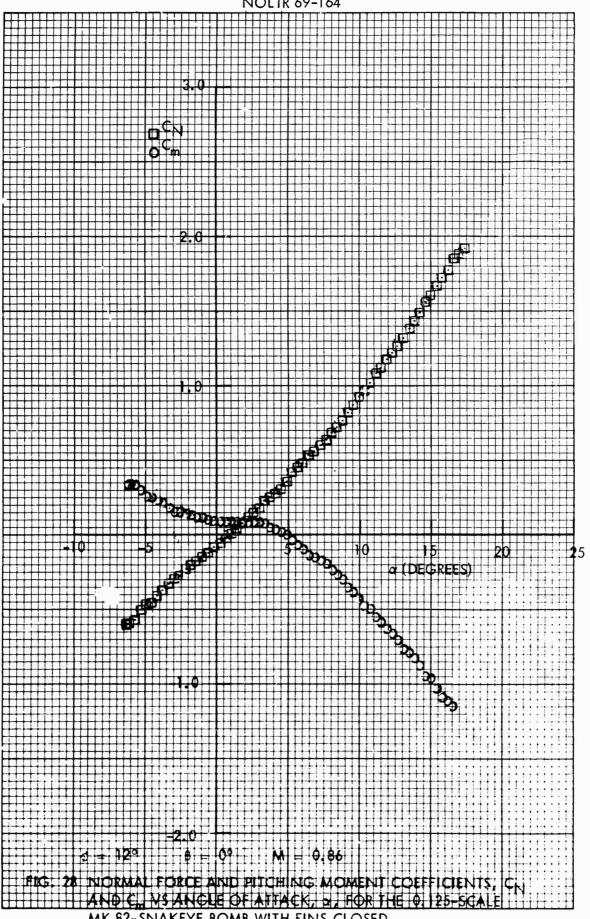




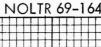


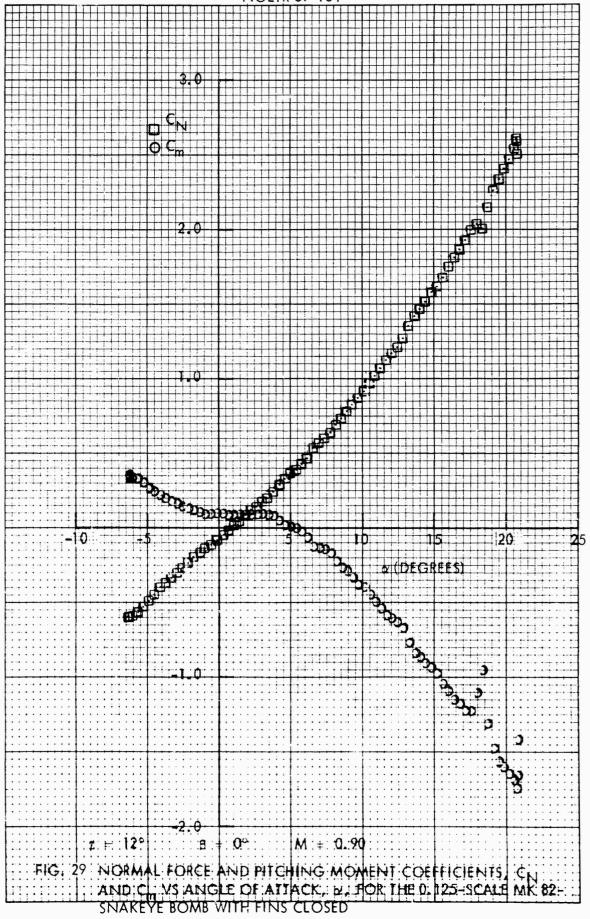


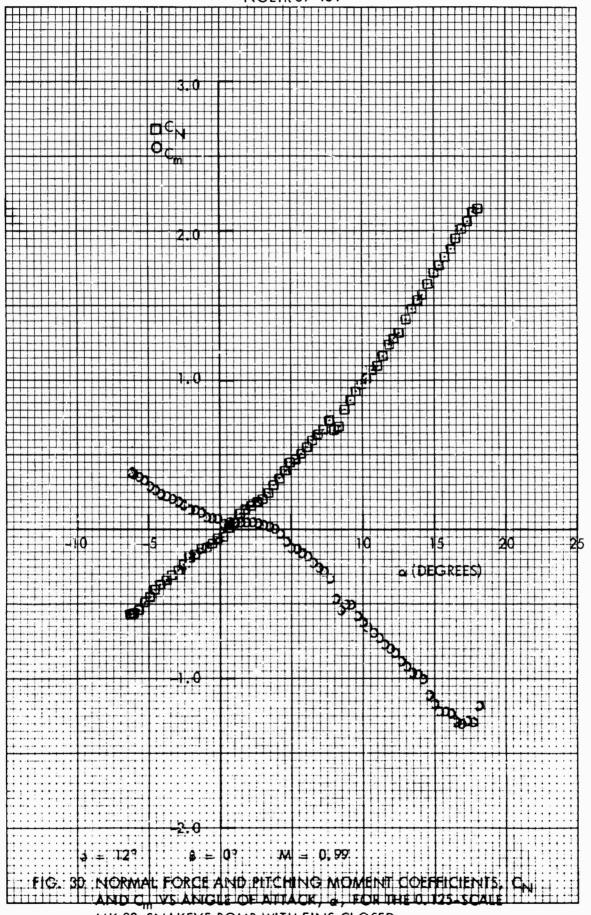




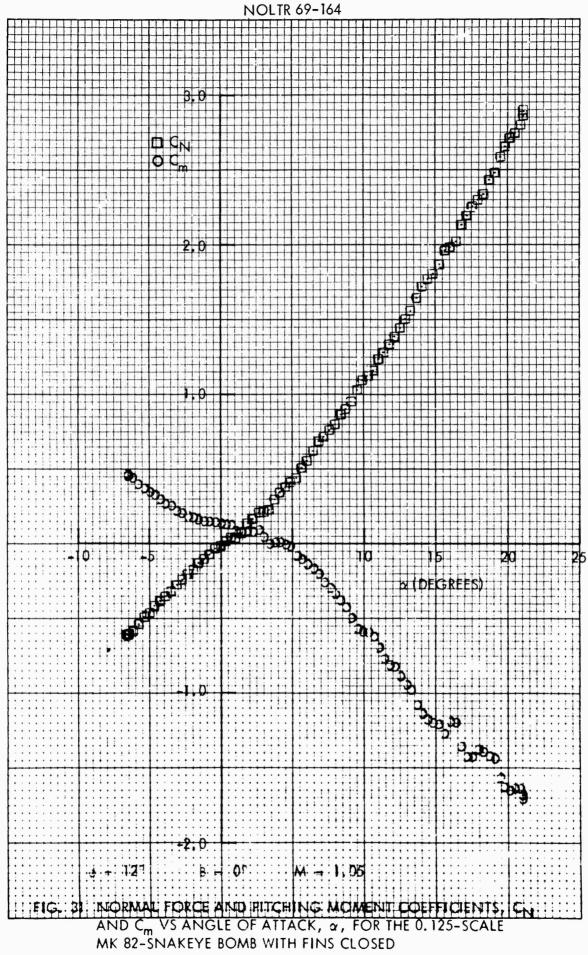
MK 82-SNAKEYE BOMB WITH FINS CLOSED



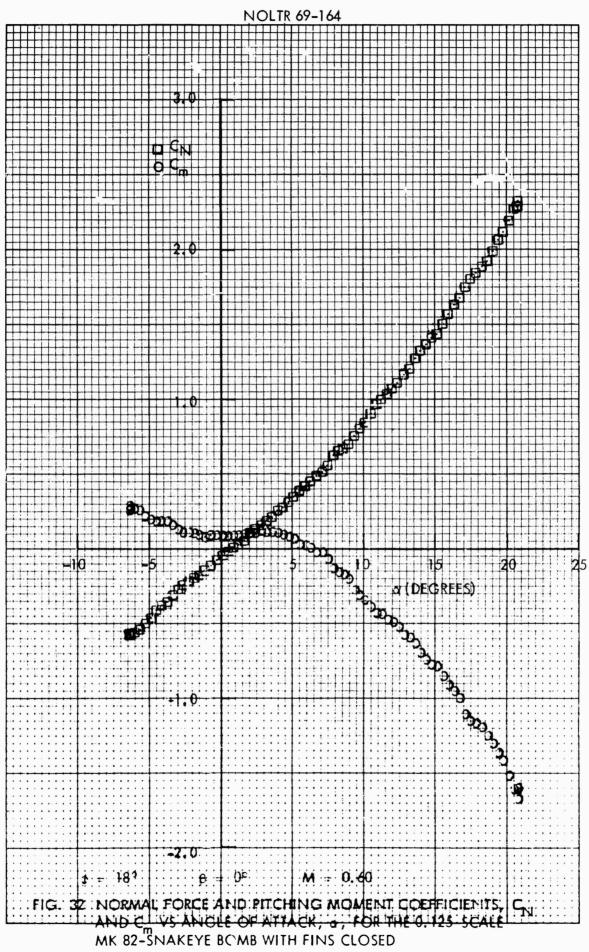


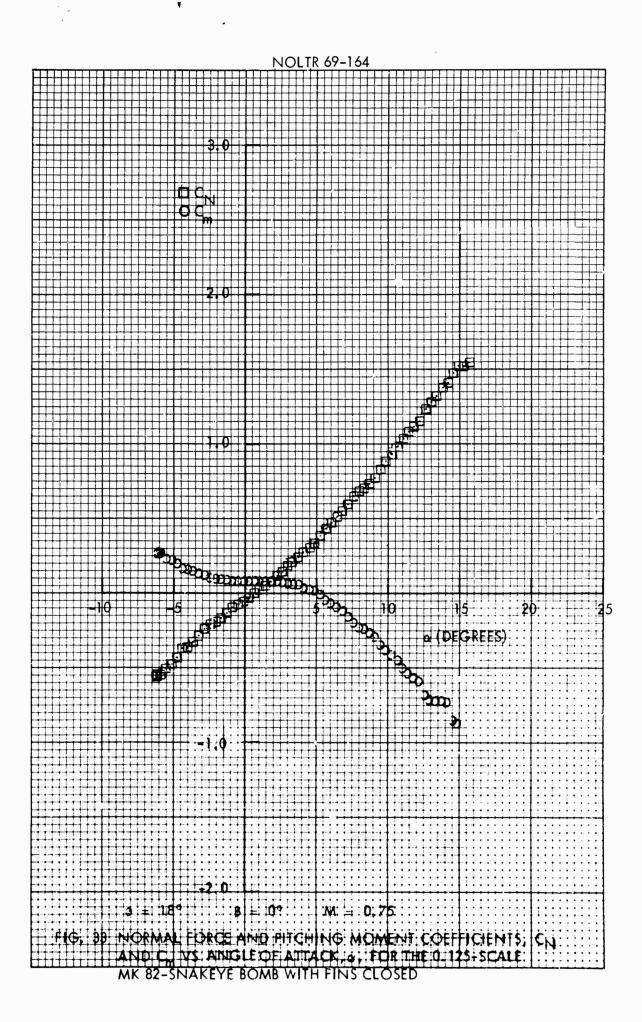


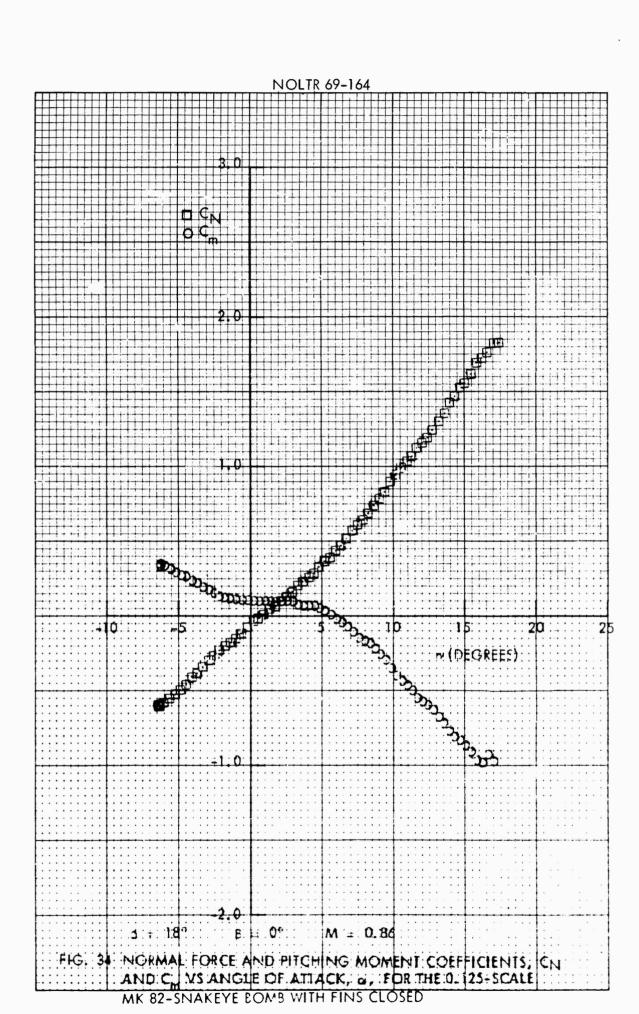
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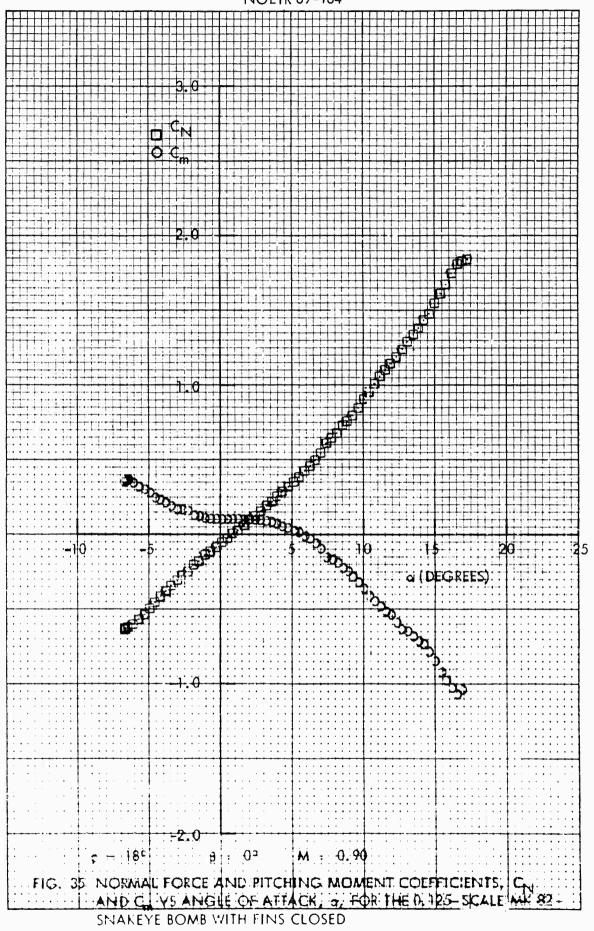




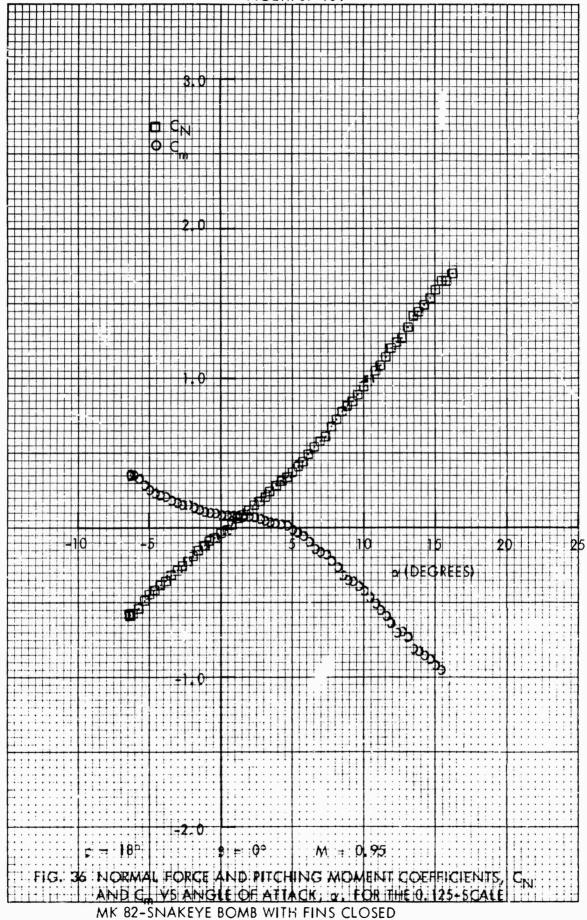


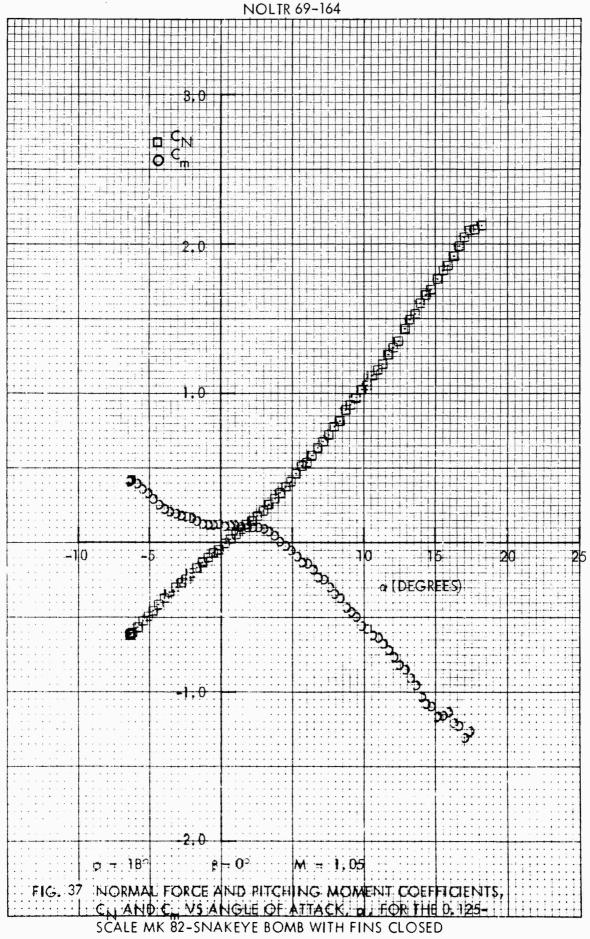


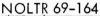


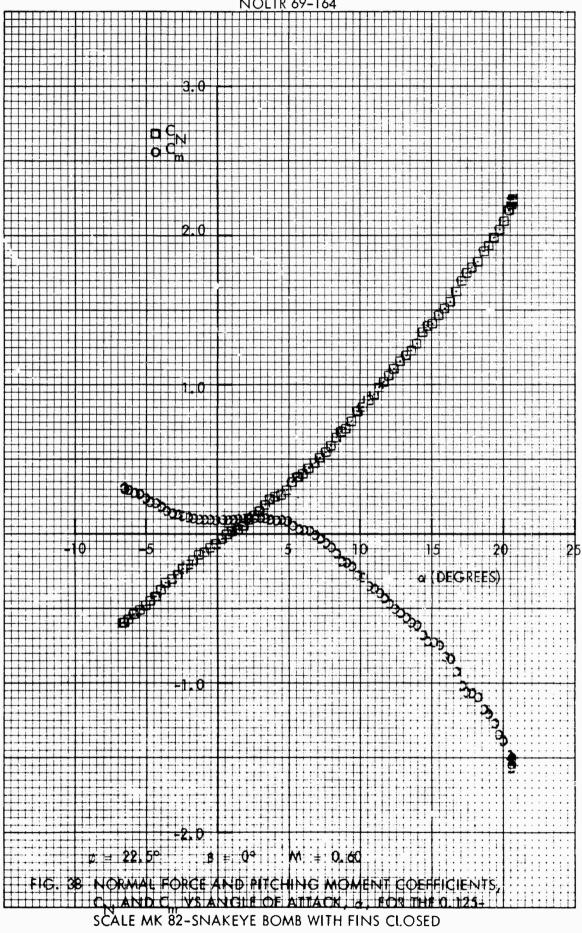


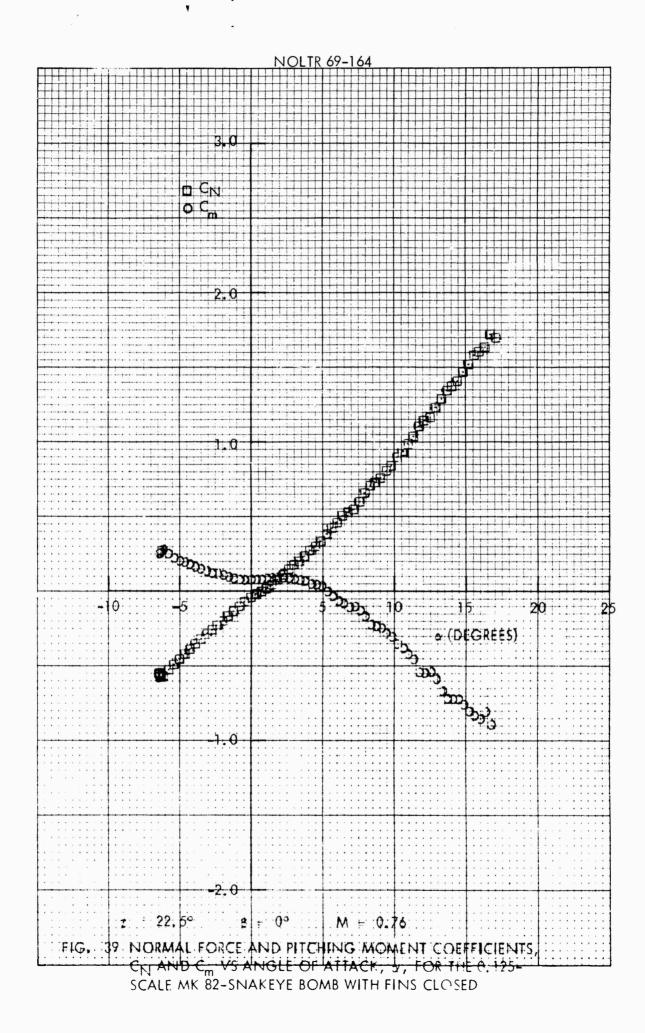


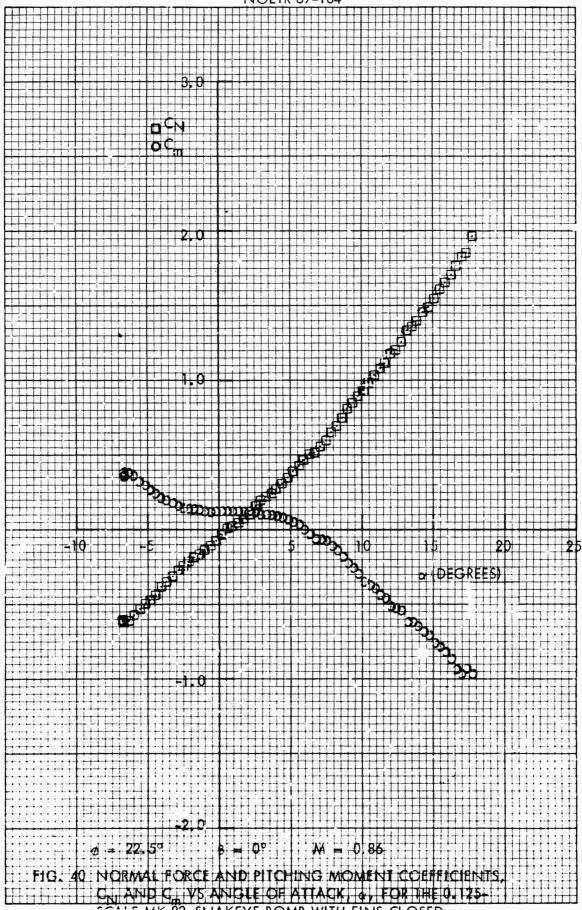




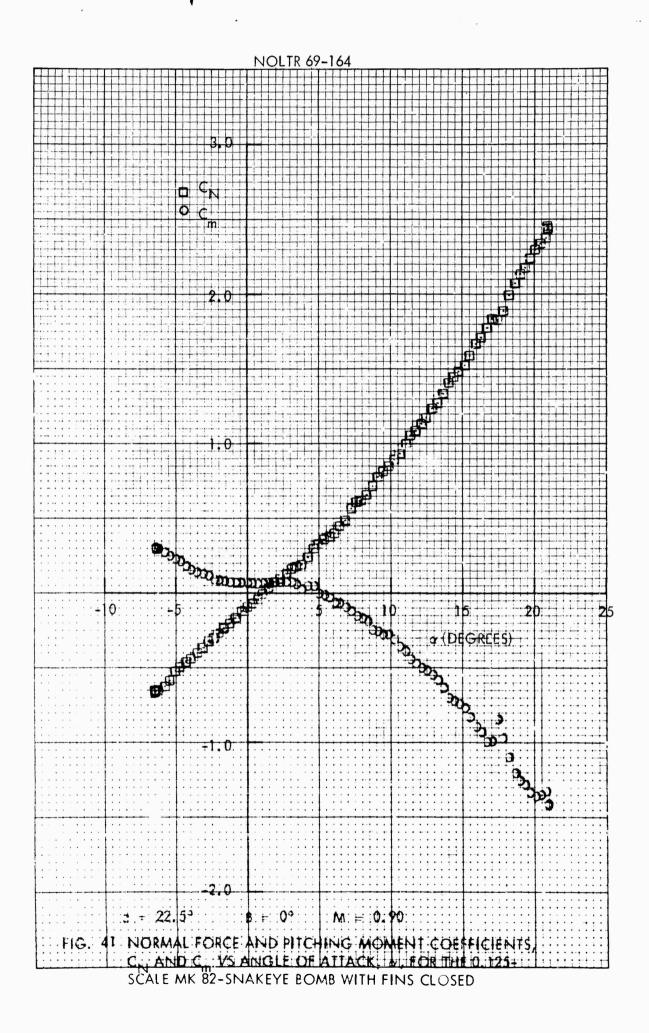


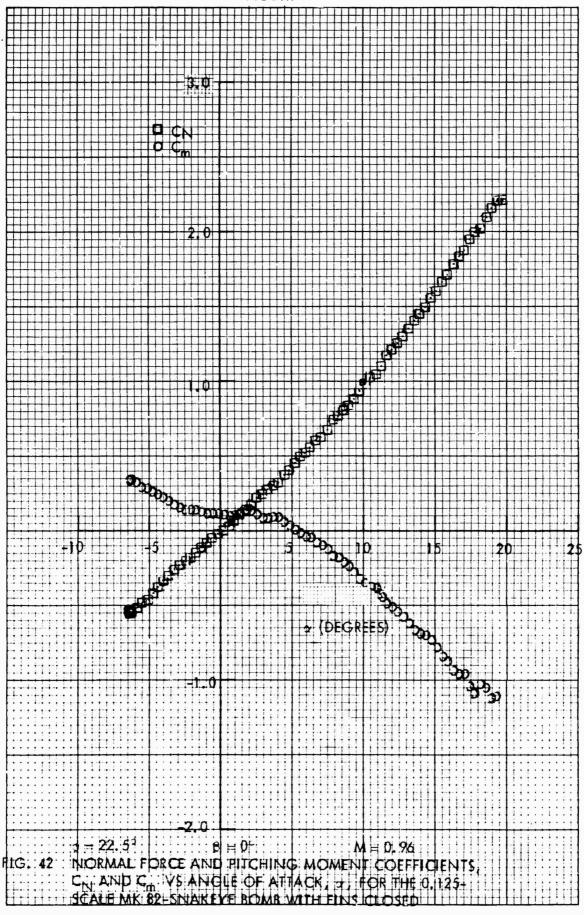


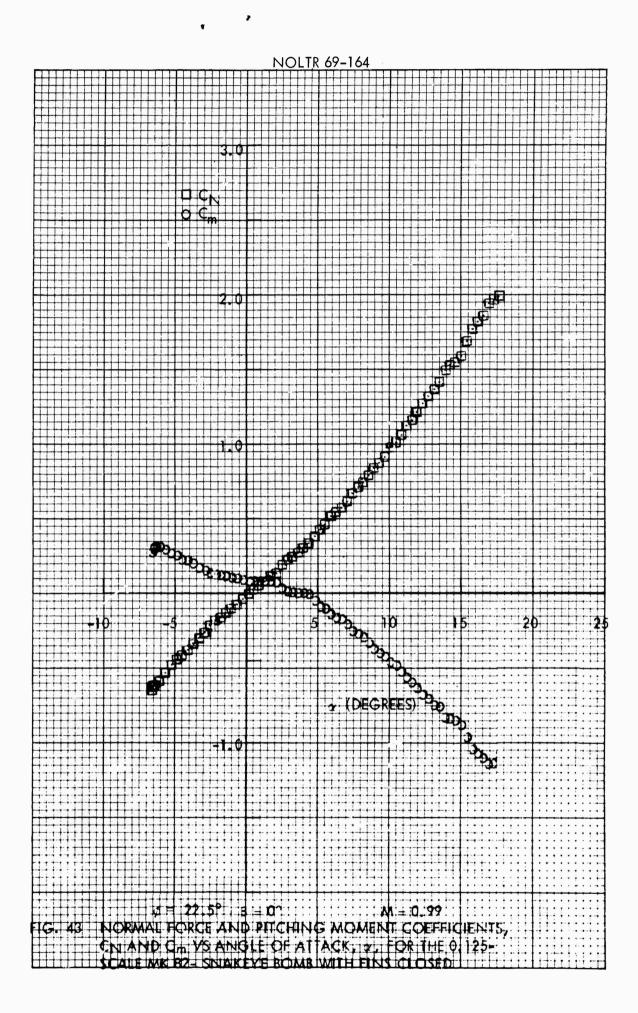


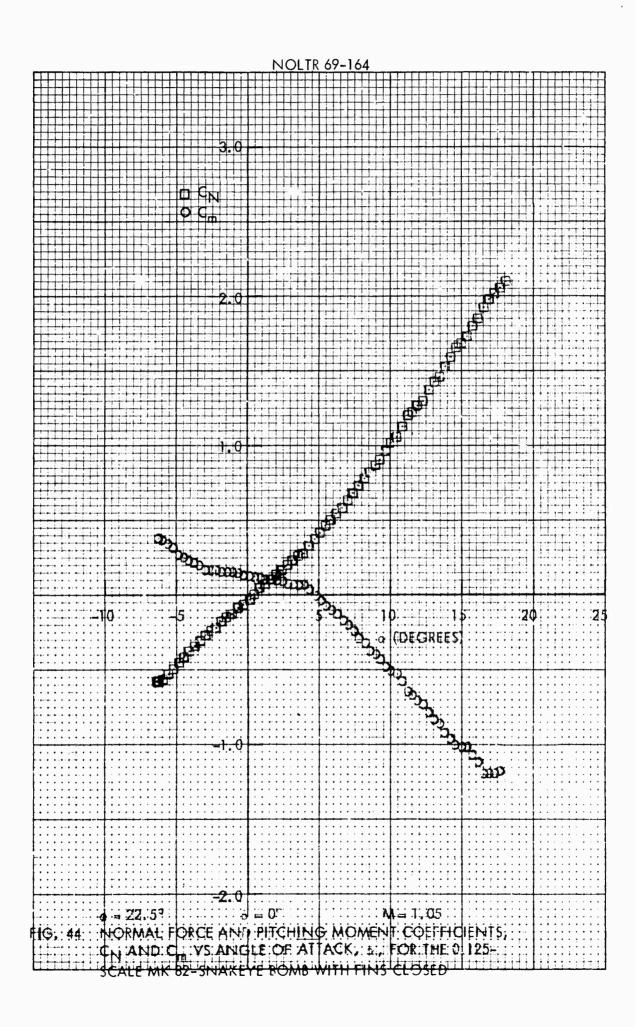


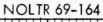
SCALE MK 82-SNAKEYE BOMB WITH FINS CLOSED

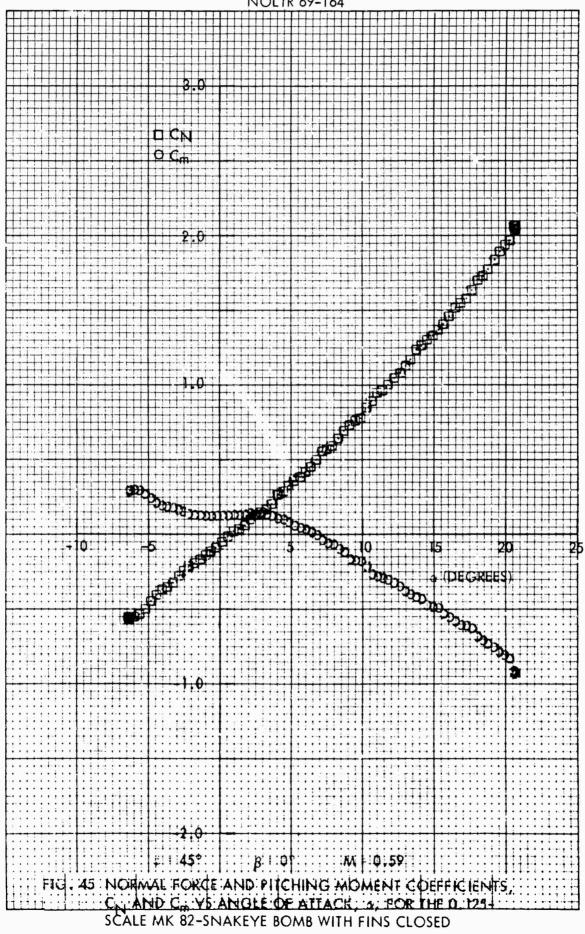


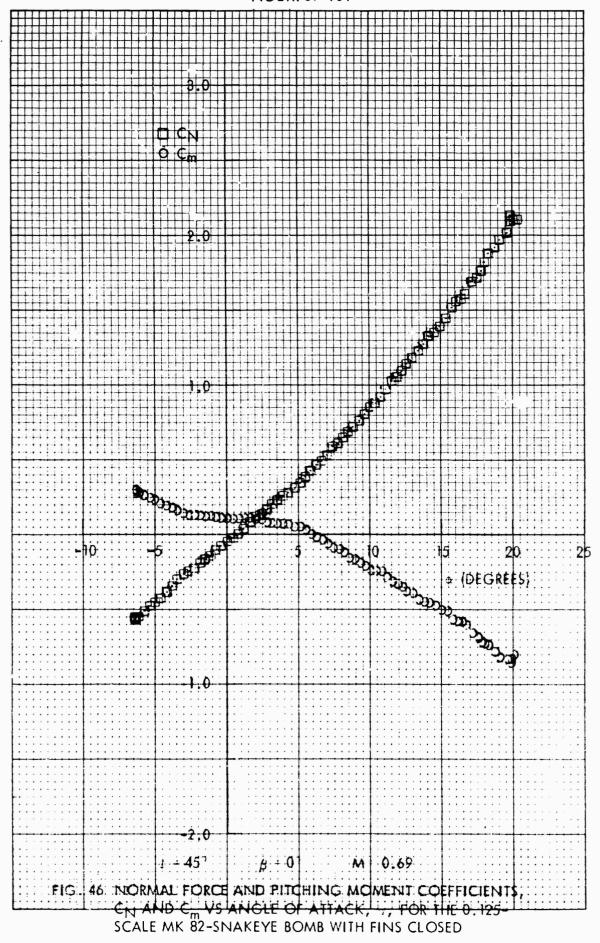


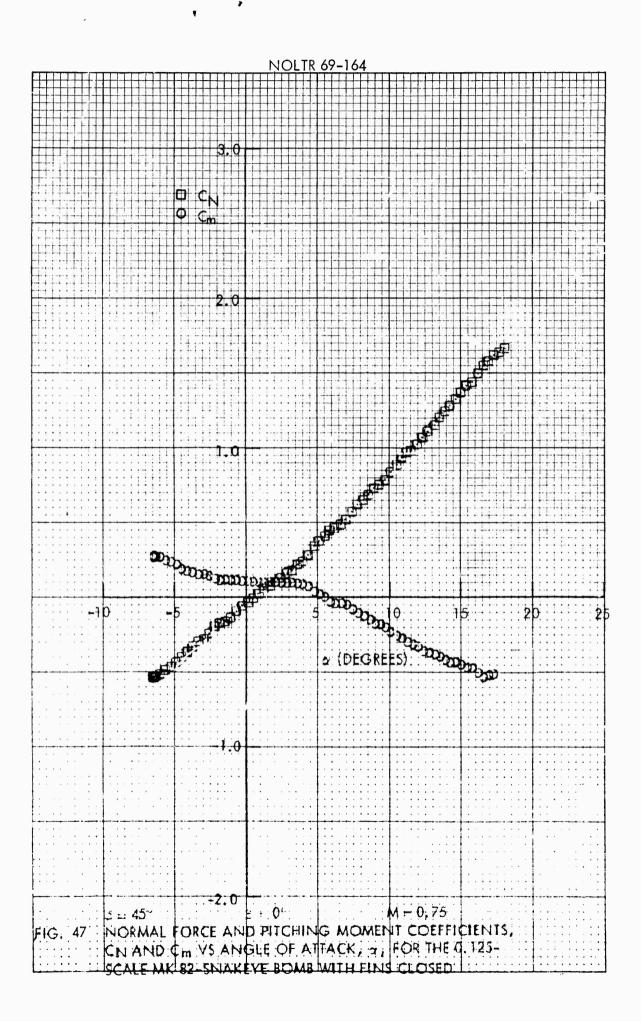


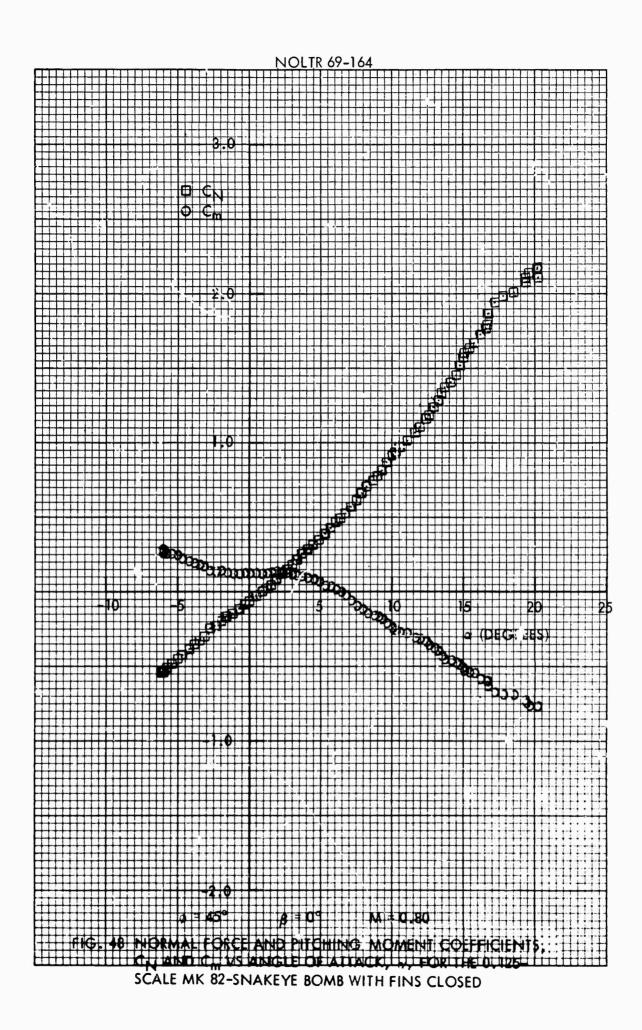


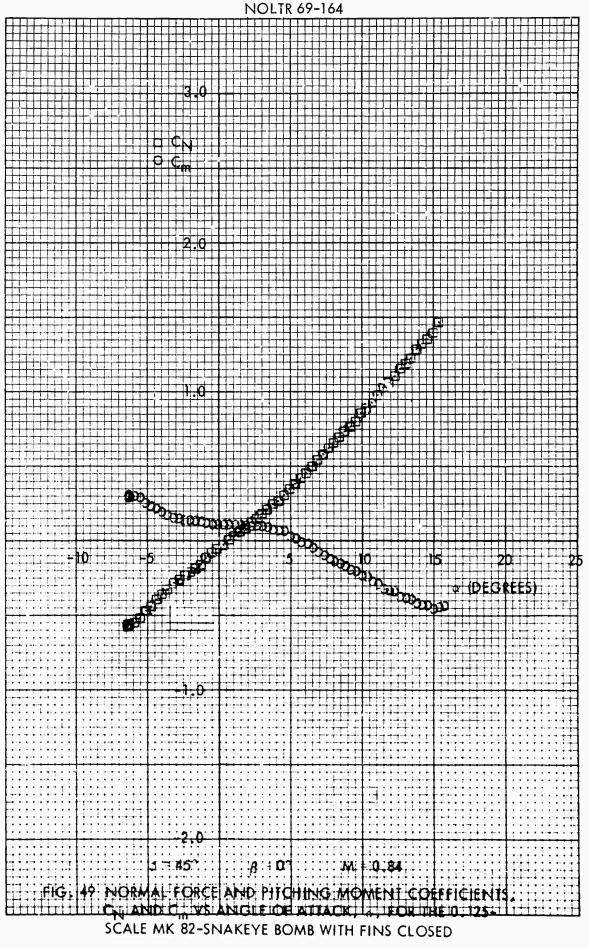


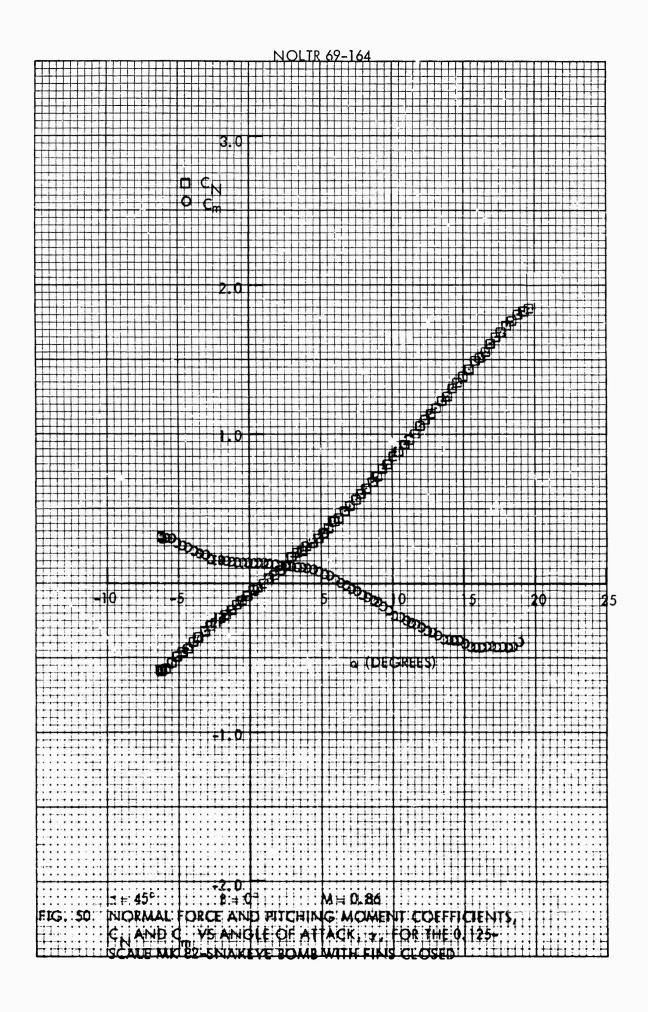


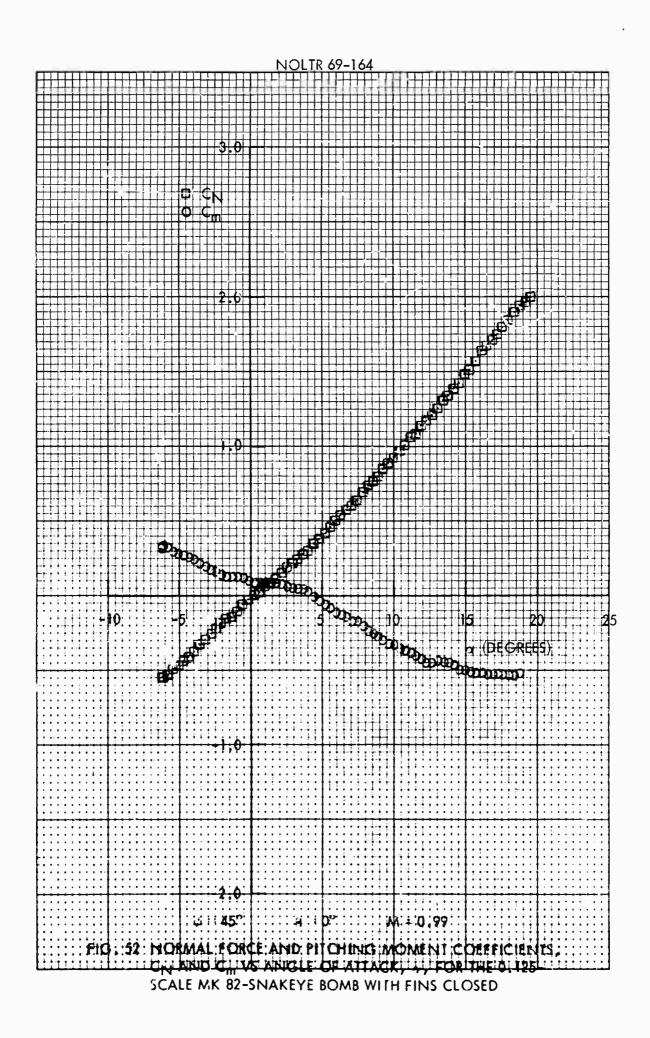


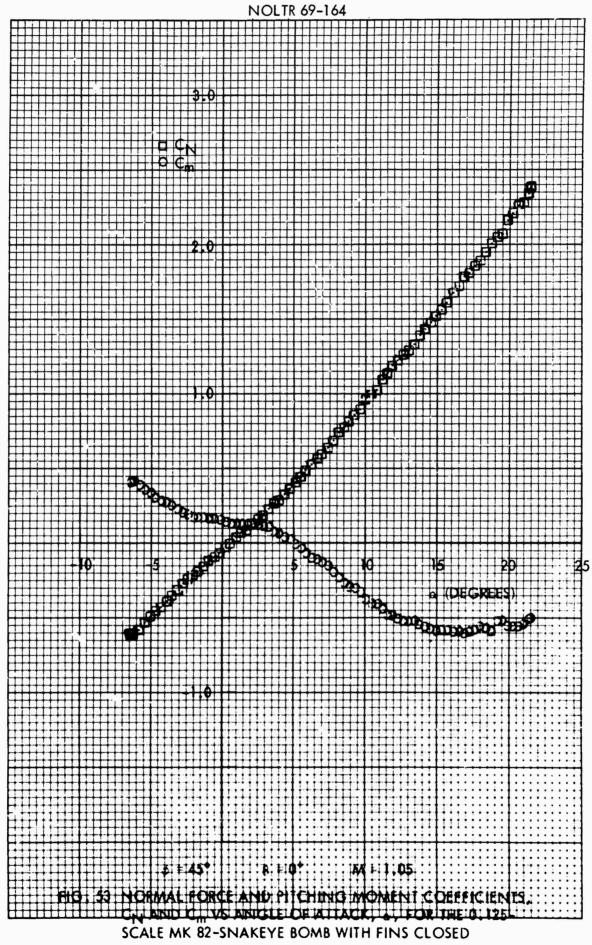




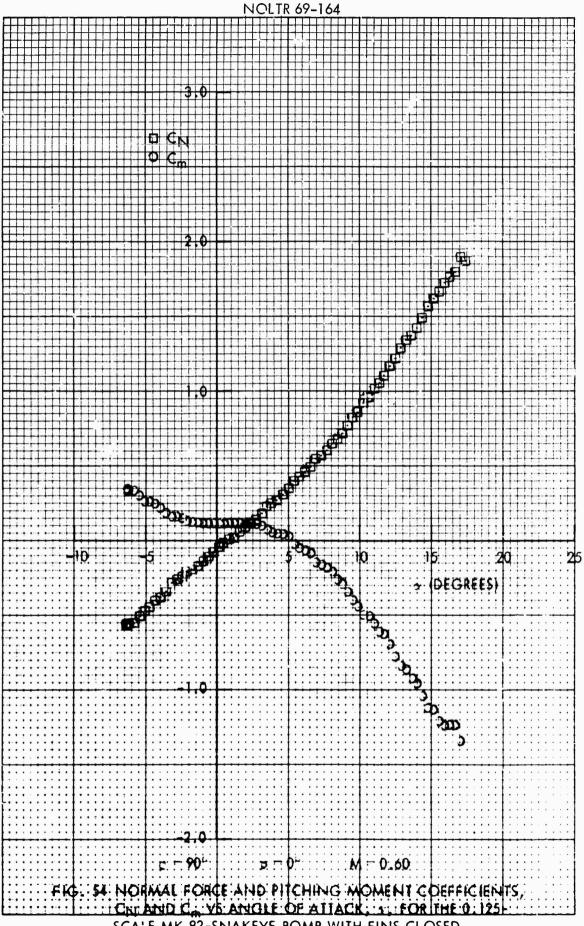




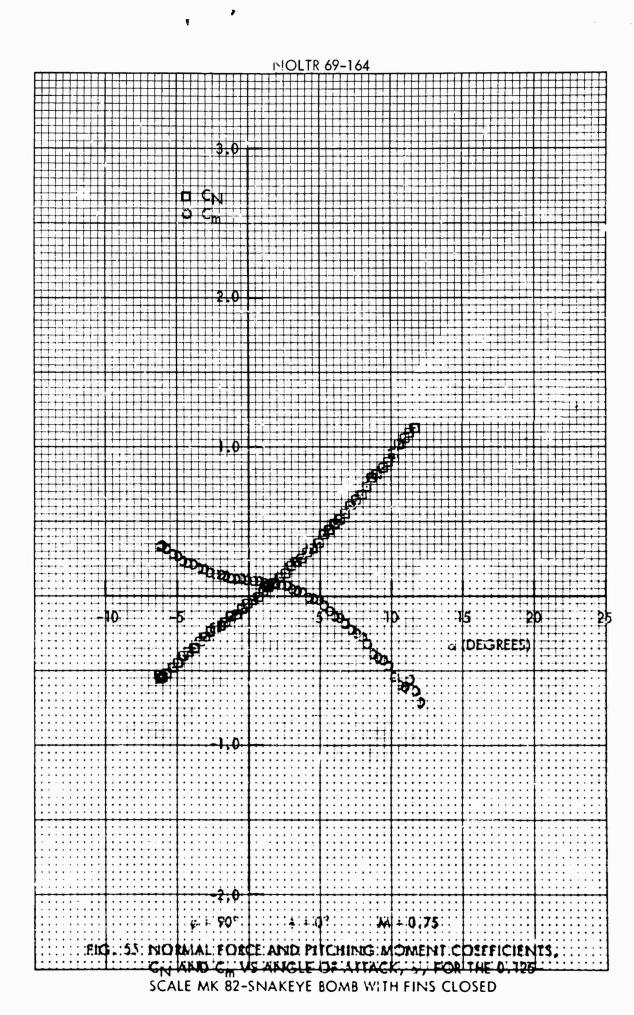


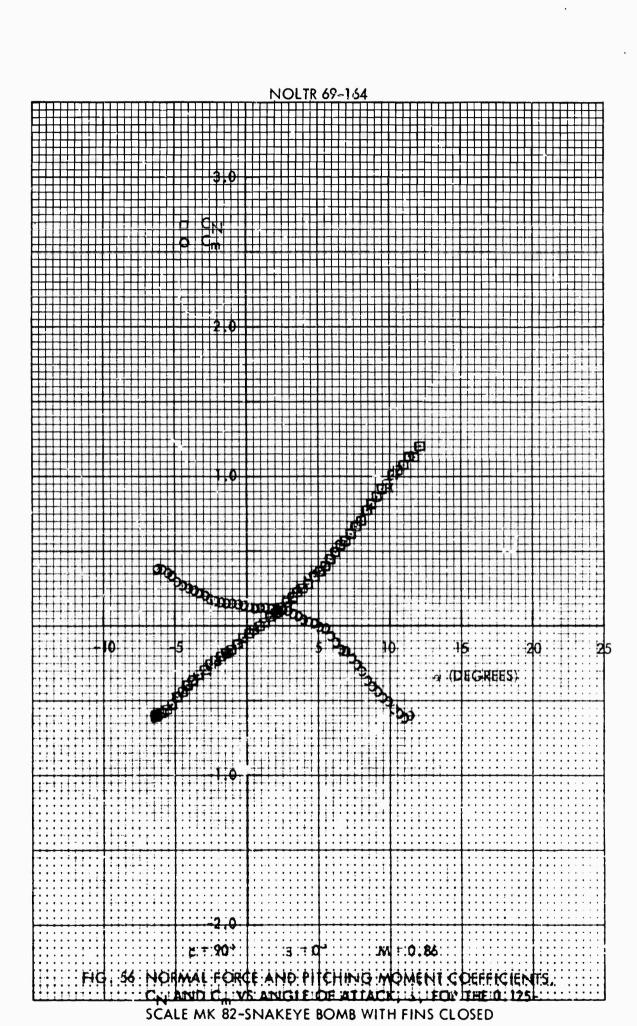




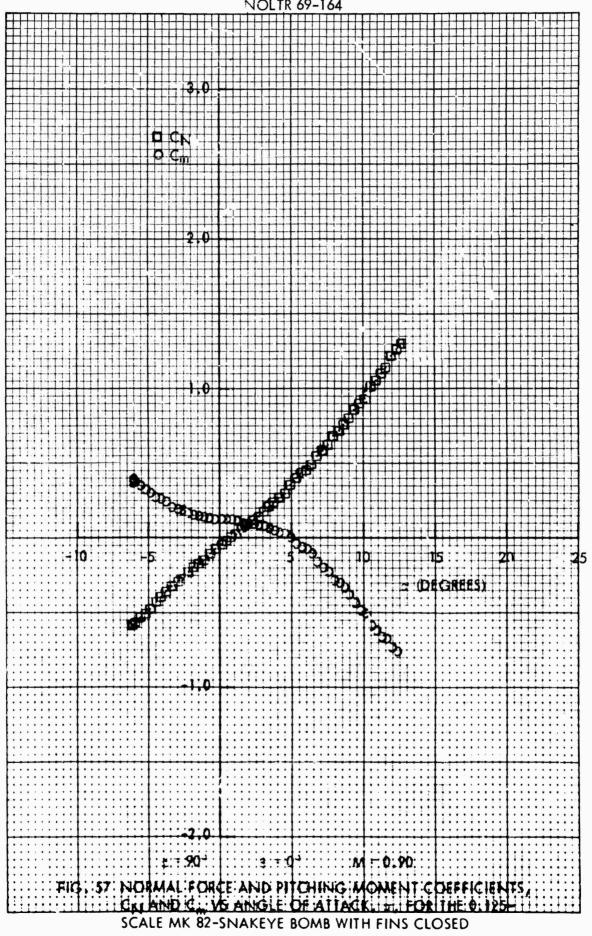


SCALE MK 82-SNAKEYE BOMB WITH FINS CLOSED

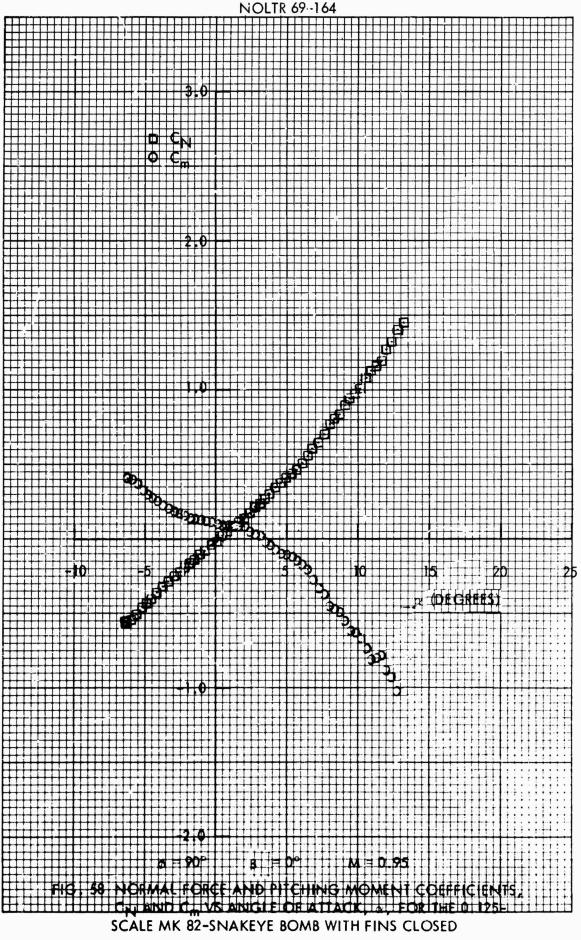


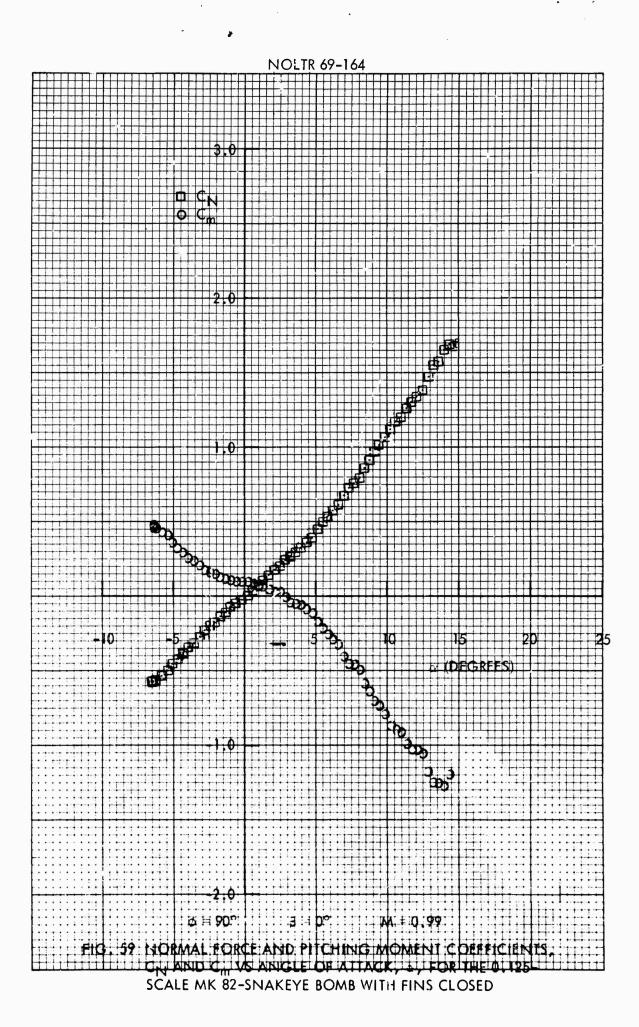


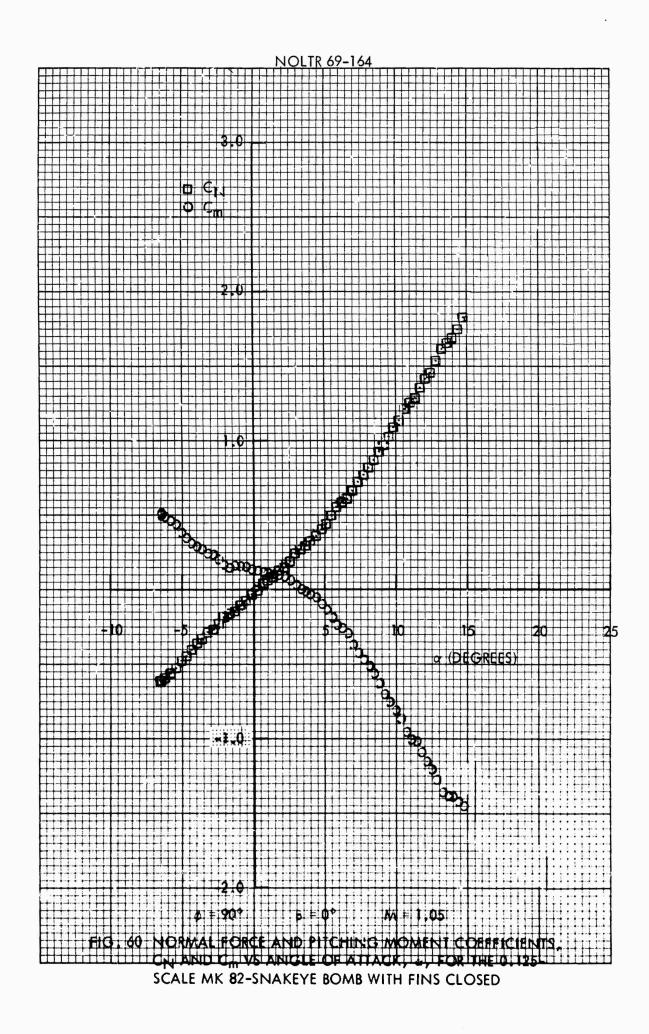


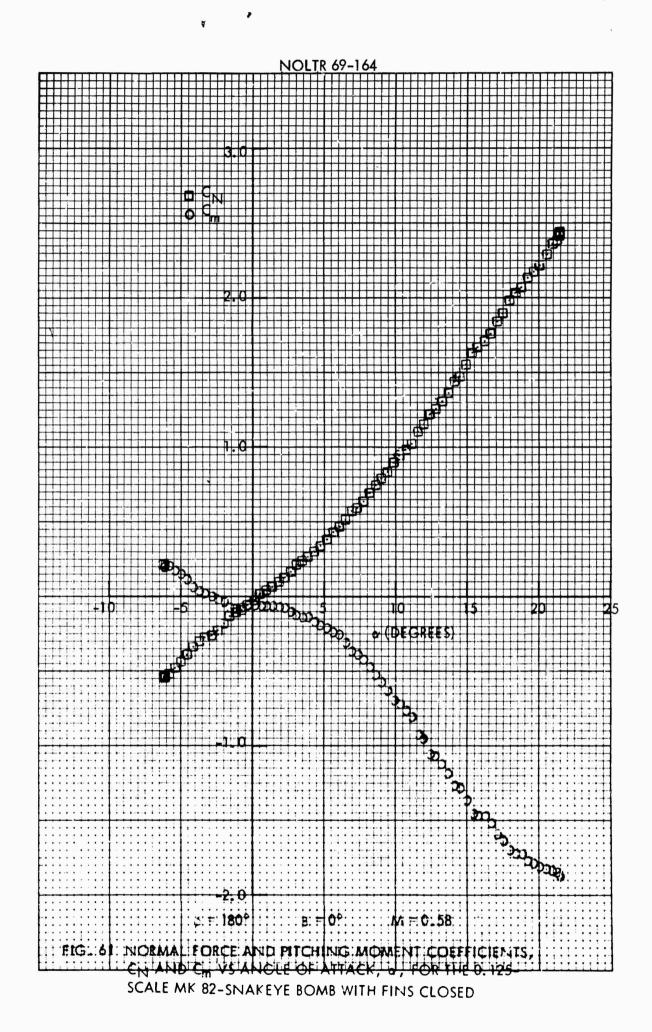


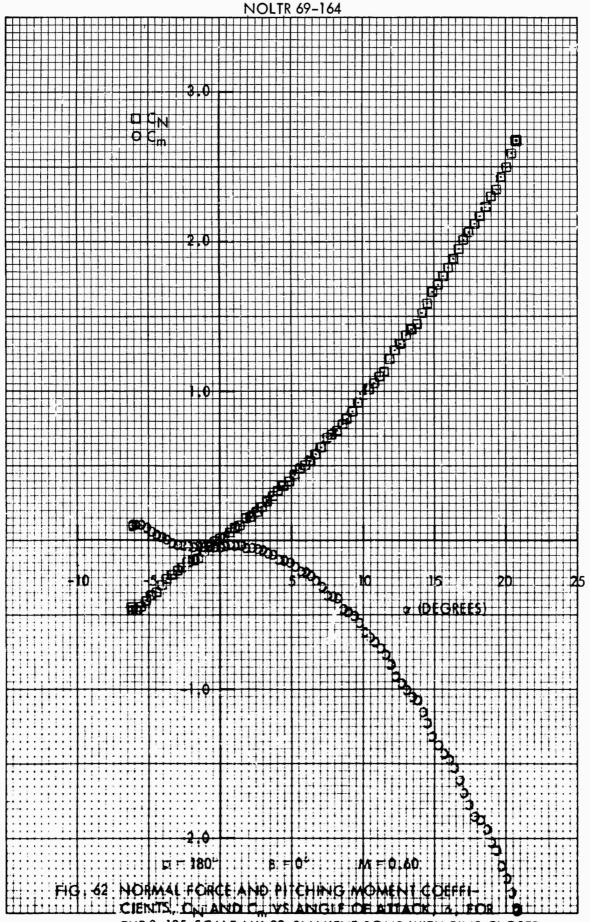




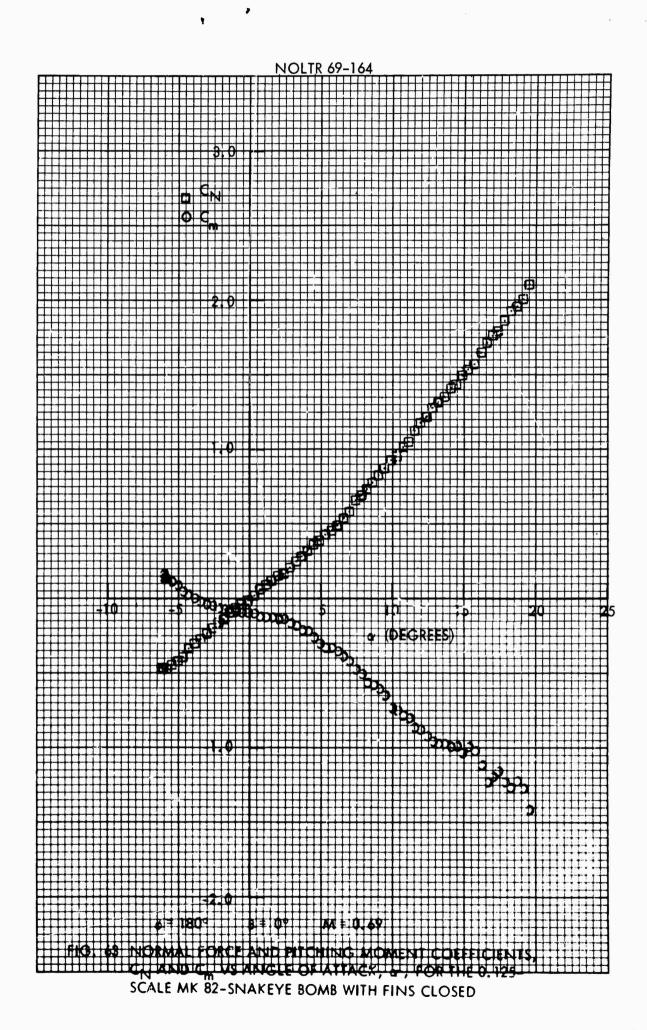


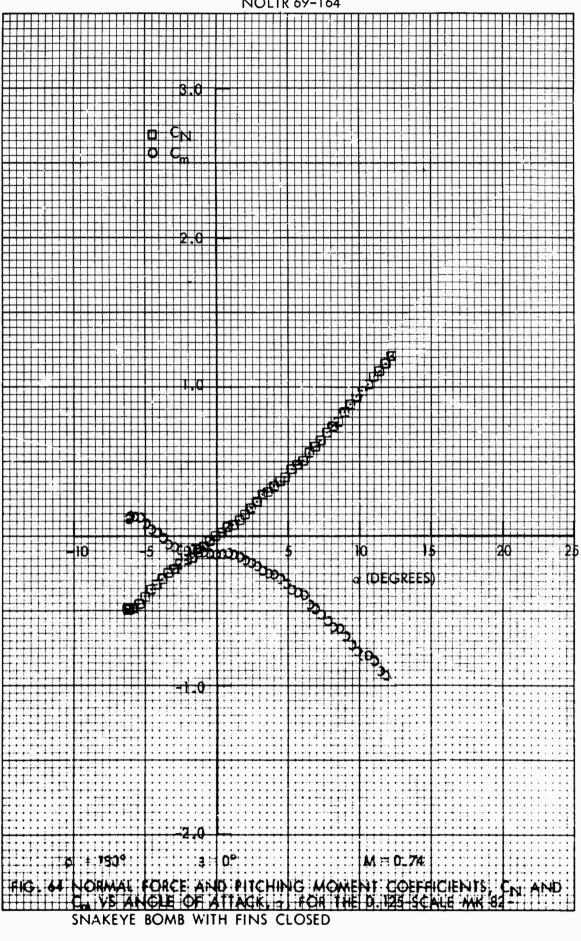


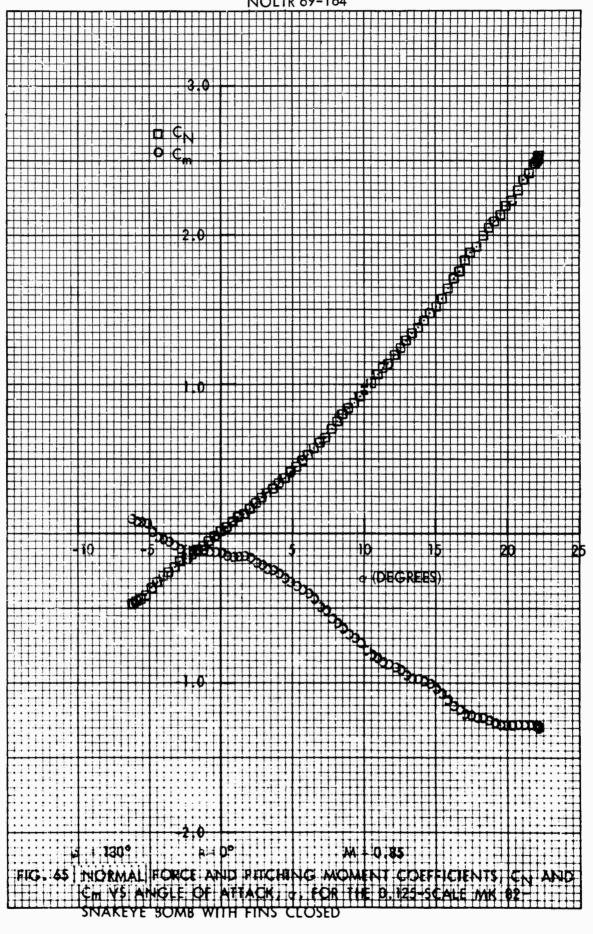


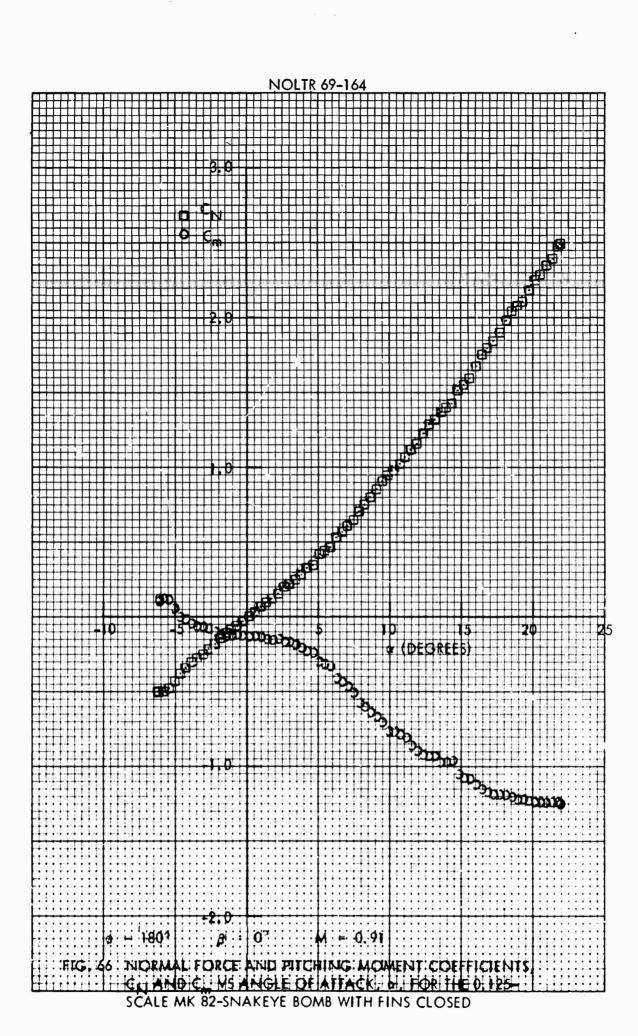


THE 0.125-SCALE MK 82-SNAKEYE BOMB WITH FINS CLOSED

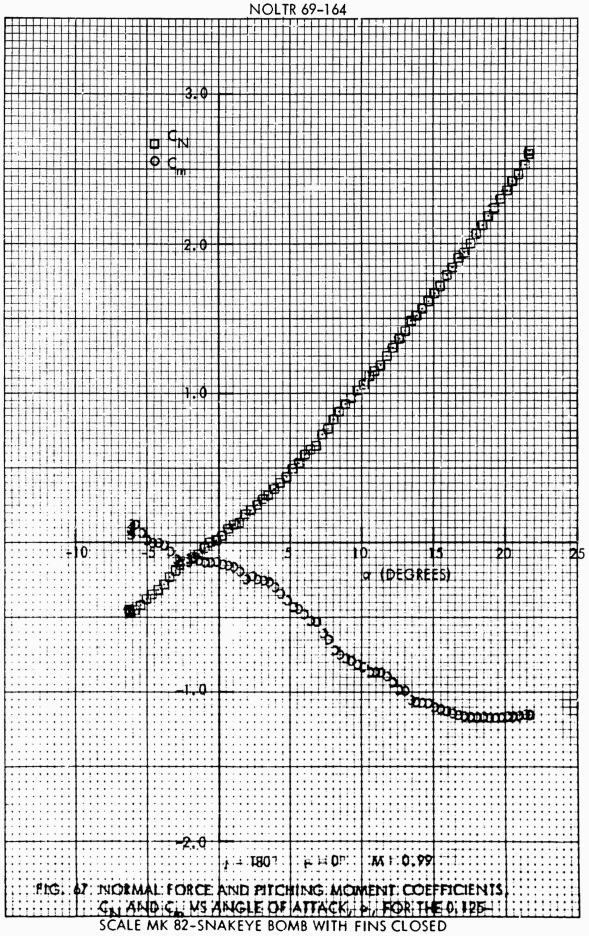


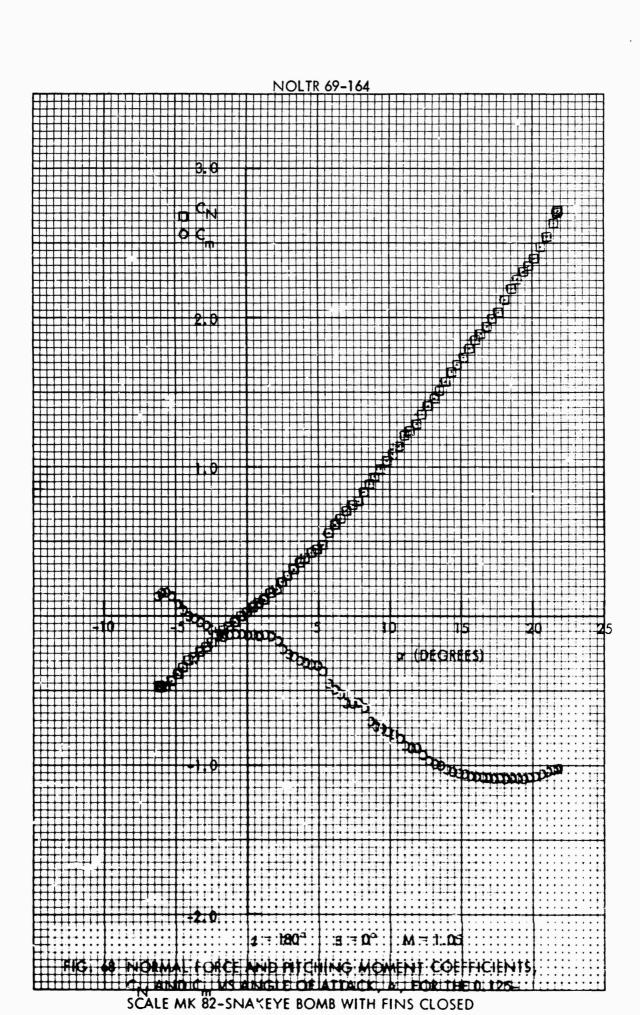




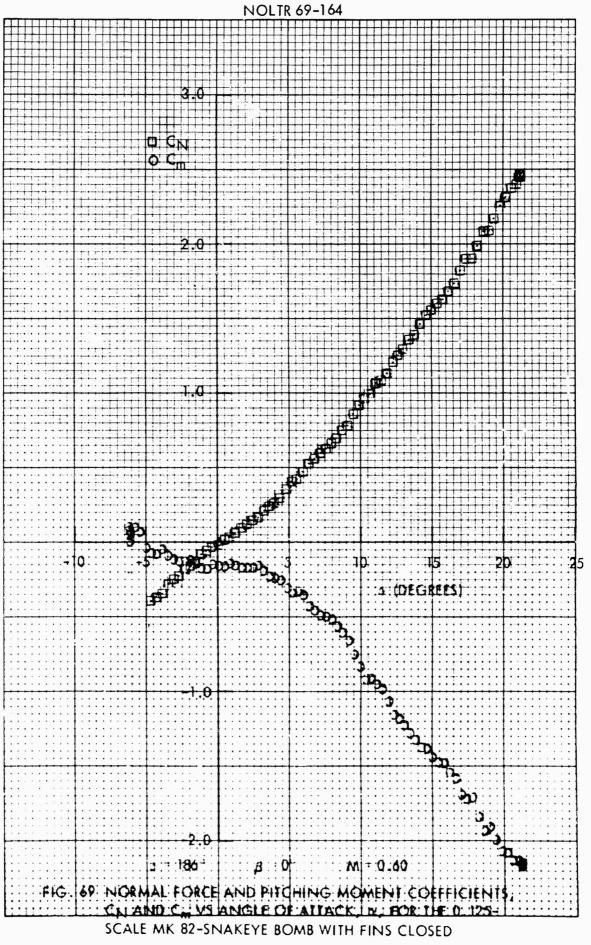


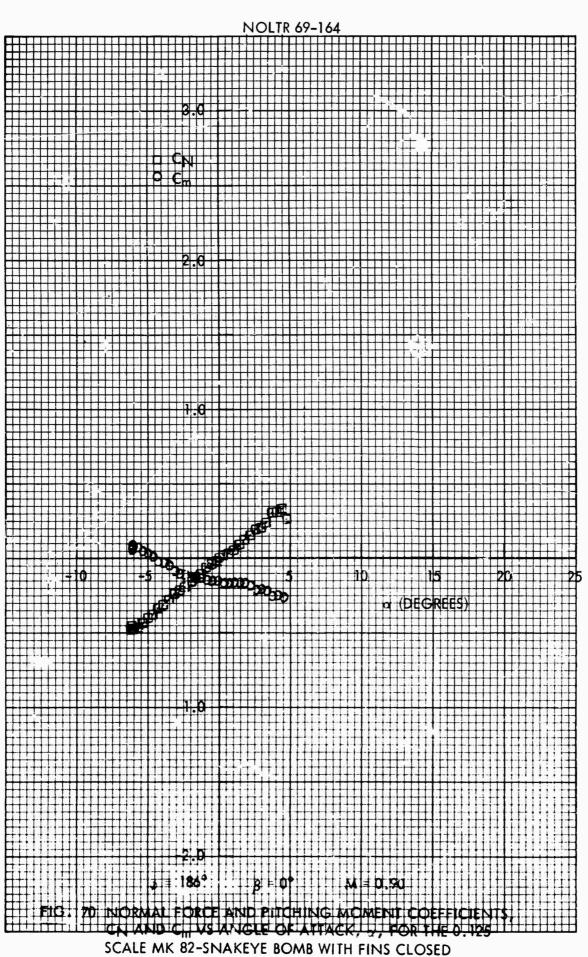




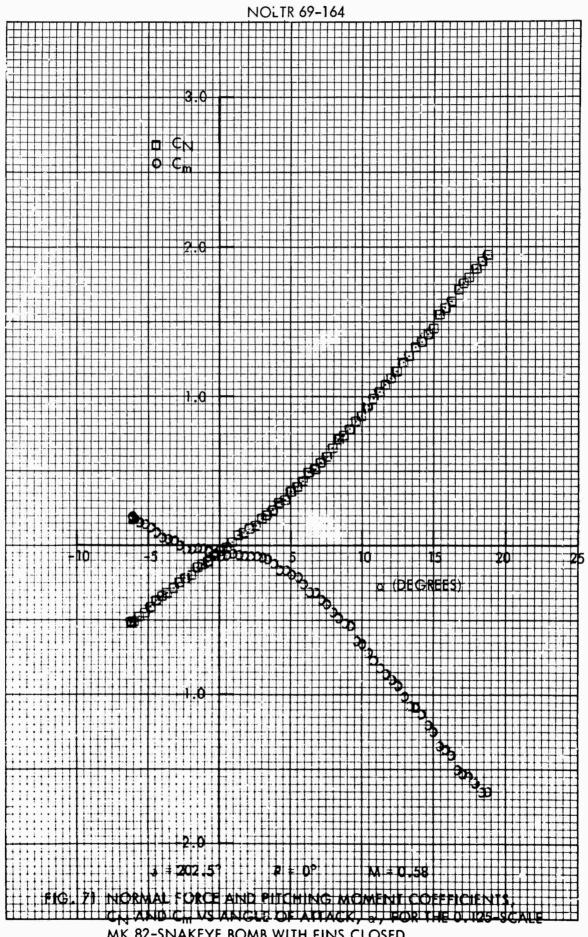


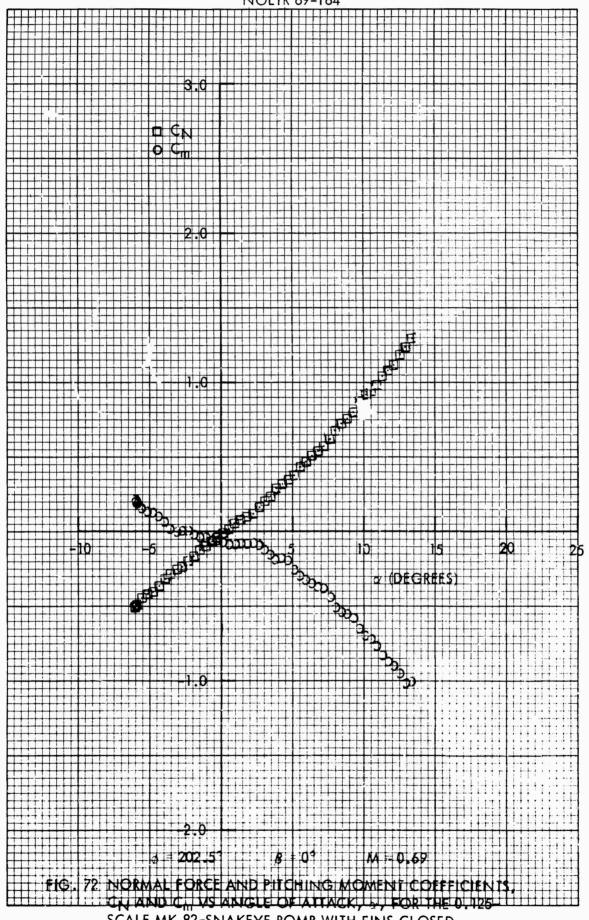




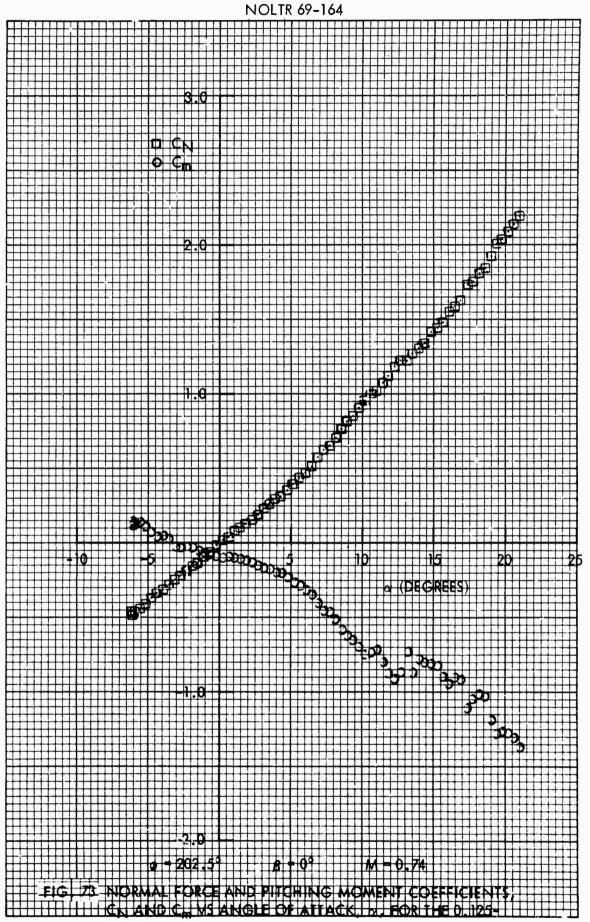




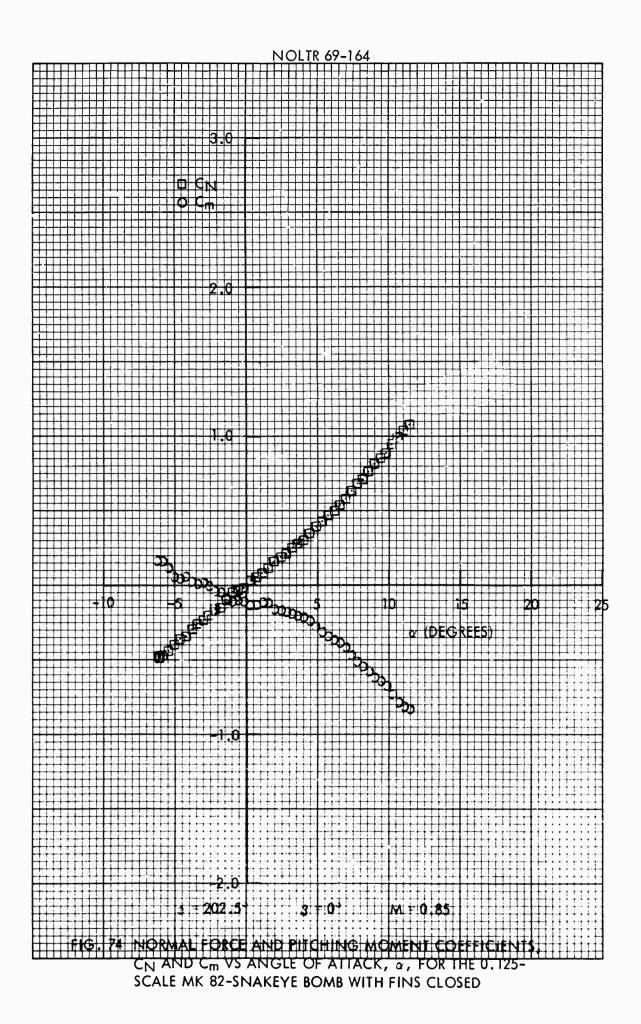


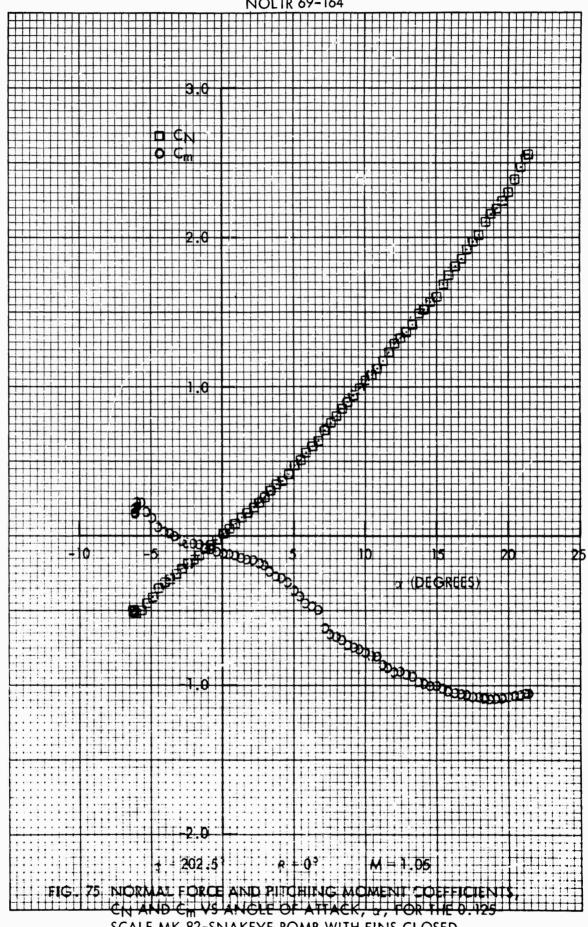


SCALE MK 82-SNAKEYE BOMB WITH FINS CLOSED

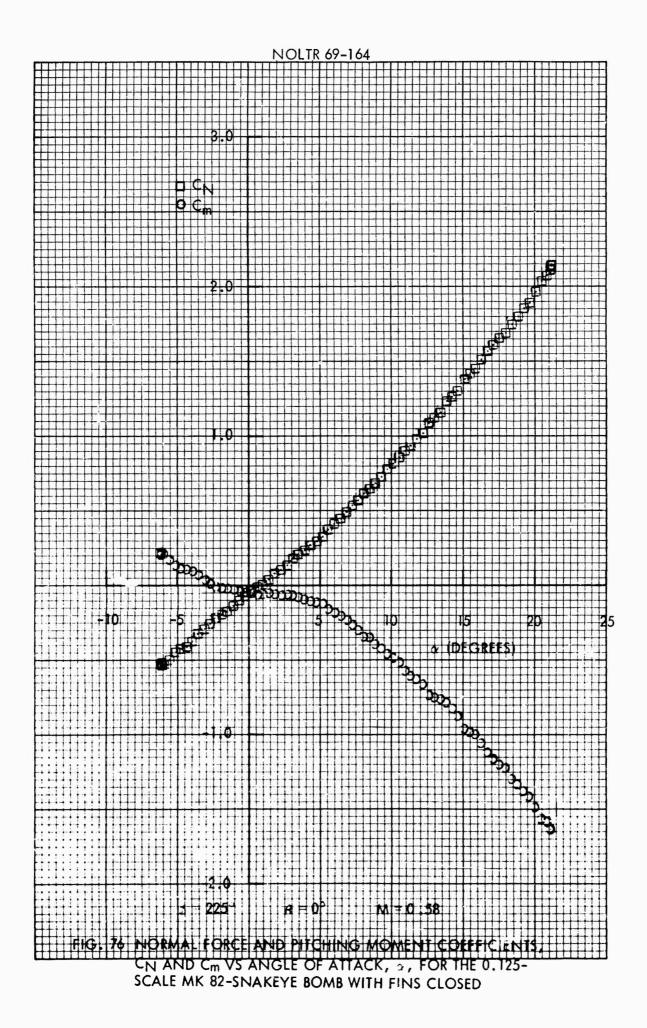


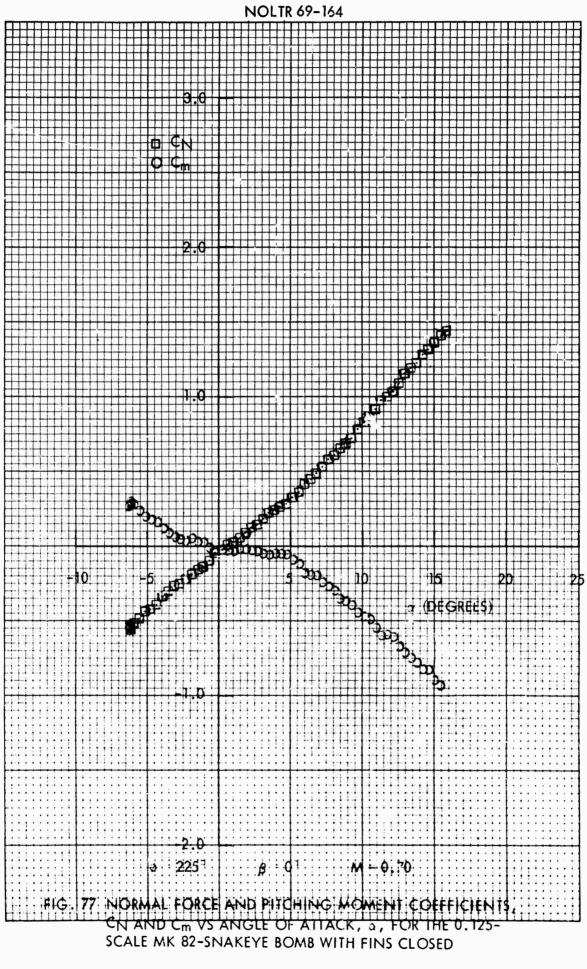
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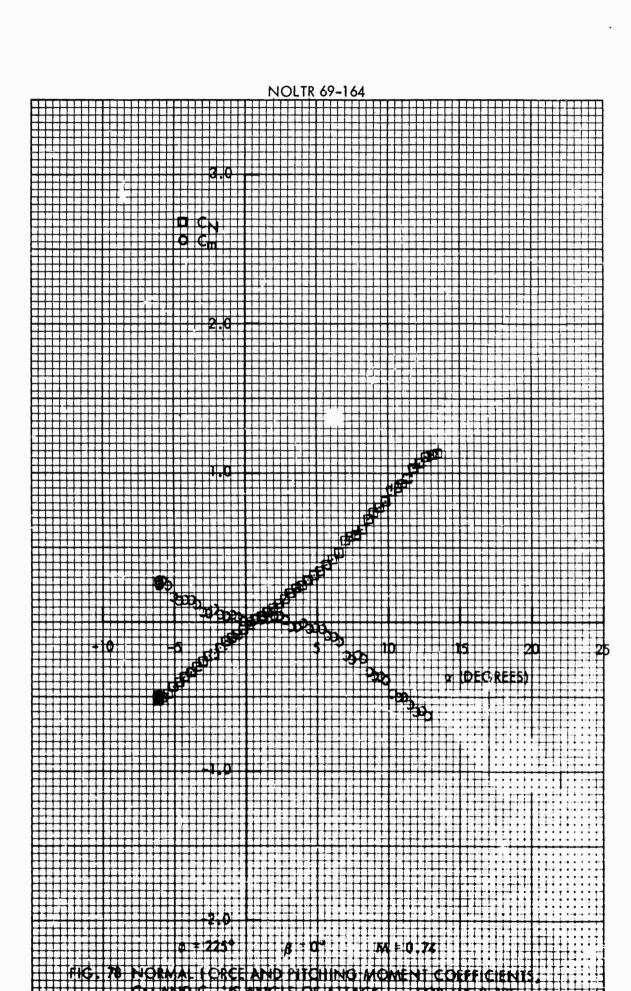




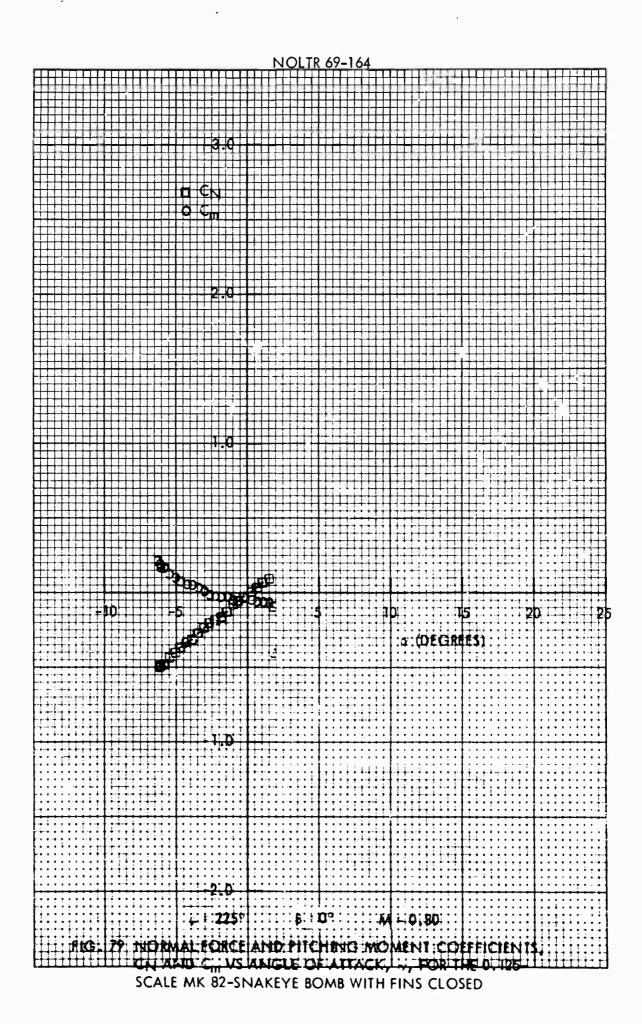
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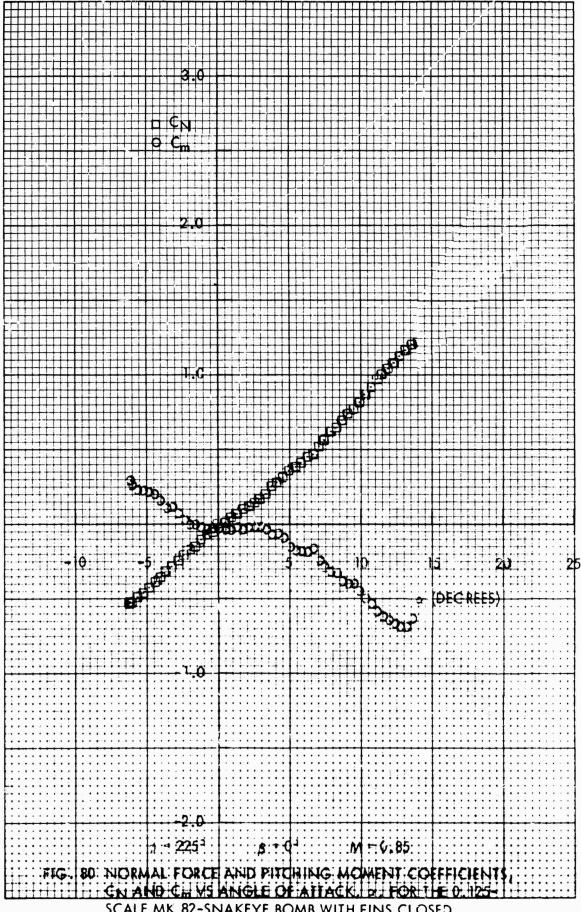




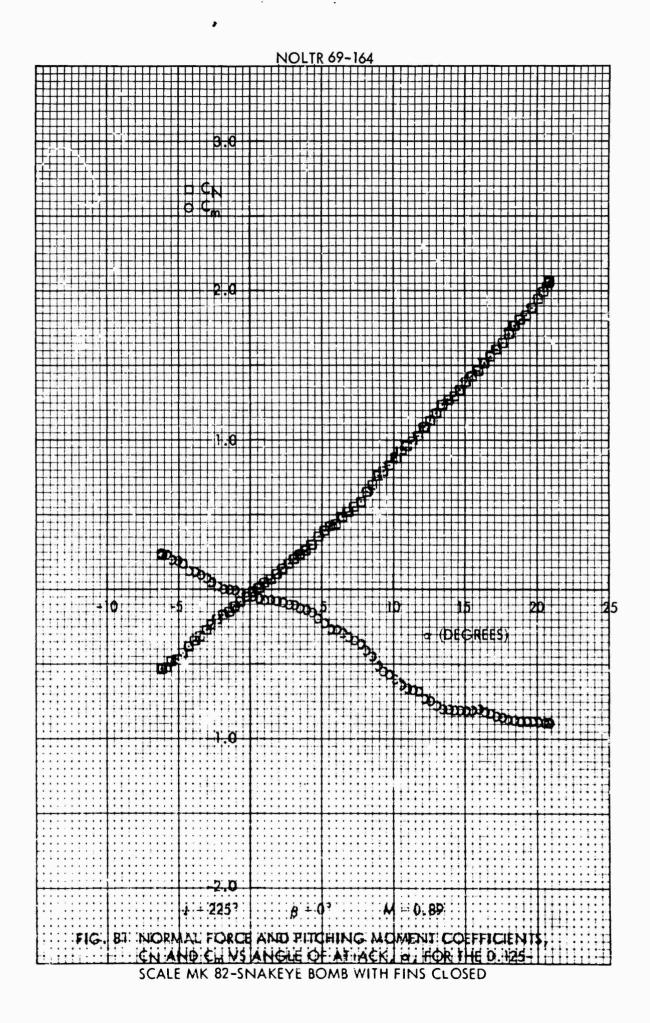
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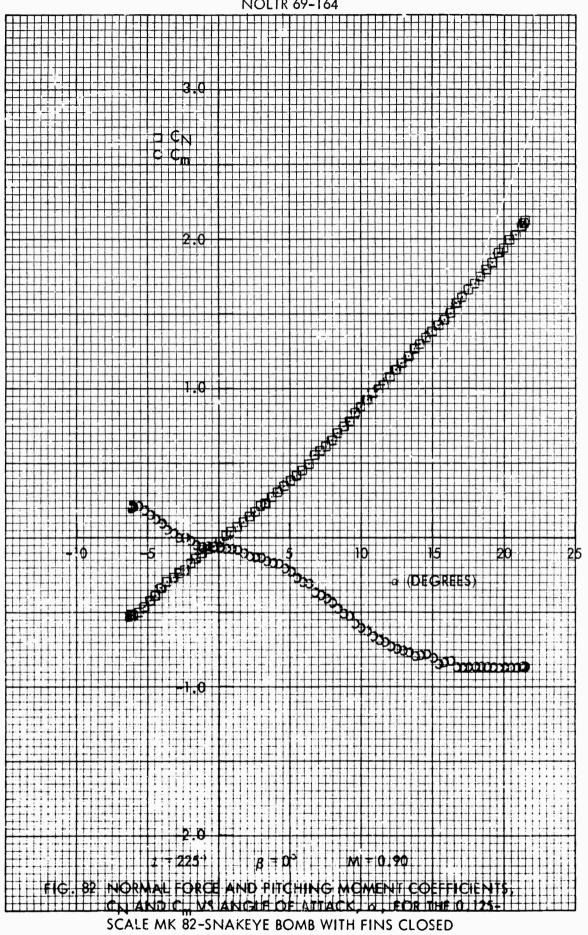


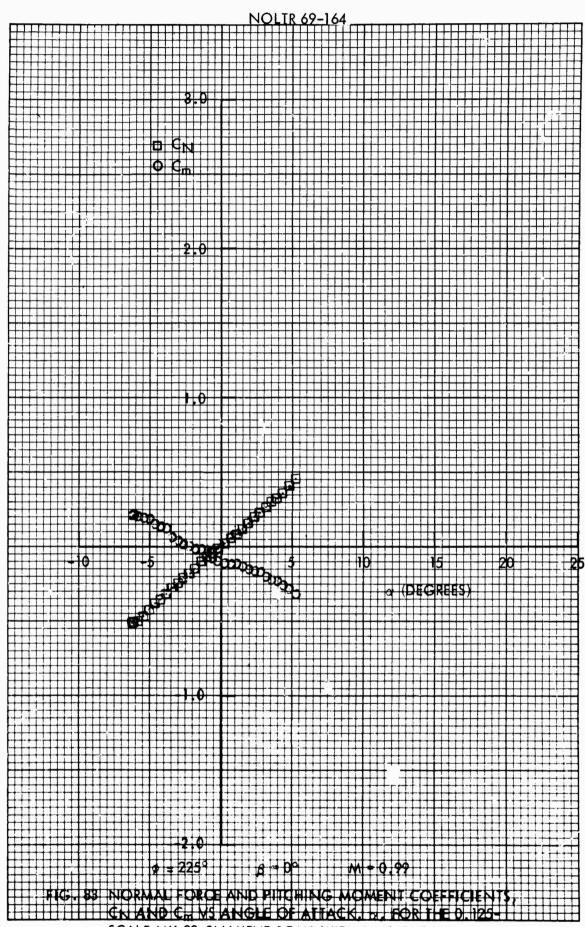
NOLTR 69-164



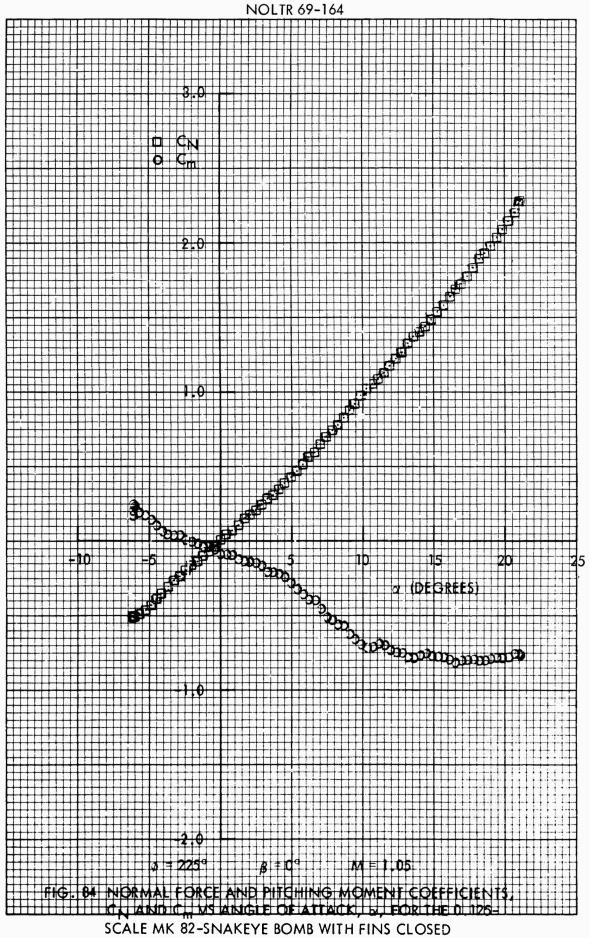
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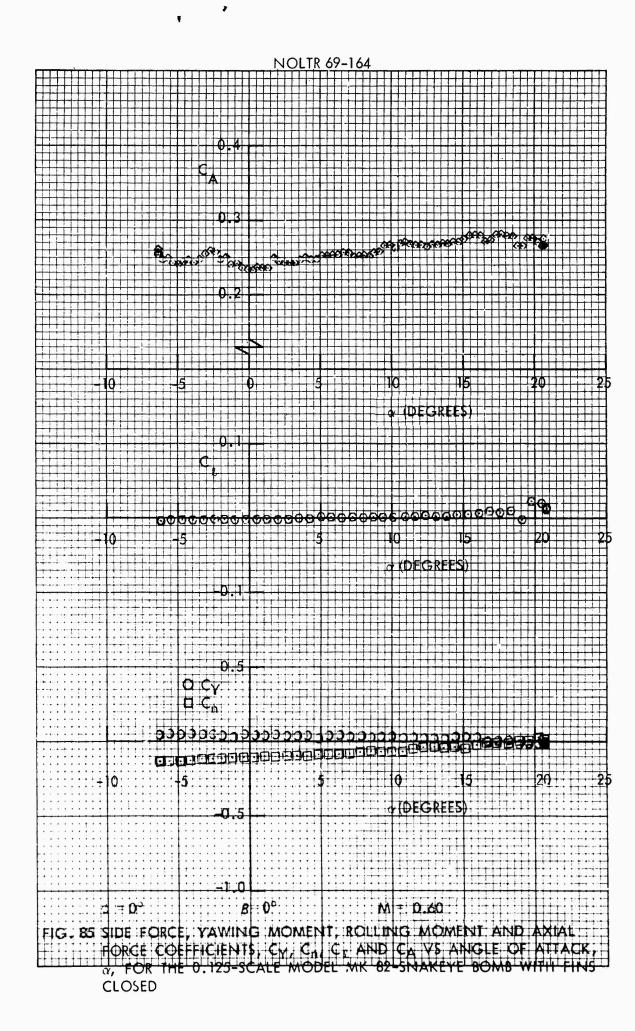




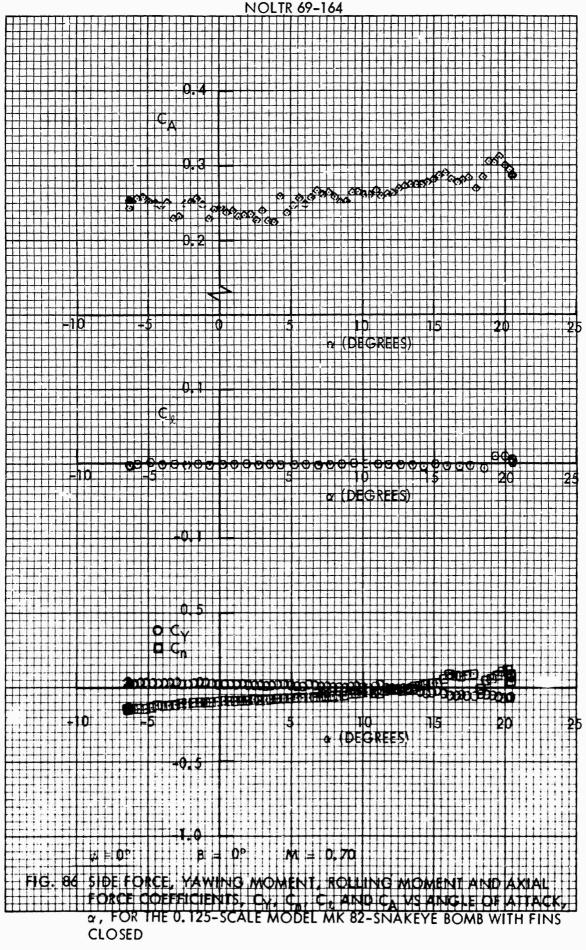


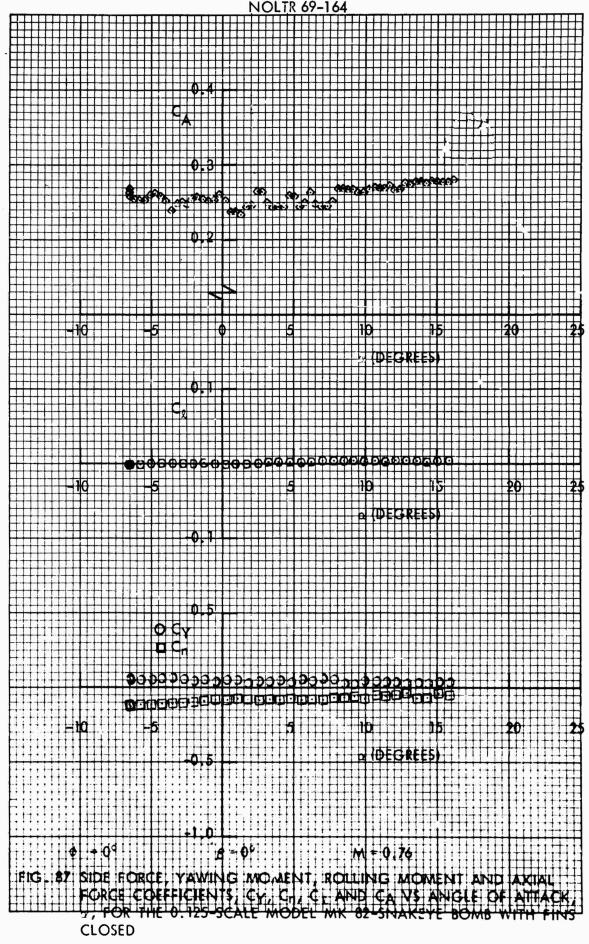
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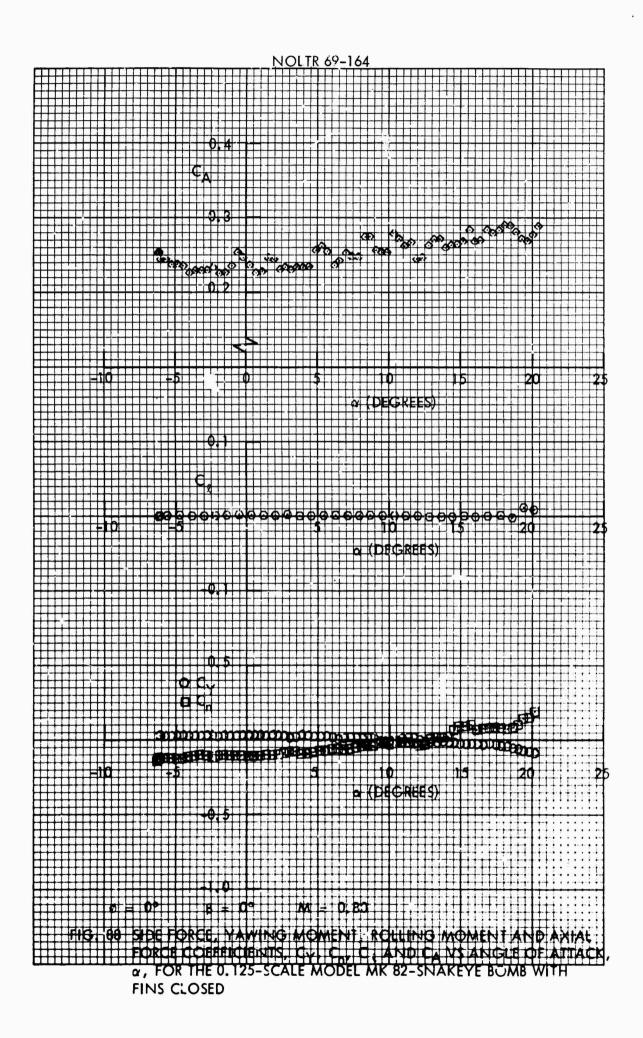


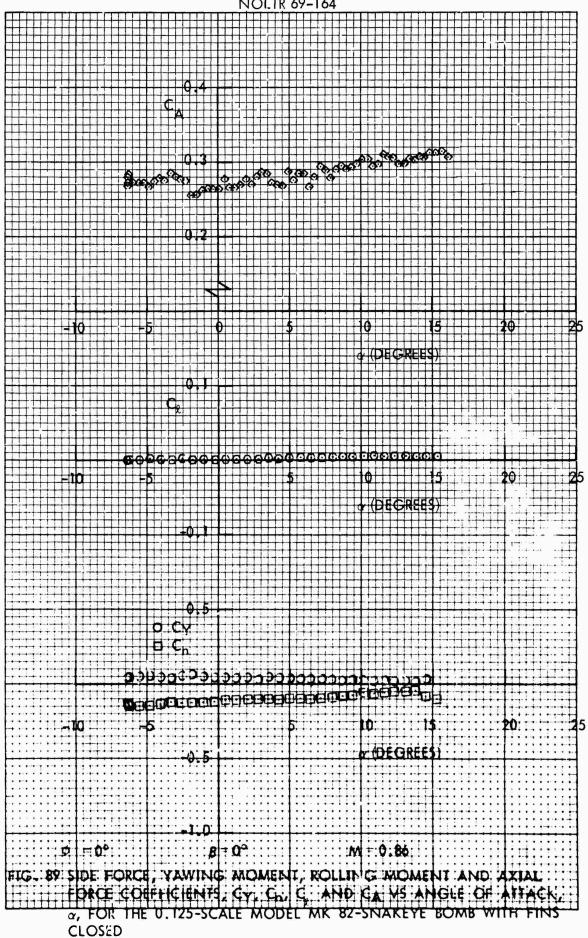




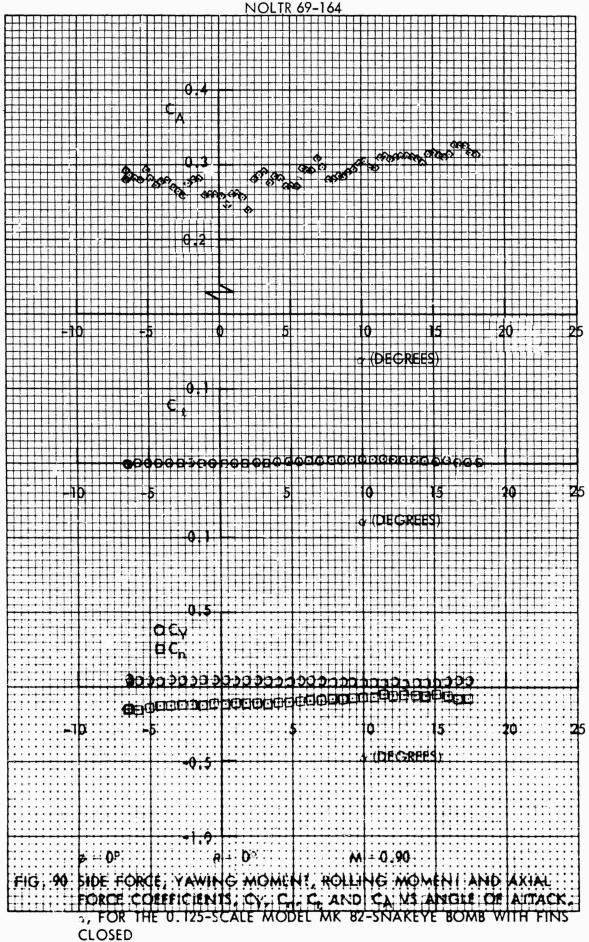


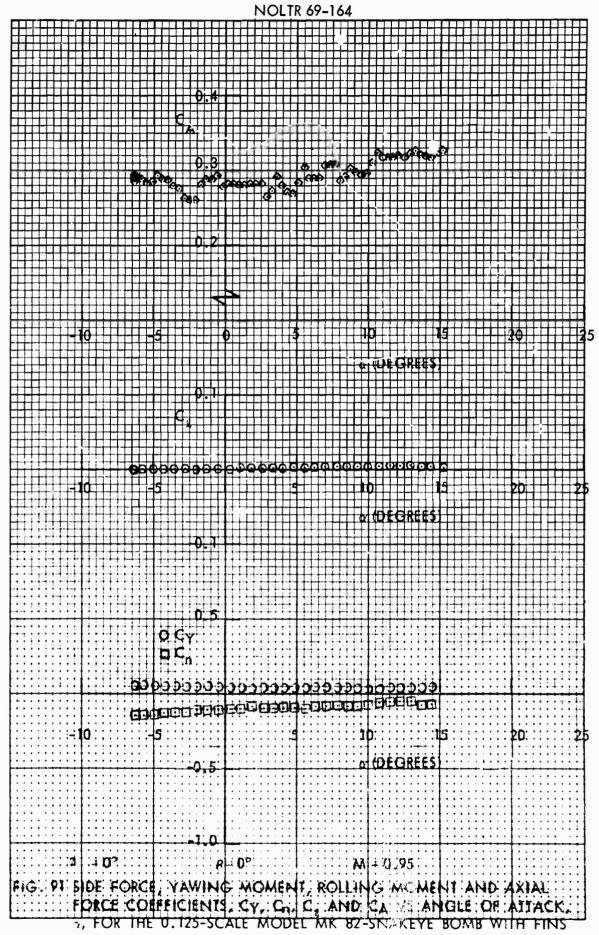






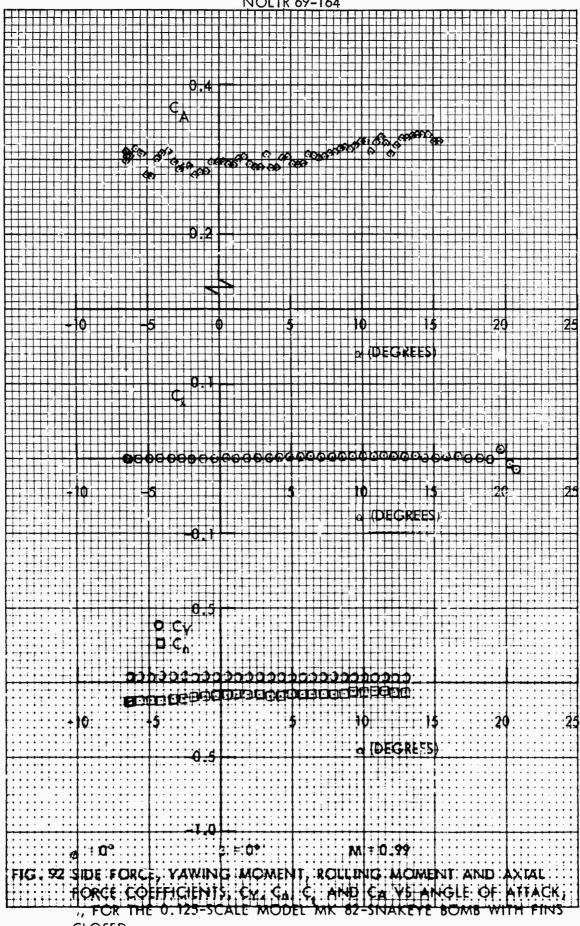


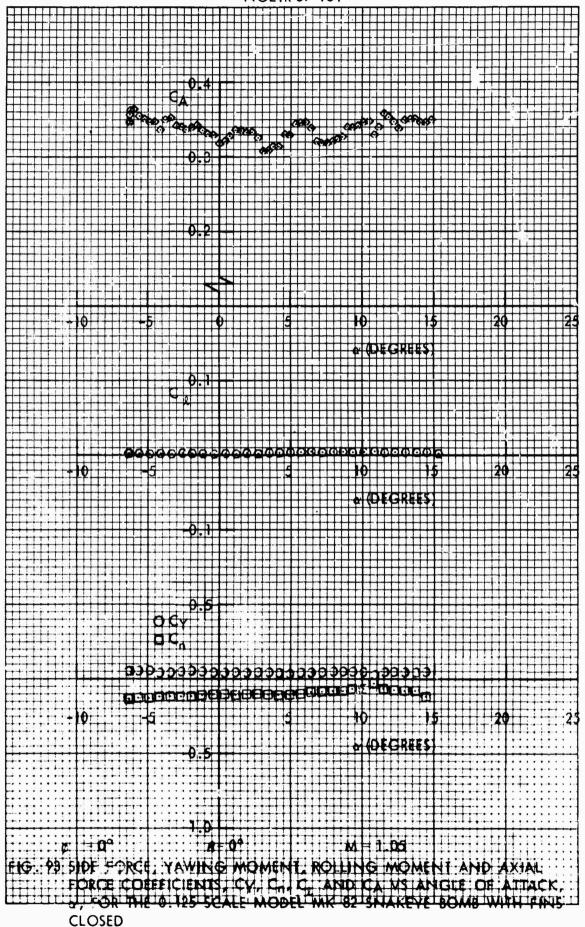


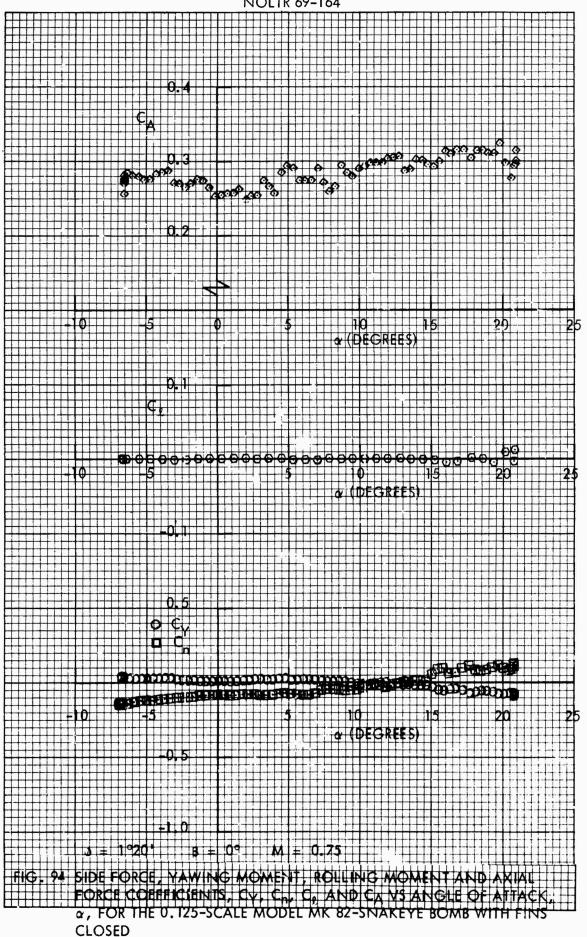


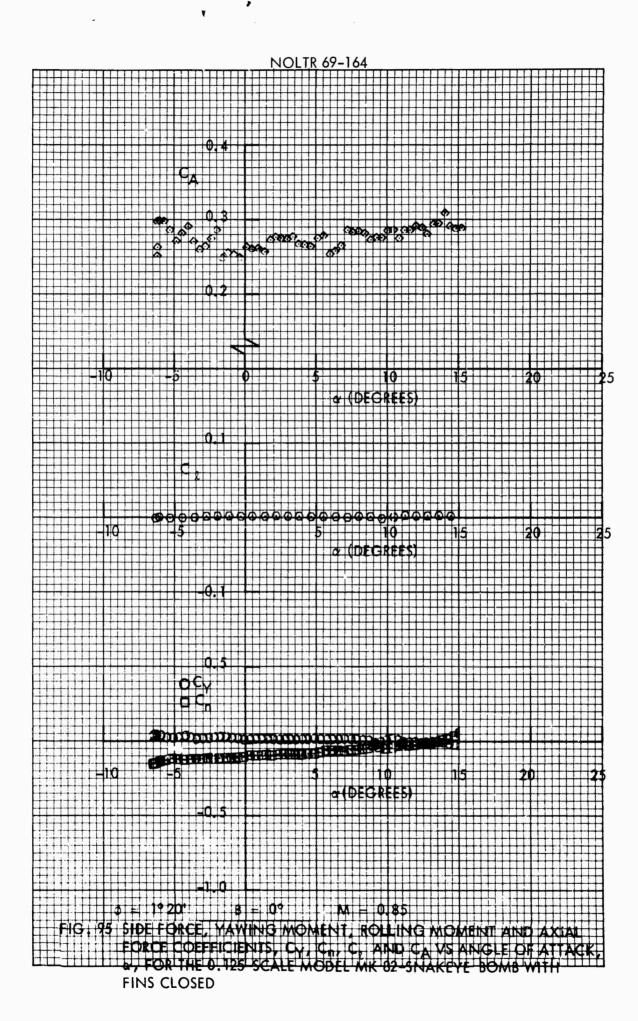
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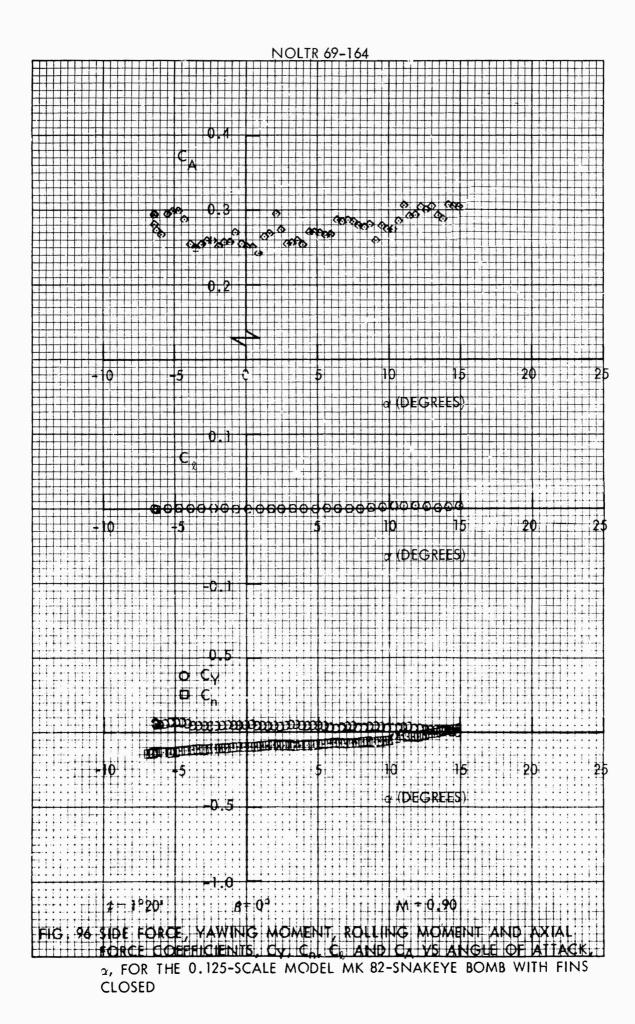
NOLTR 69-164



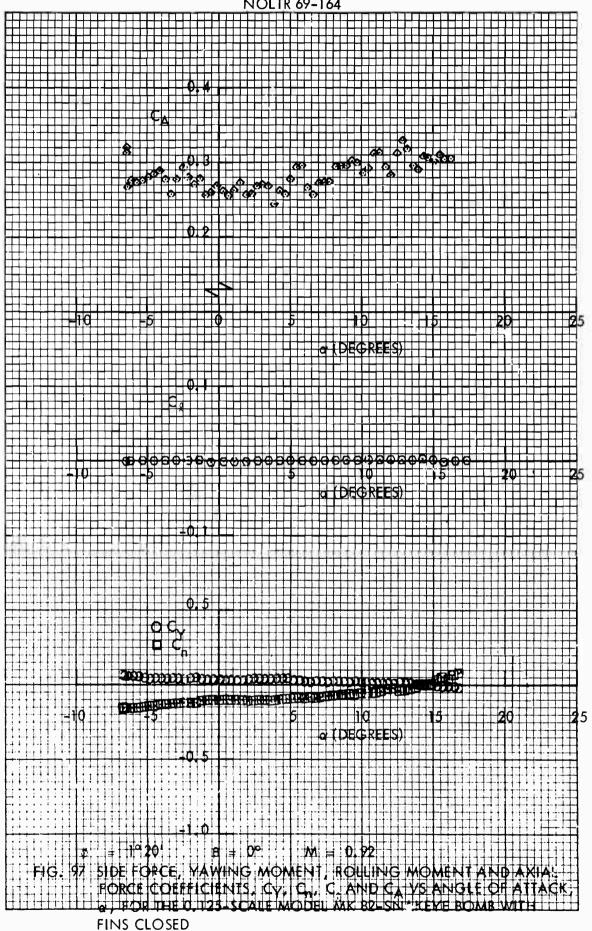


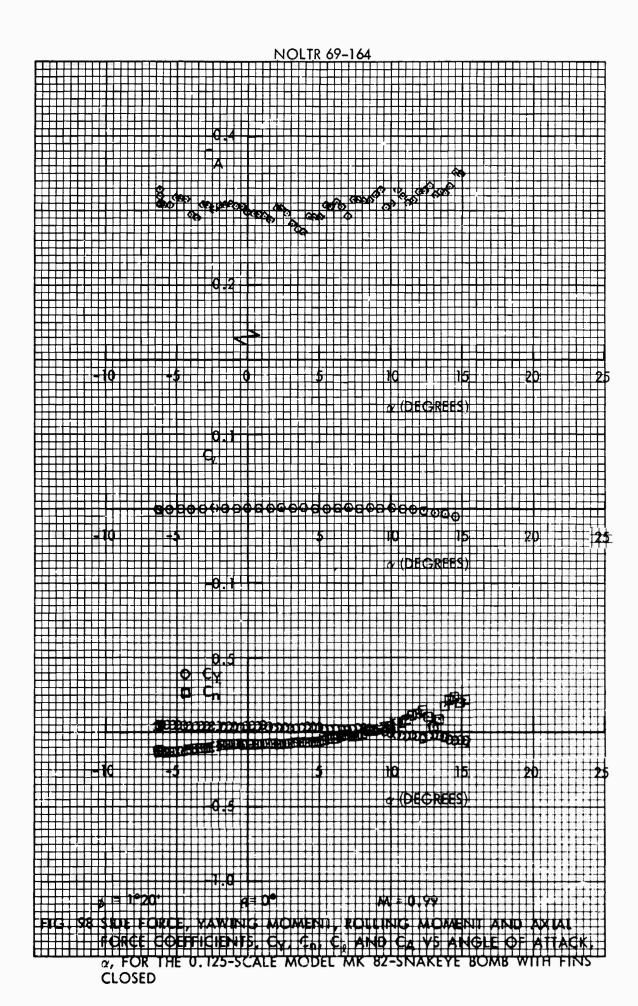


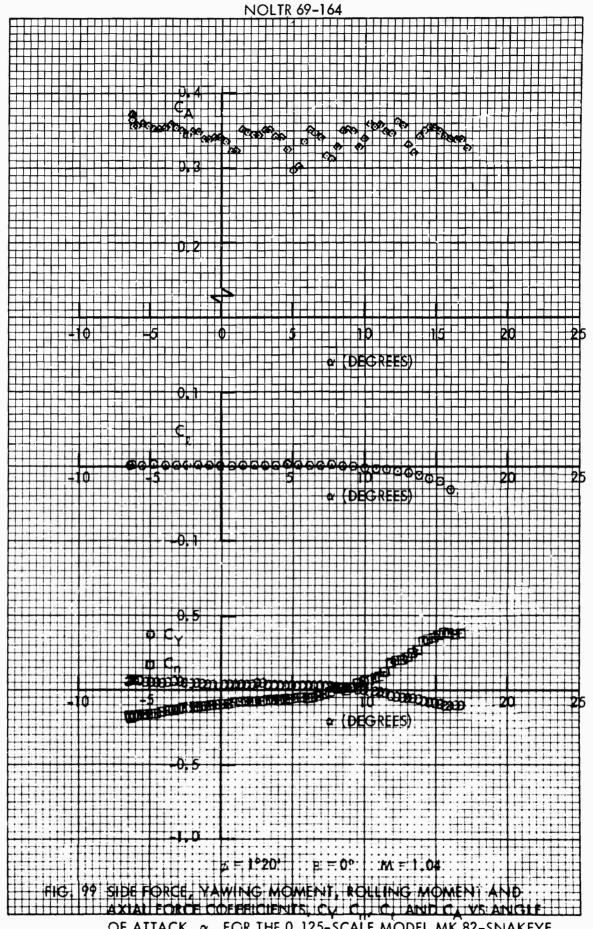






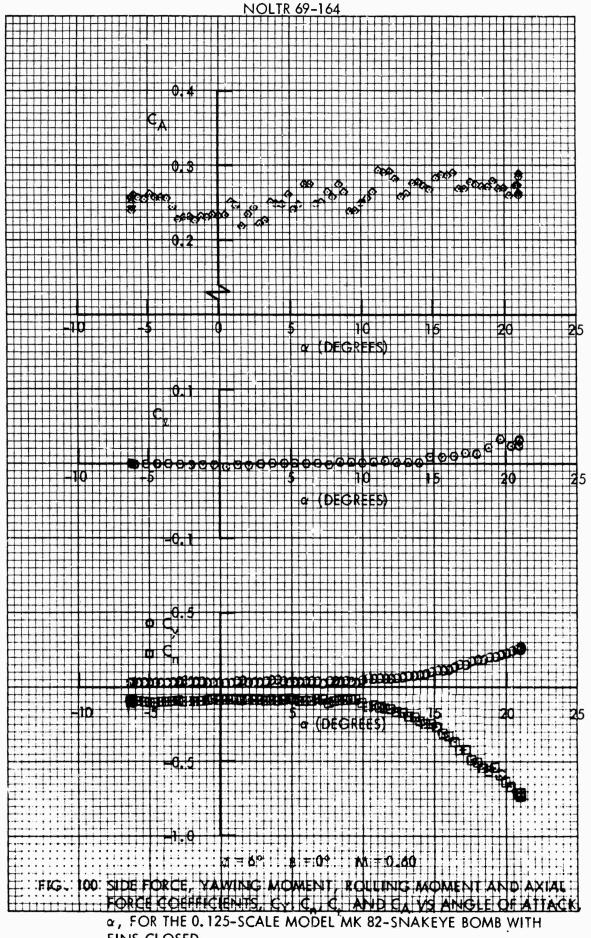




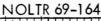


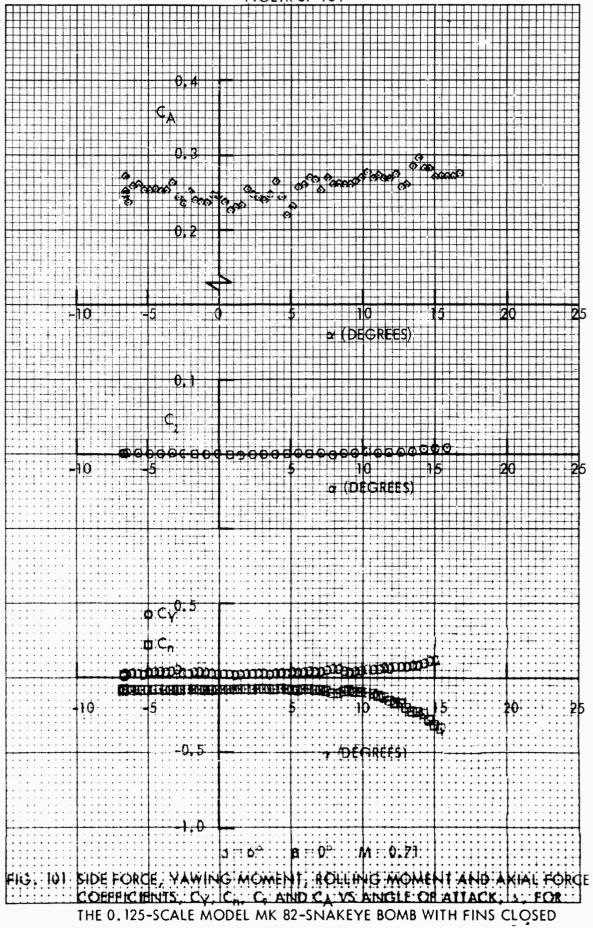
OF ATTACK, &, FOR THE 0. 125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

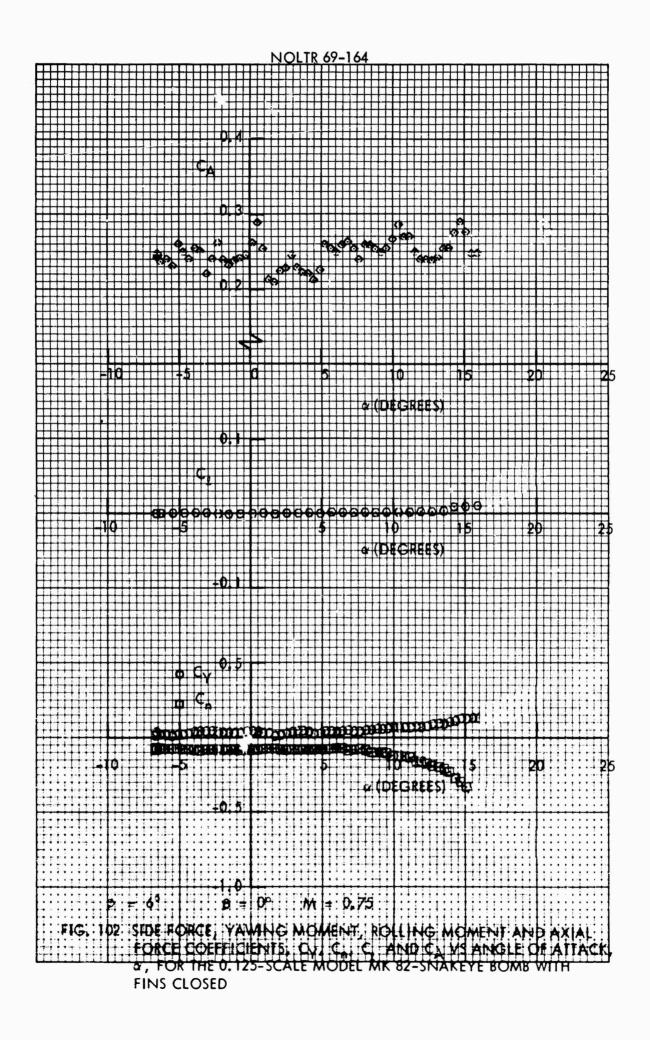


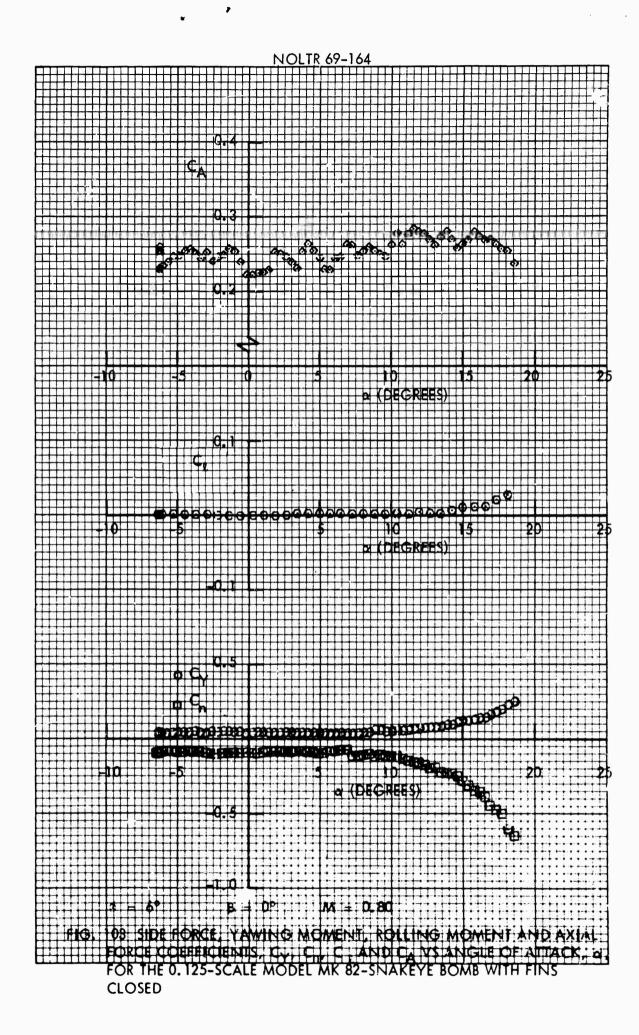


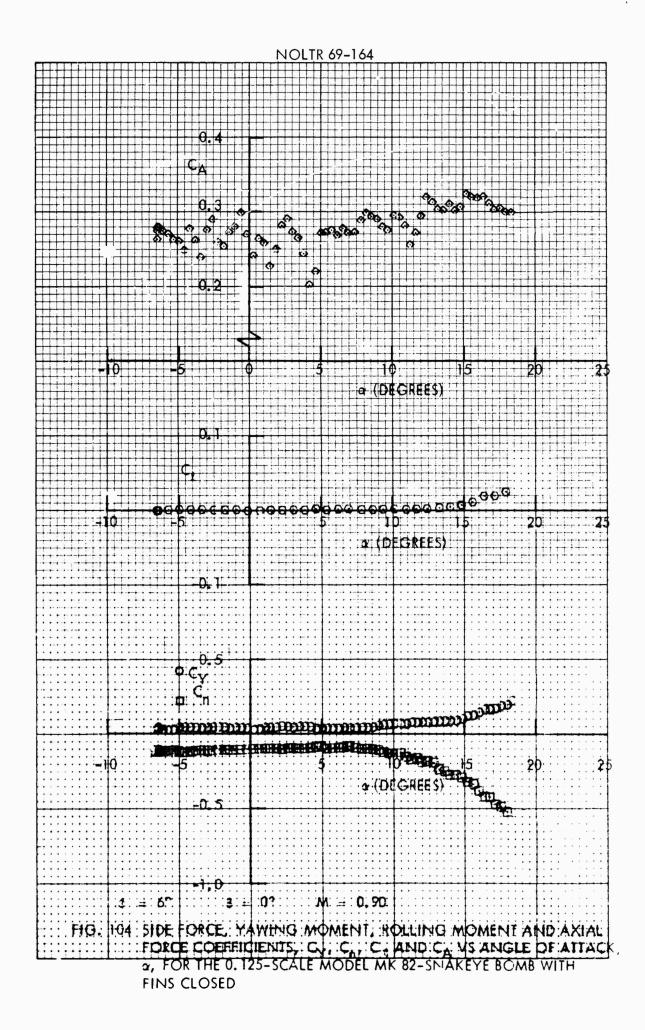
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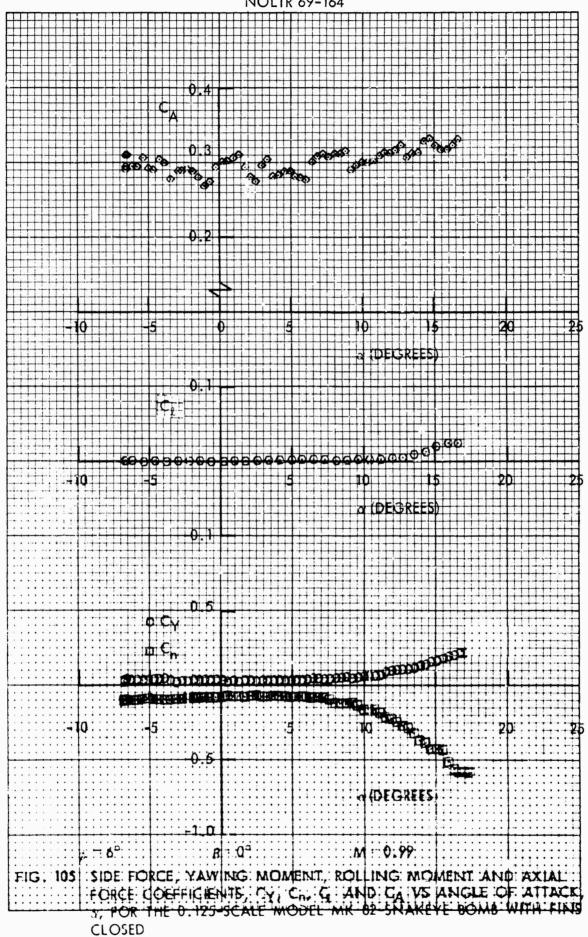




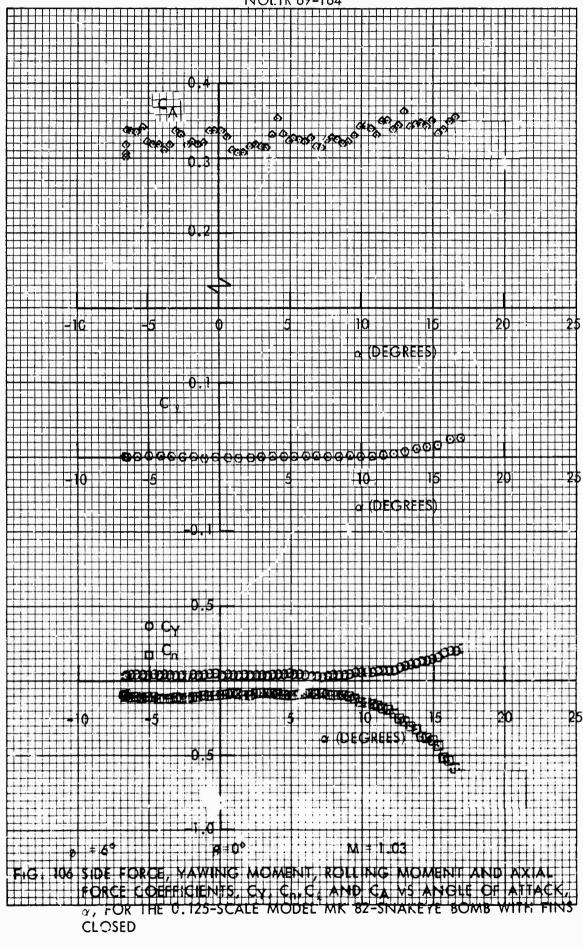


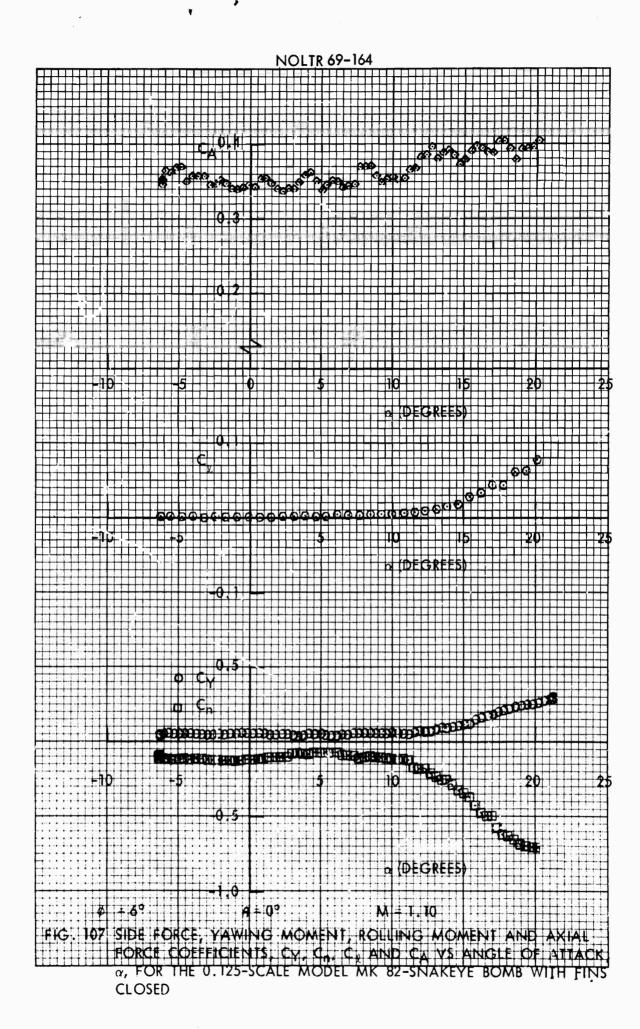


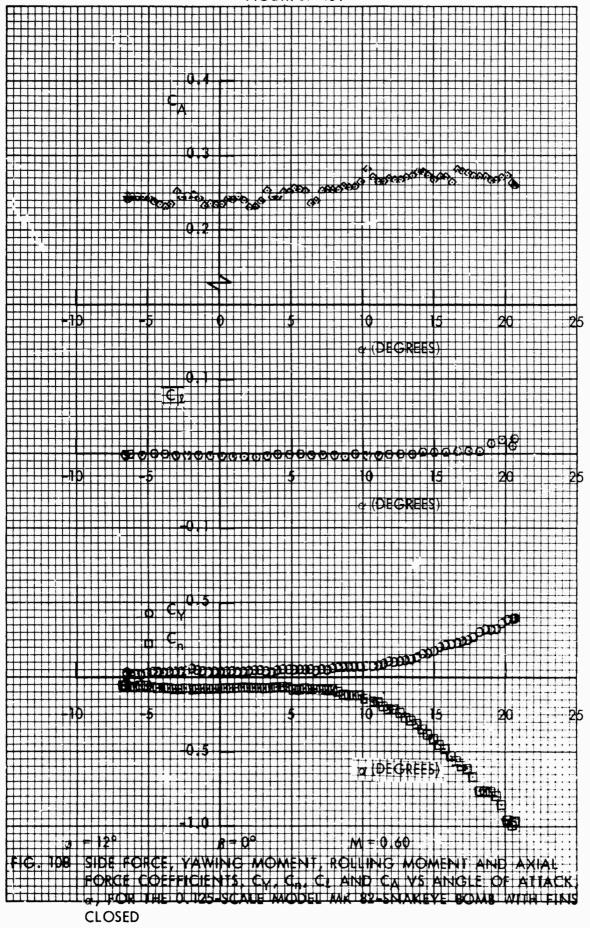


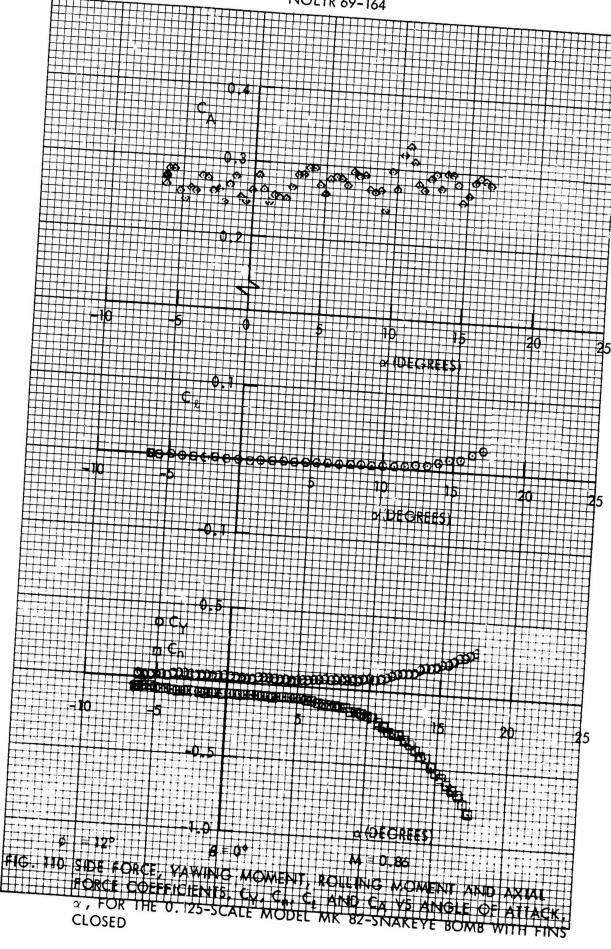


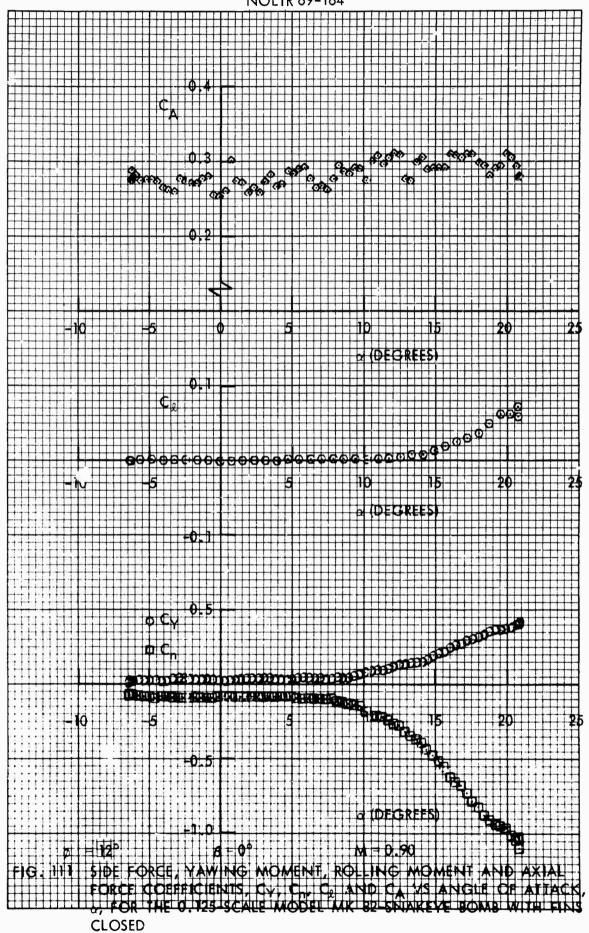


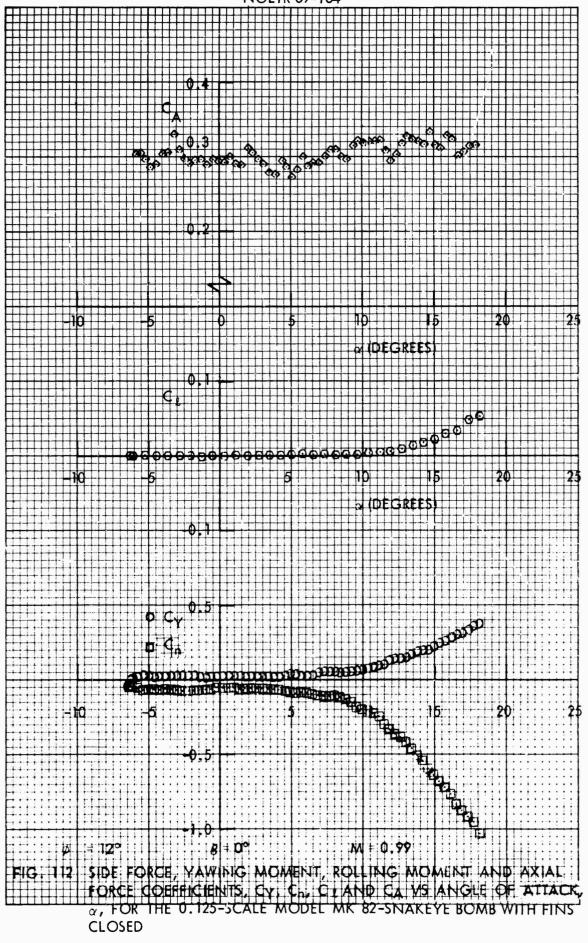


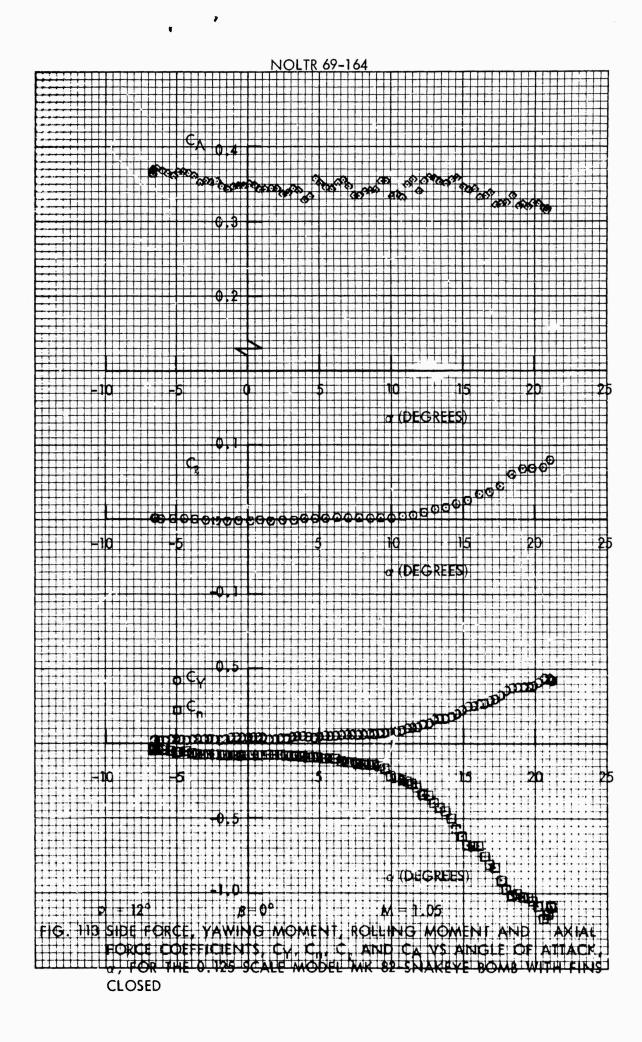


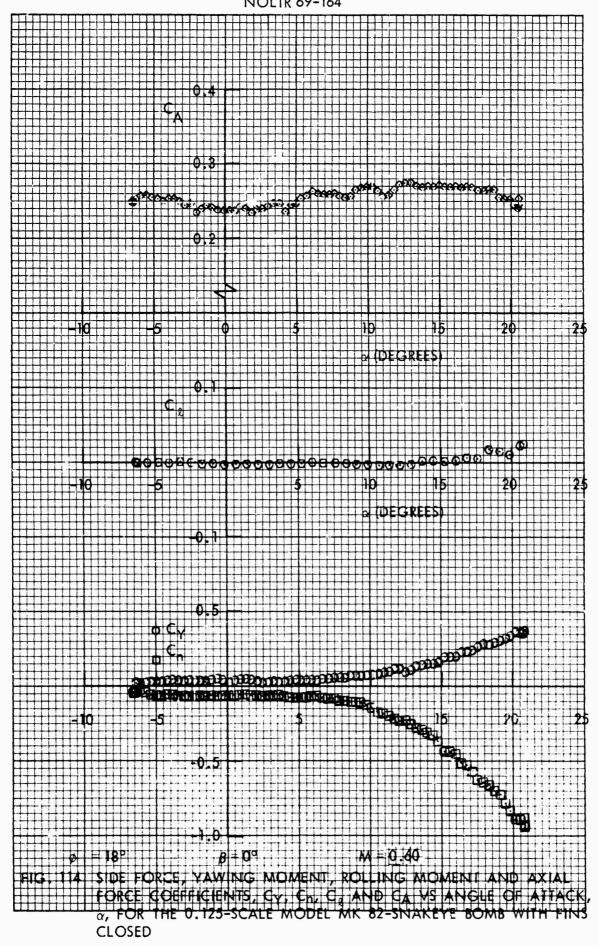


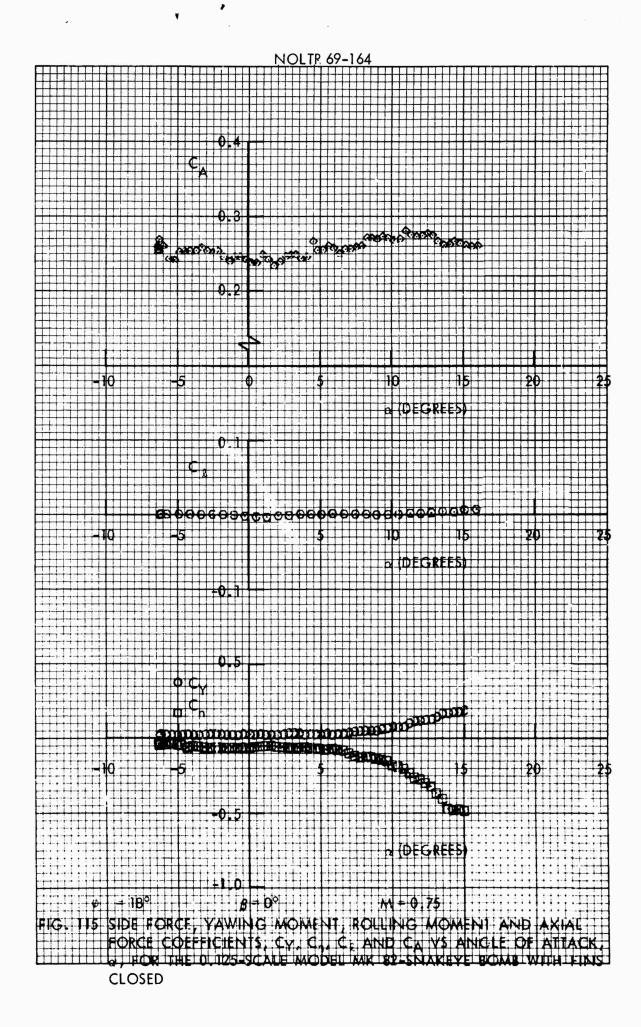


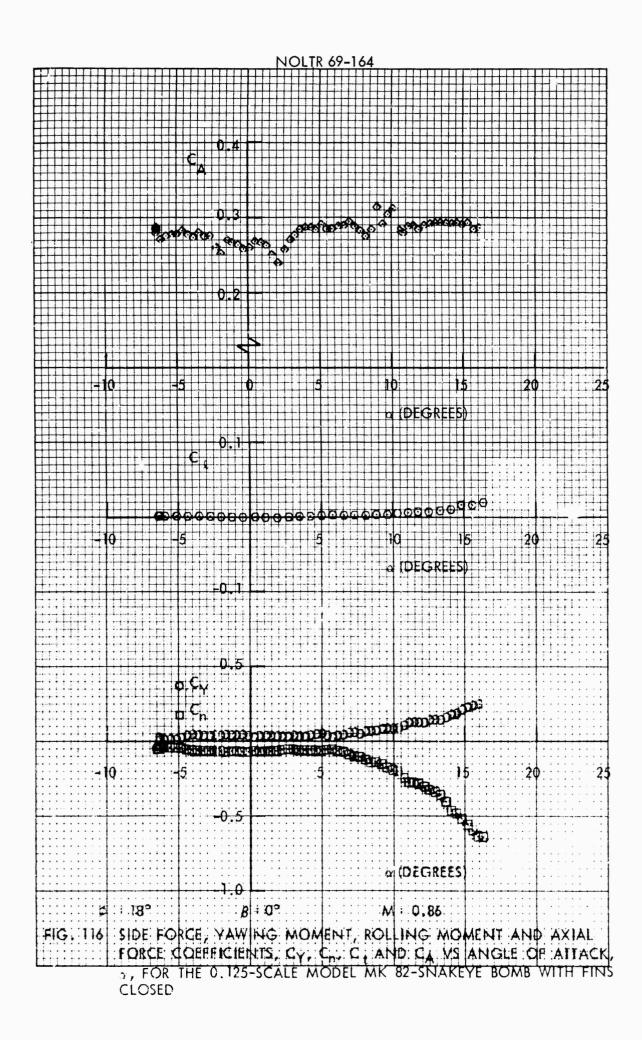


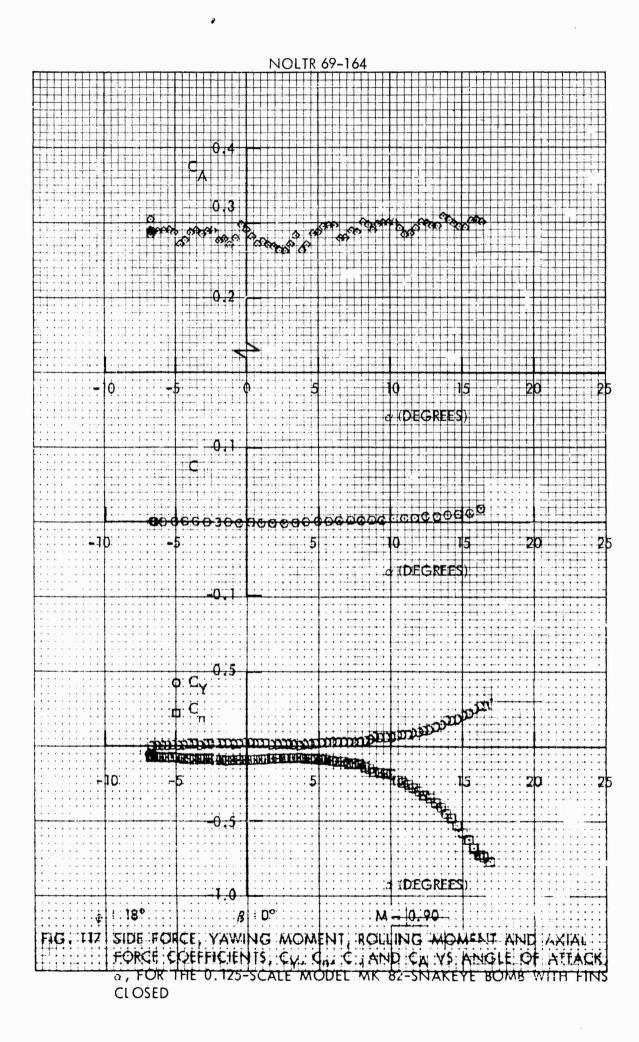


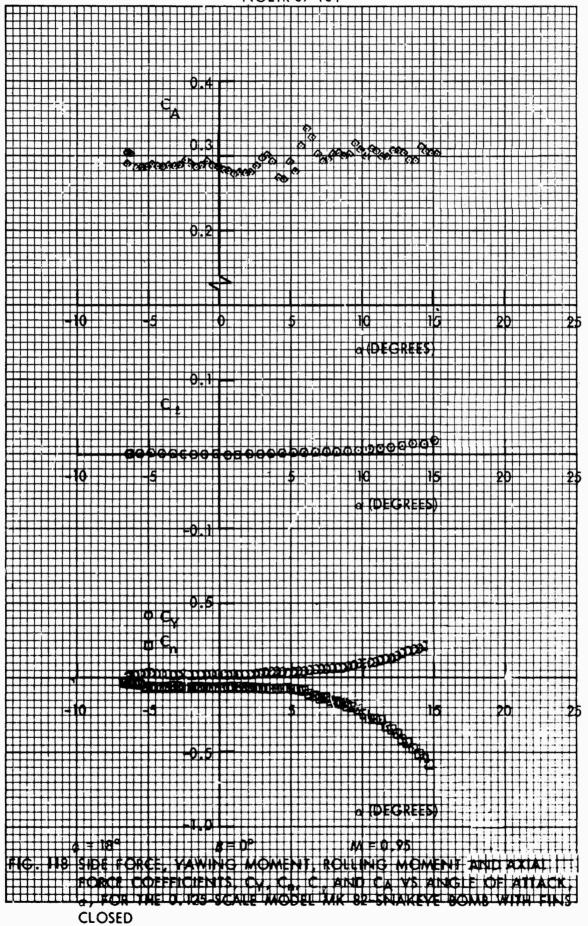


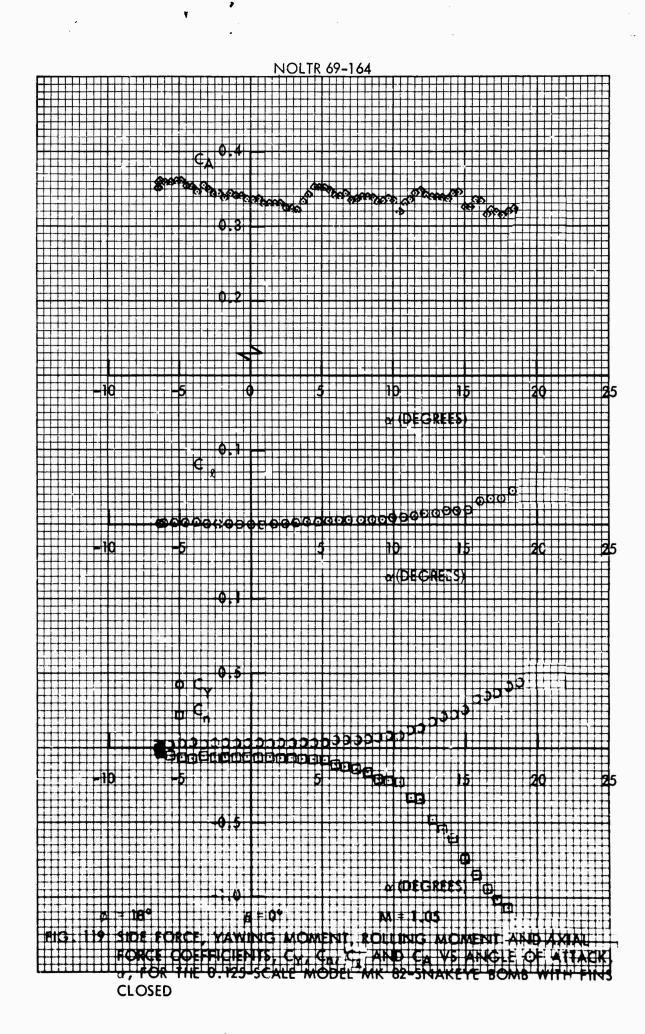




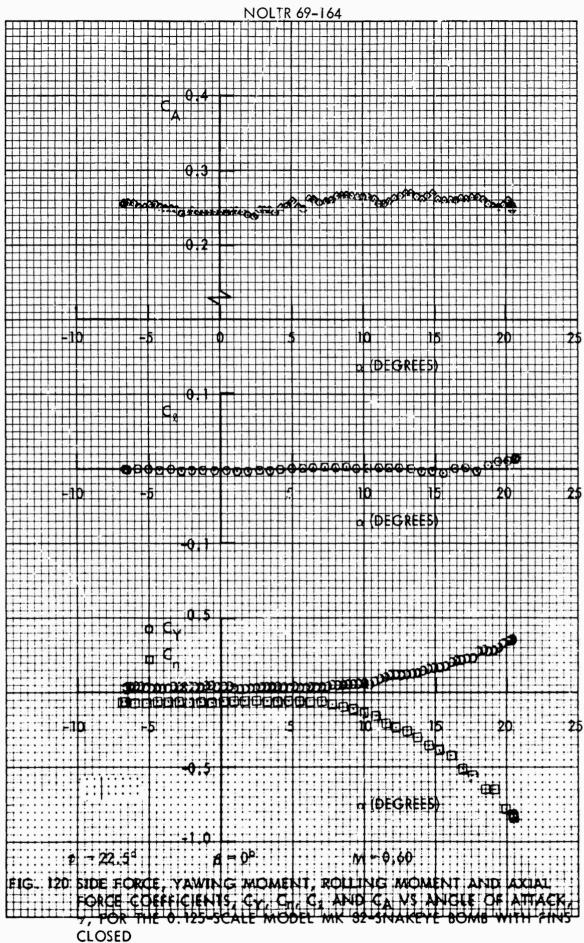


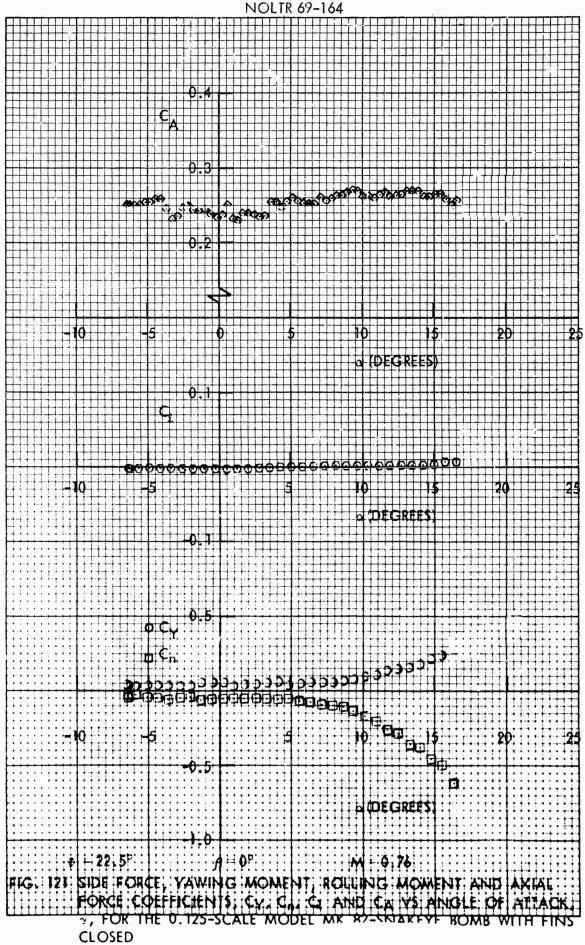




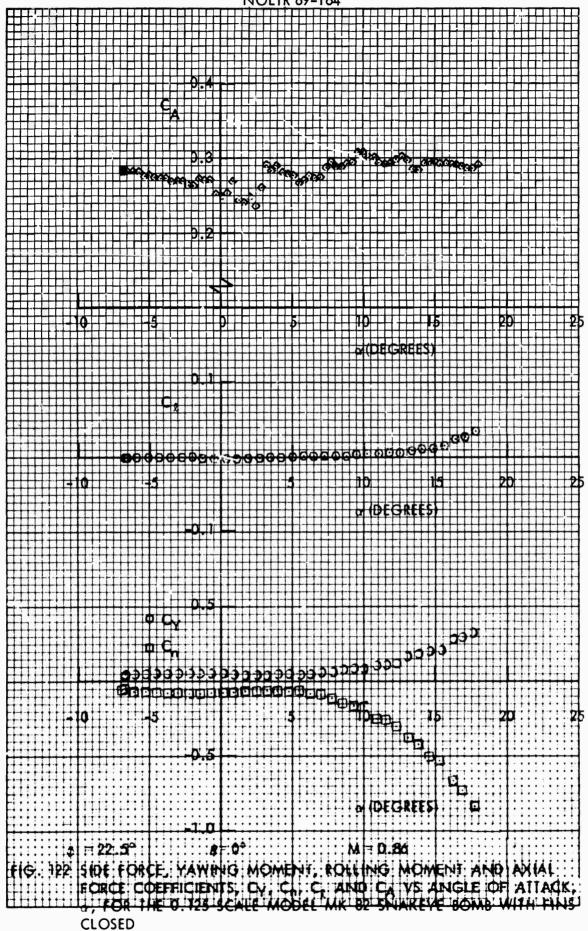


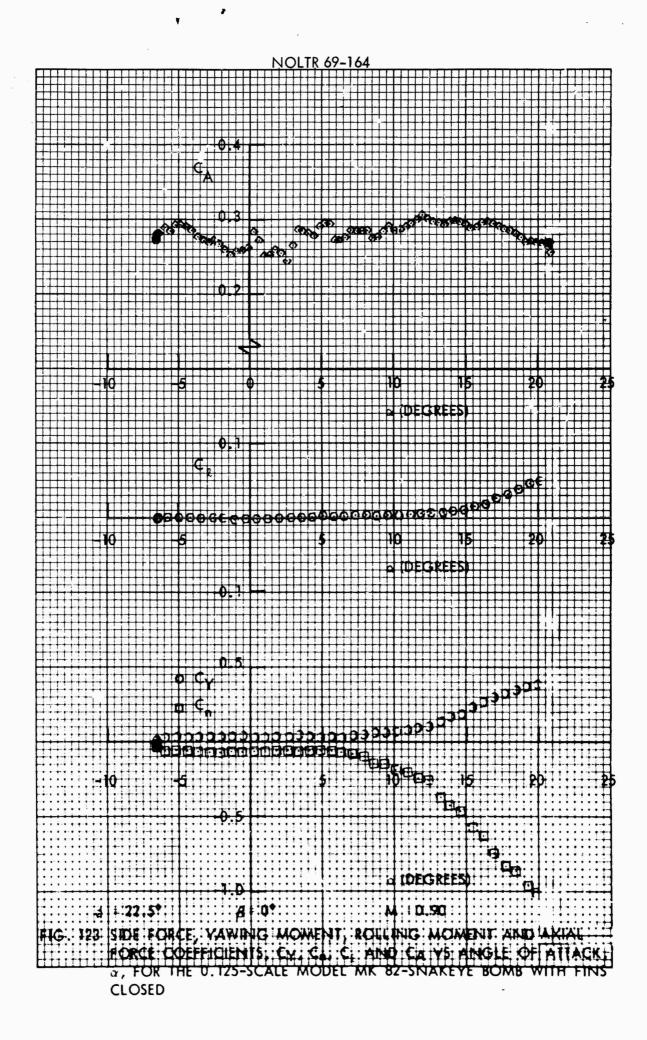




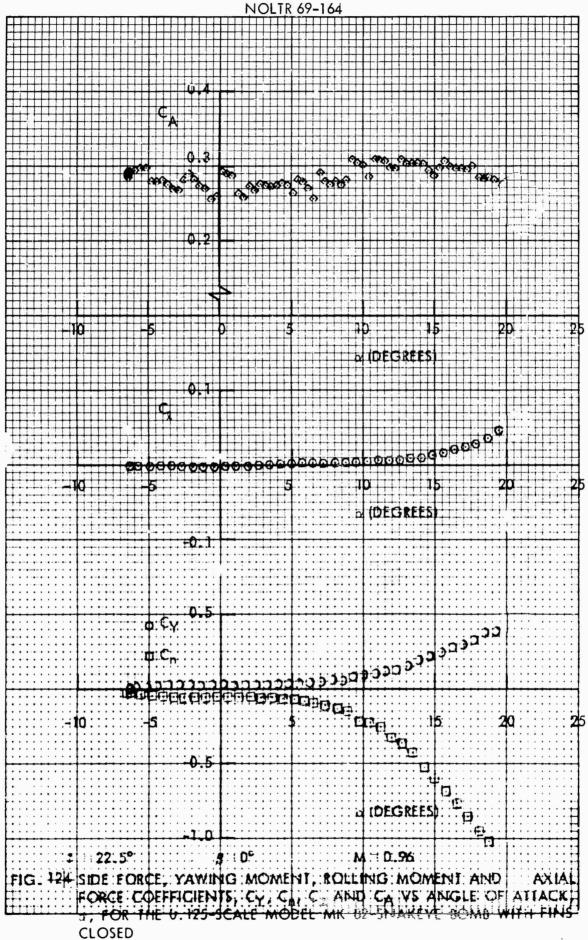


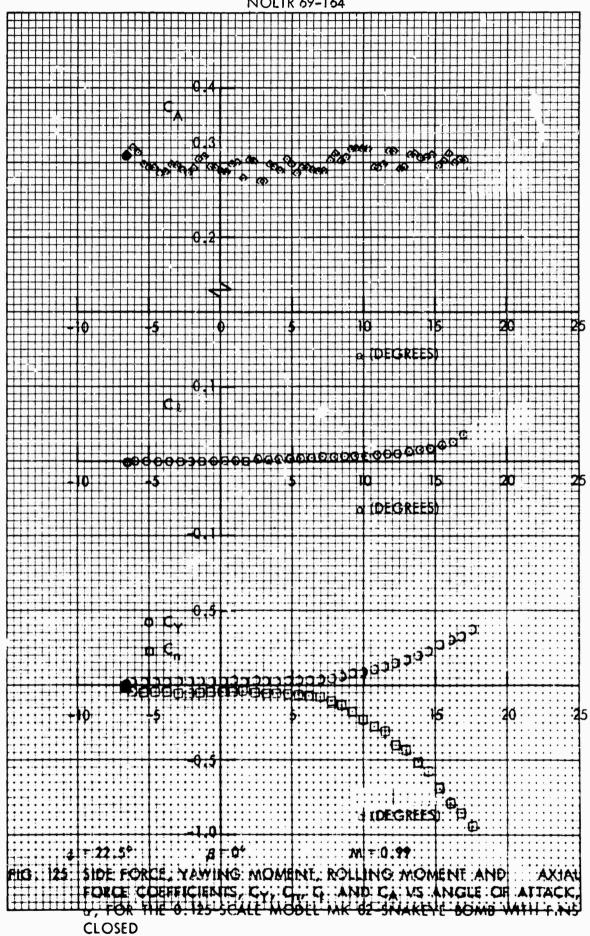


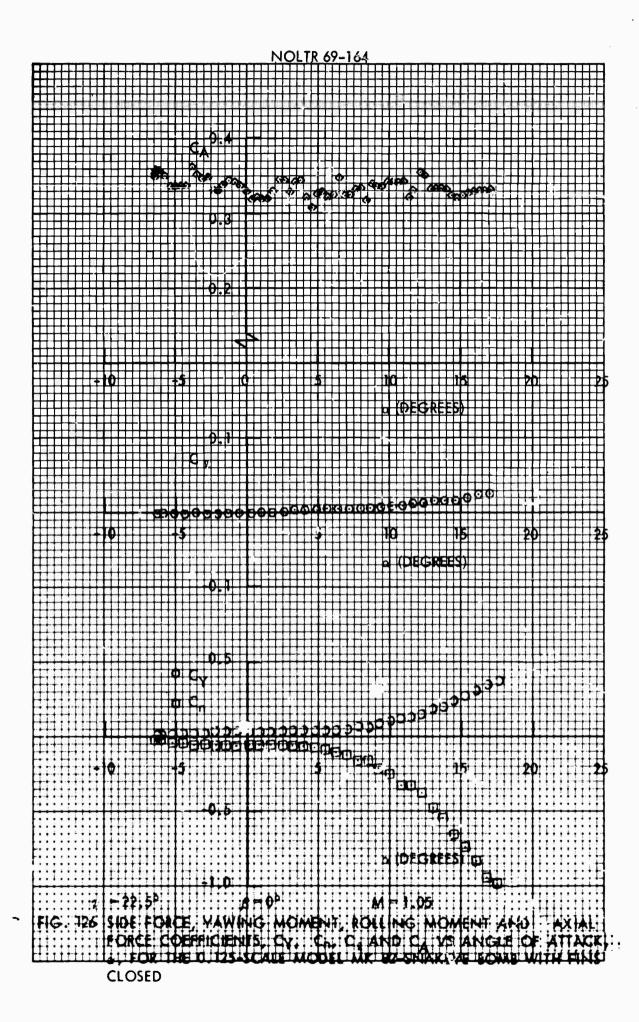




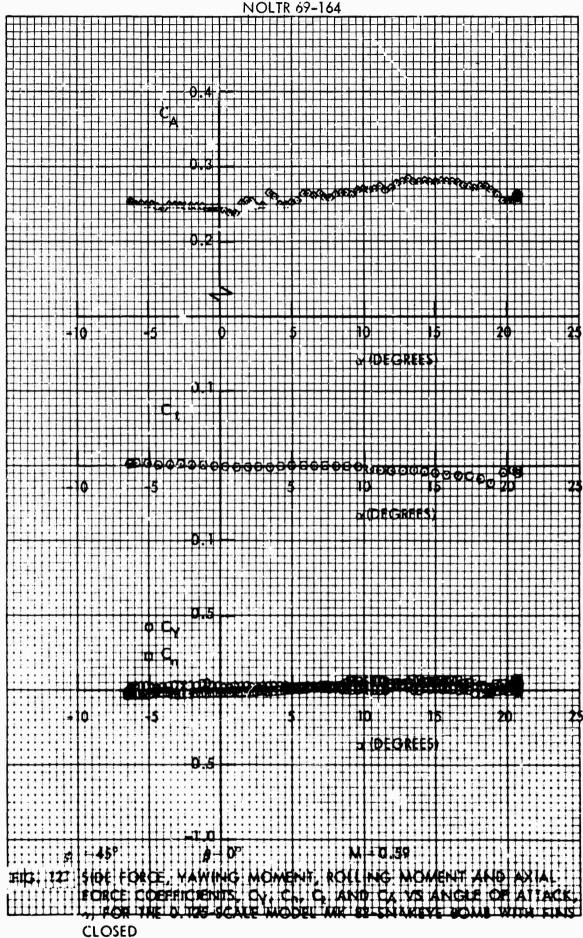




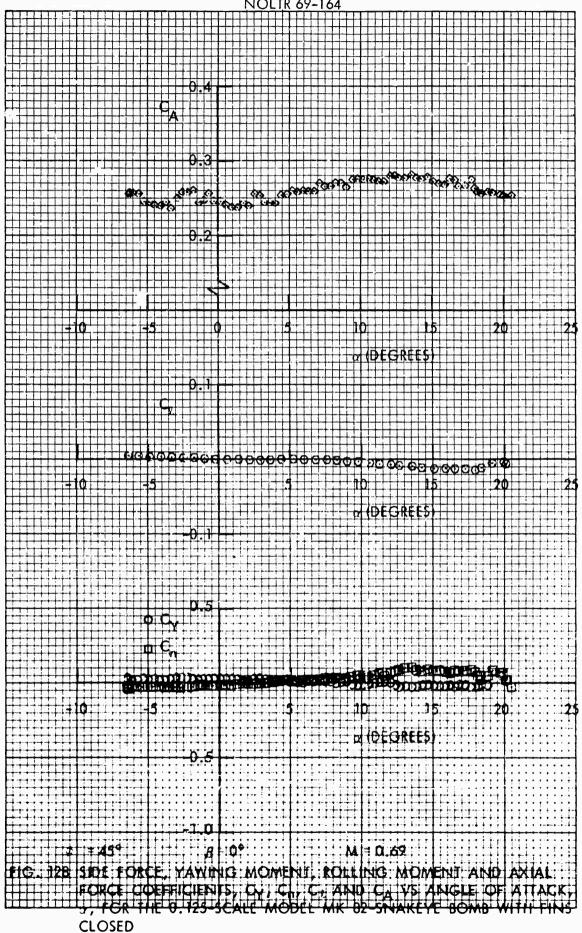


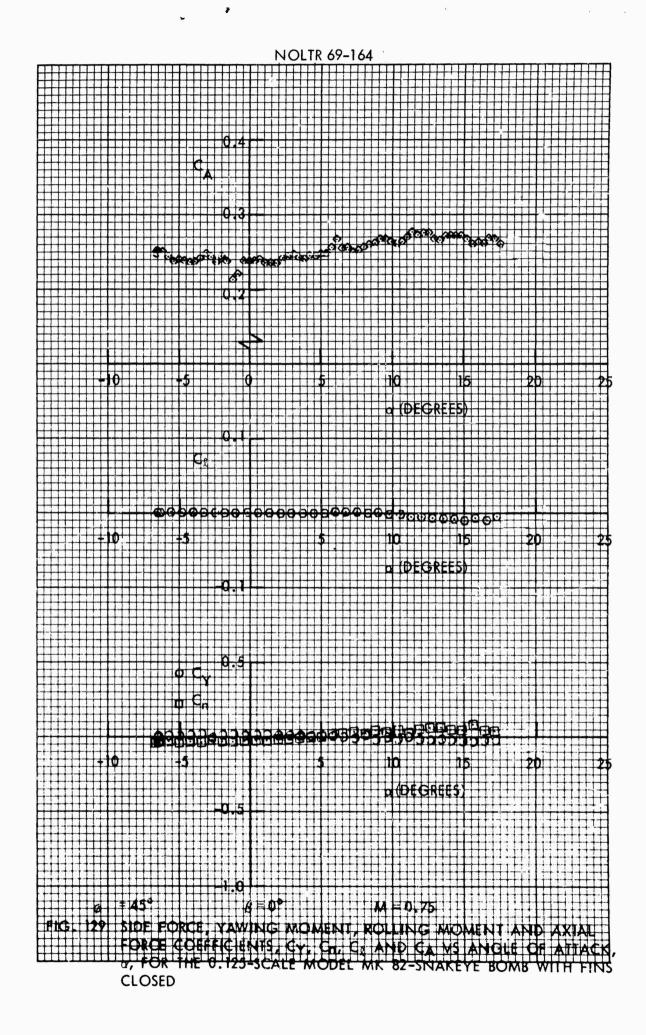


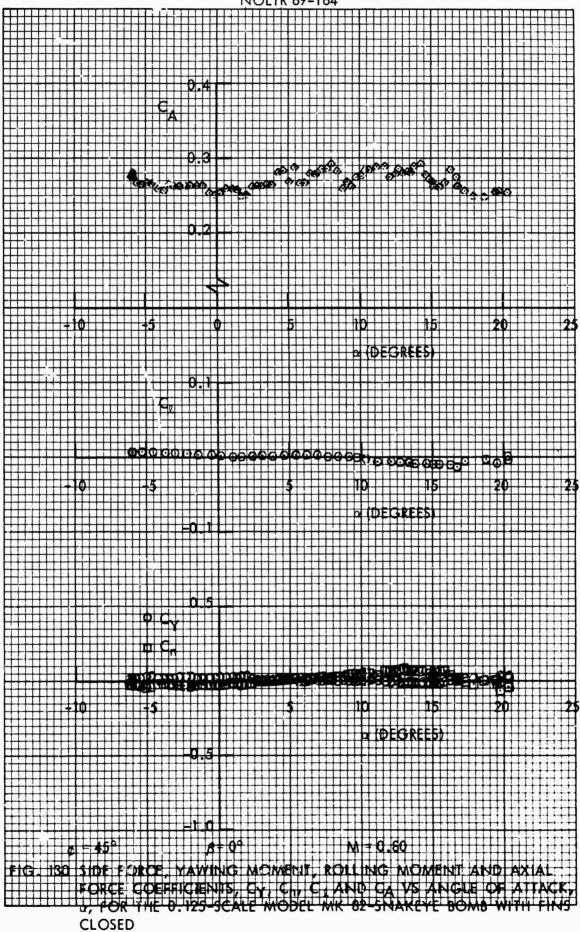




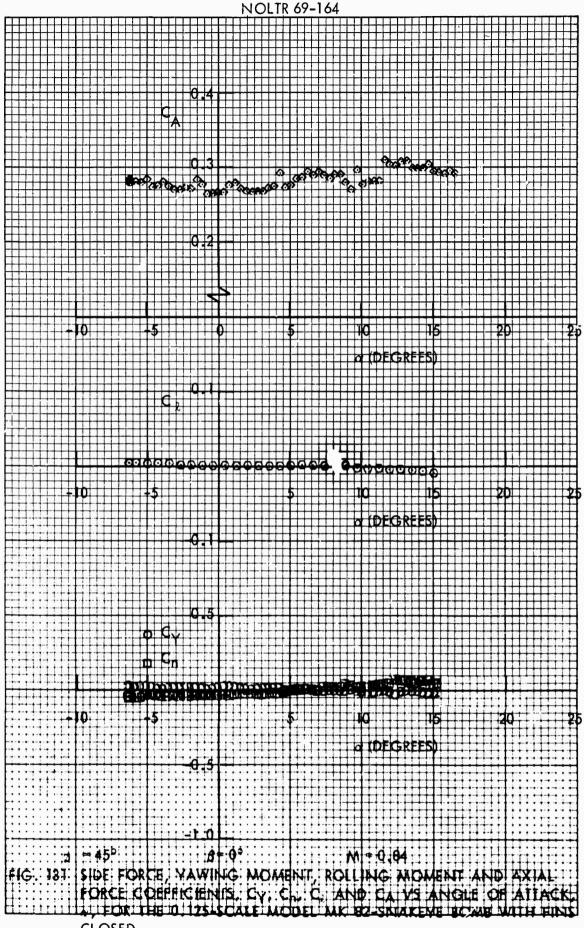


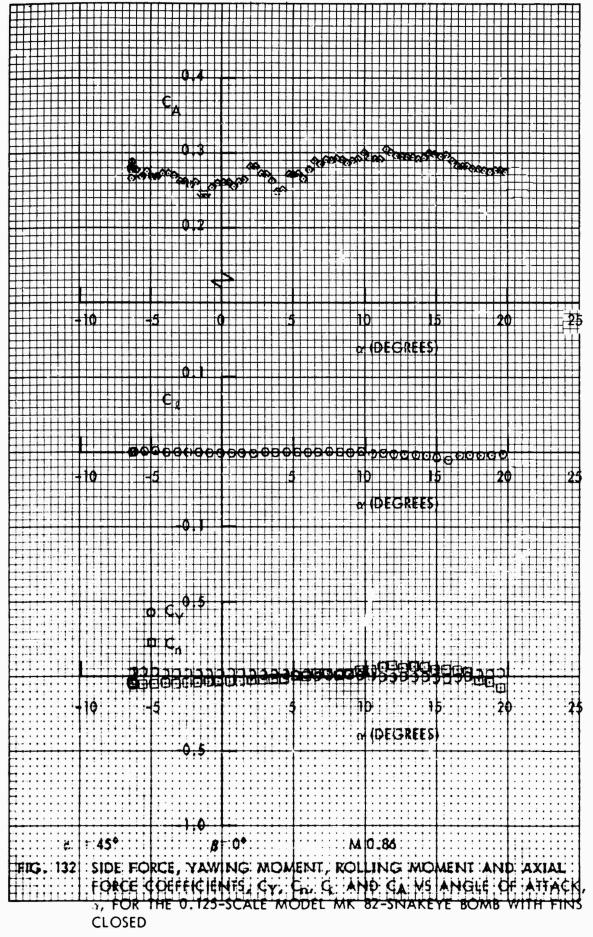




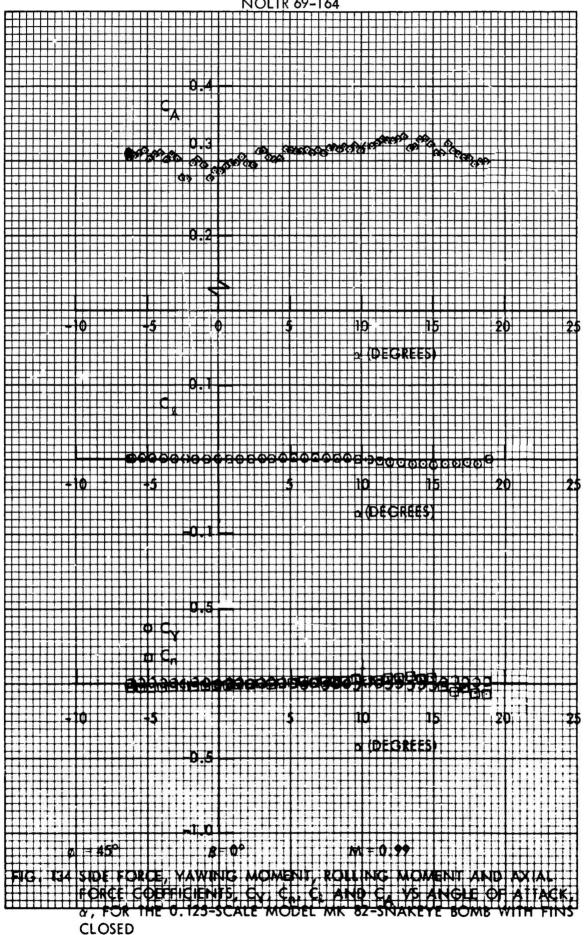






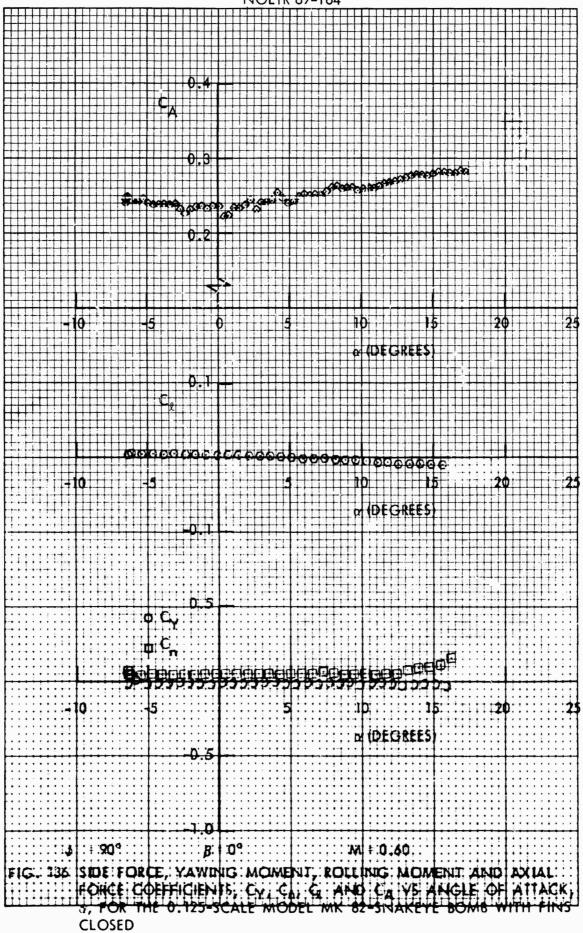


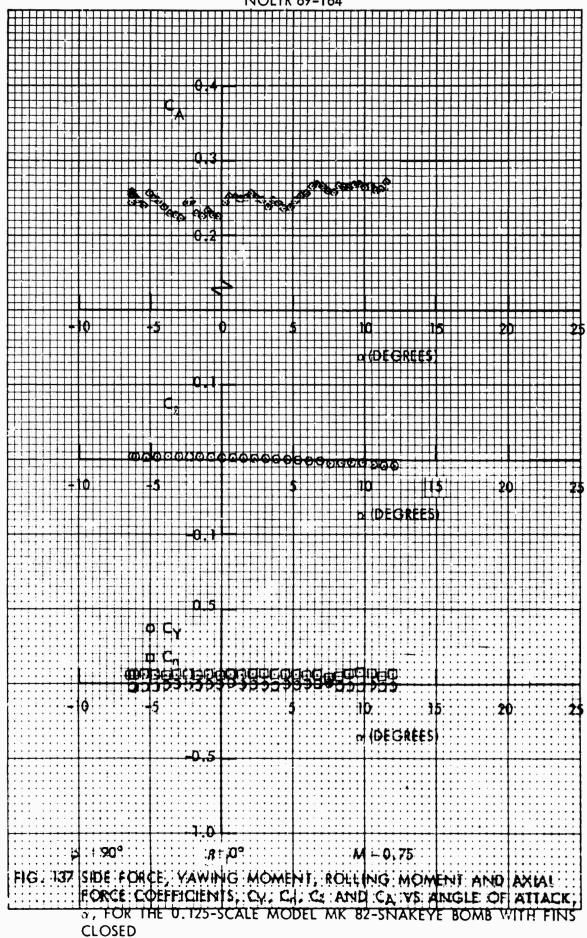


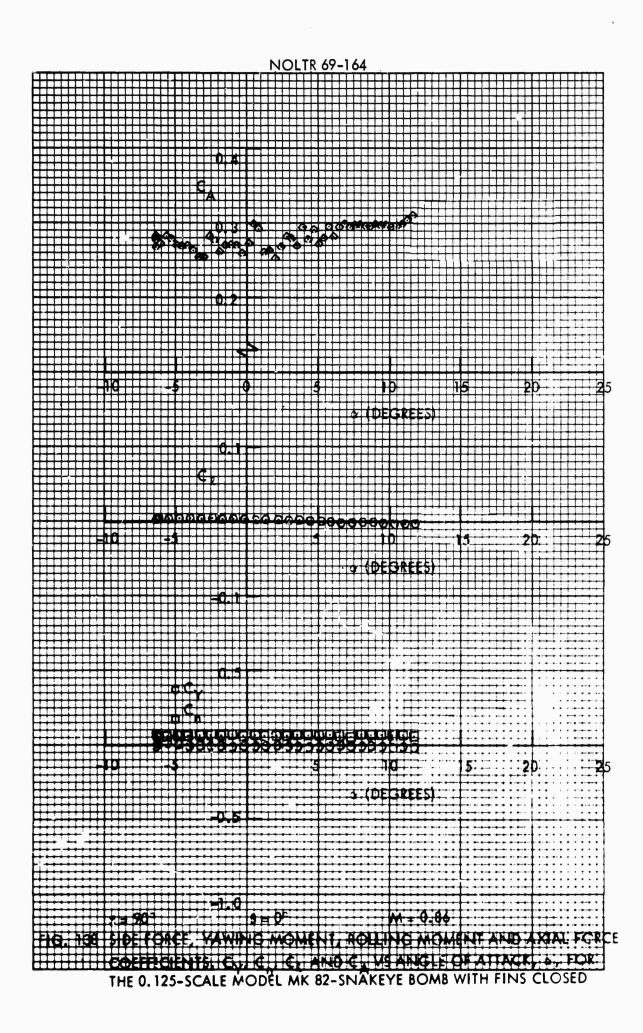


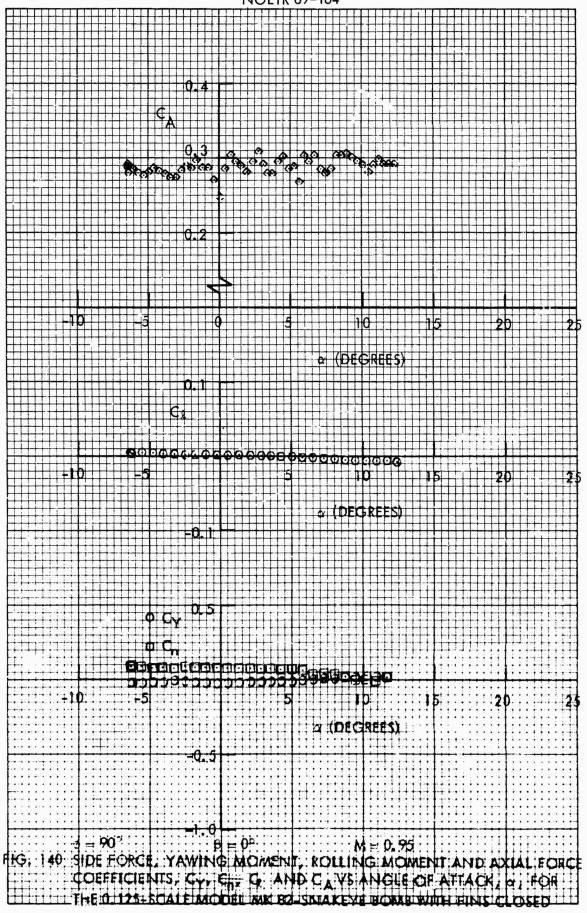
** FOR THE 0. 125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

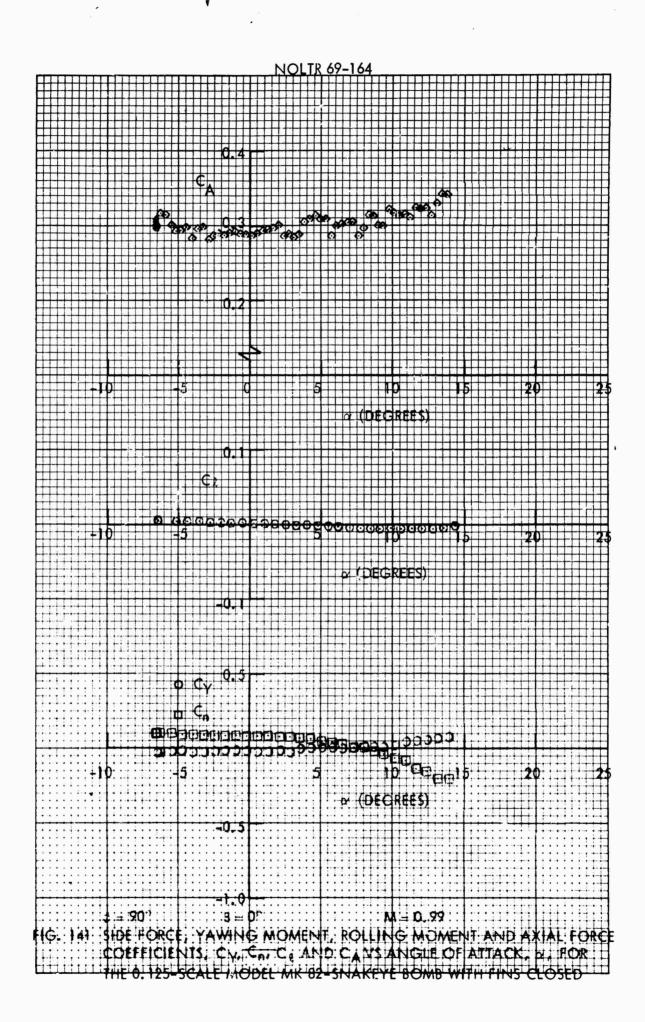


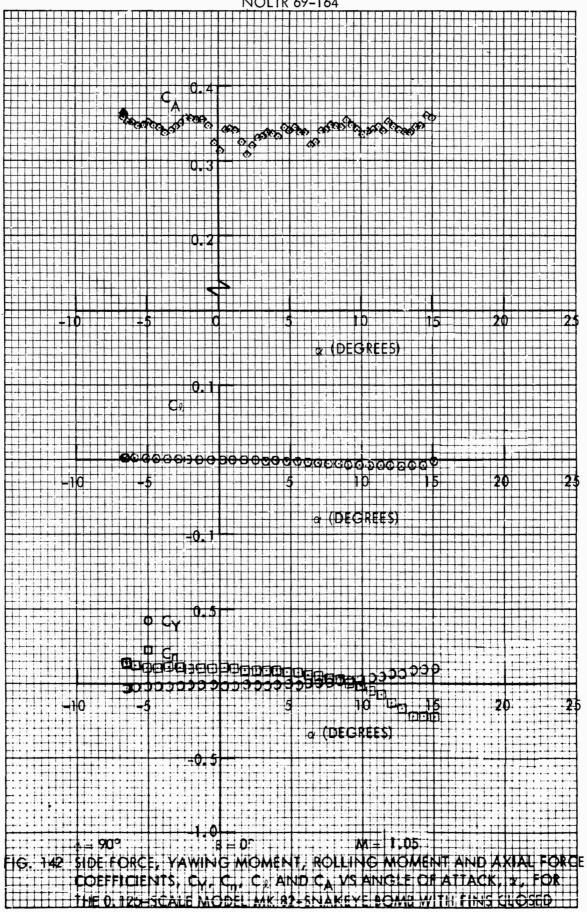


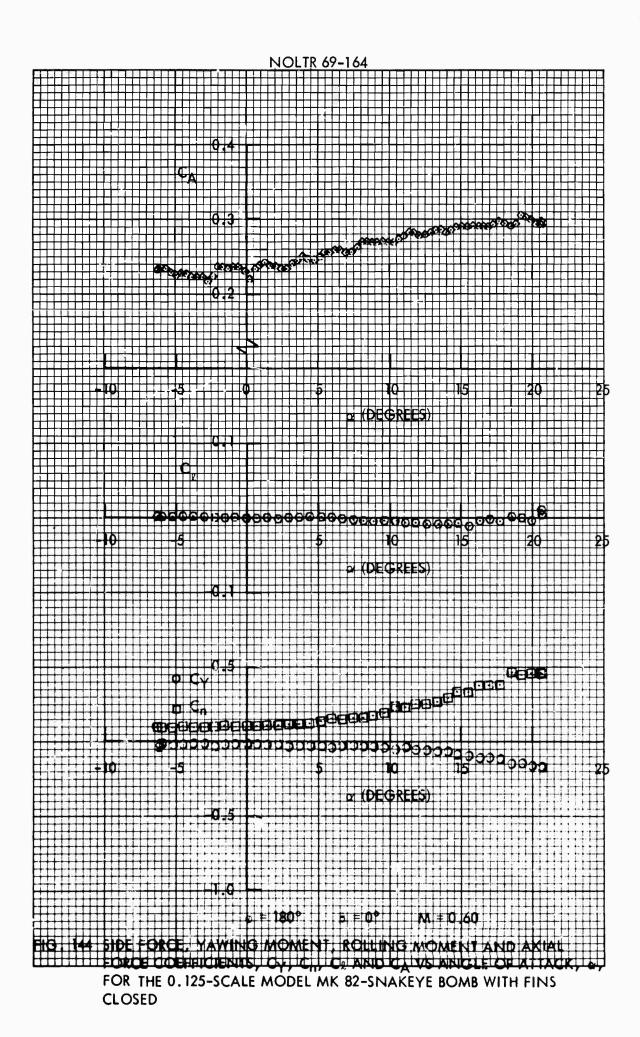


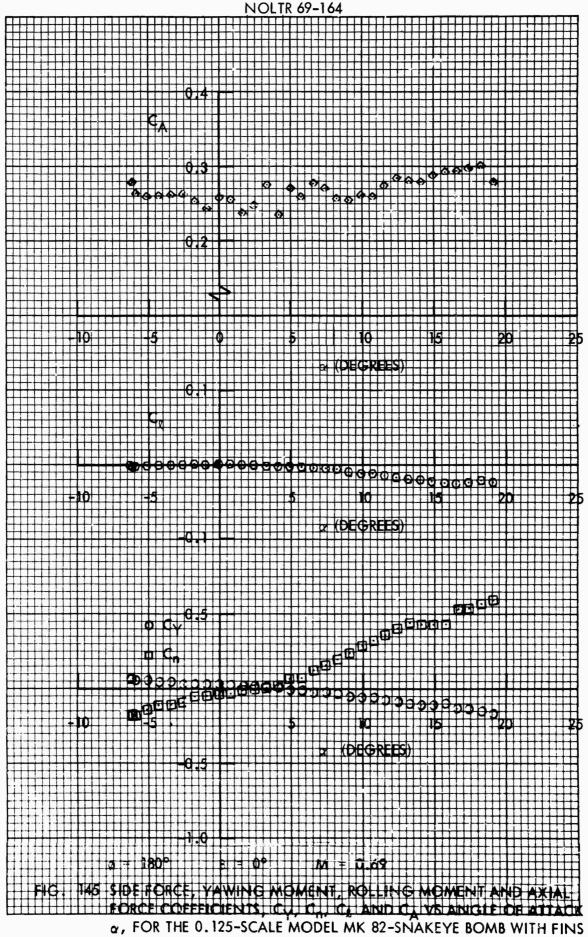




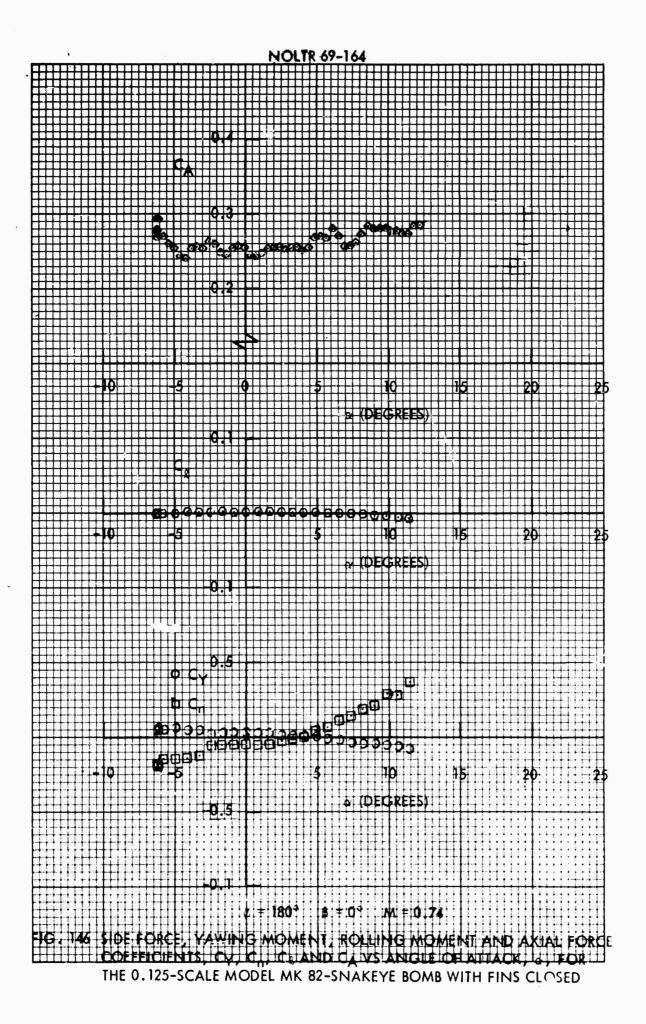


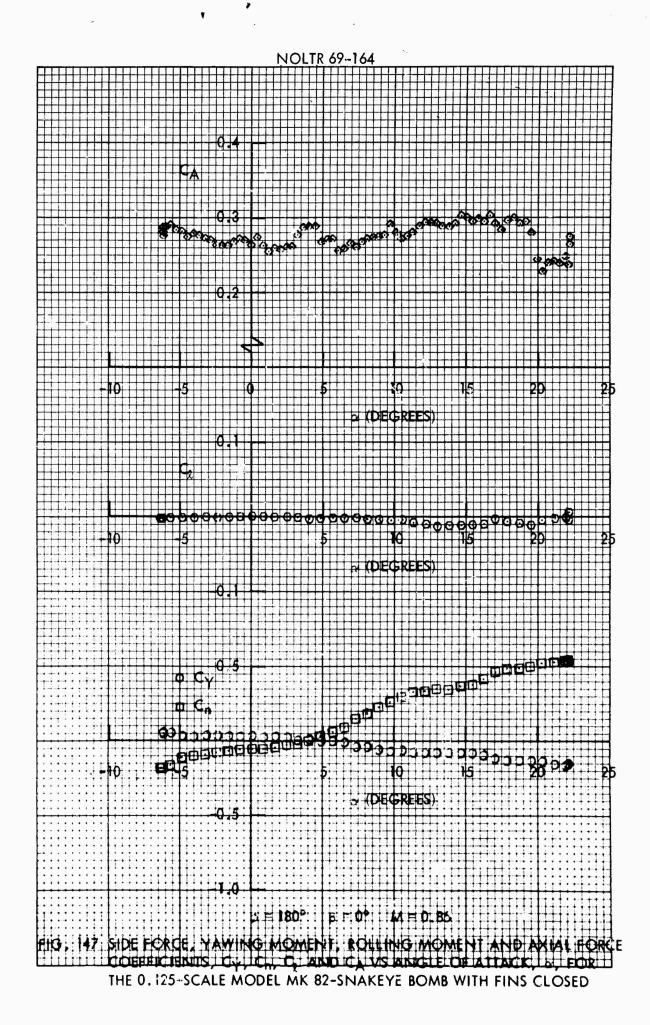


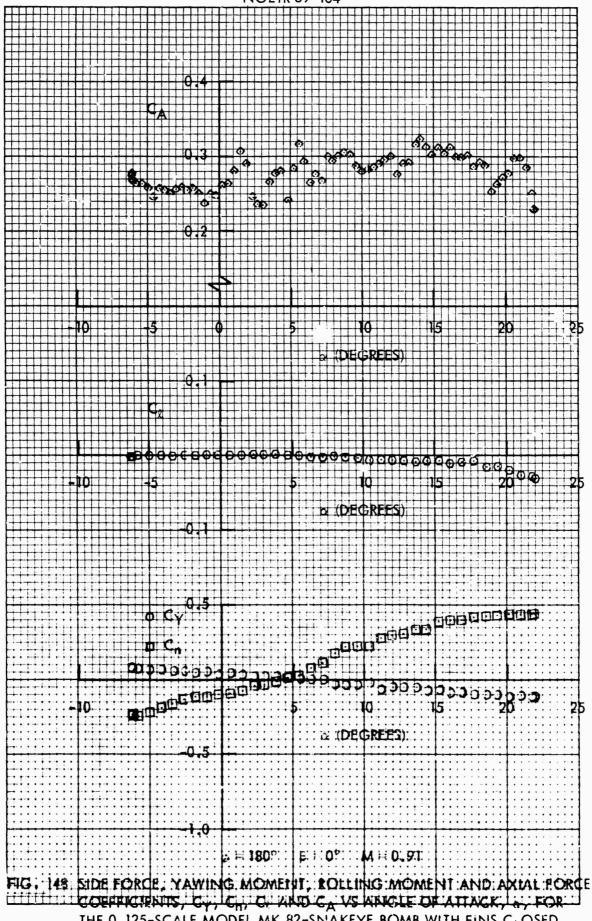




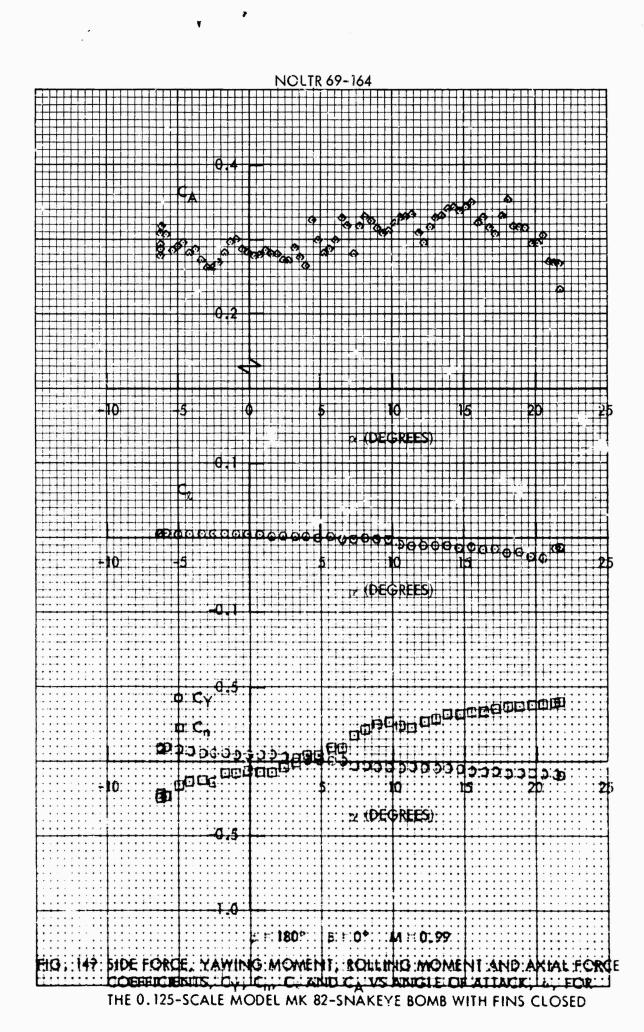
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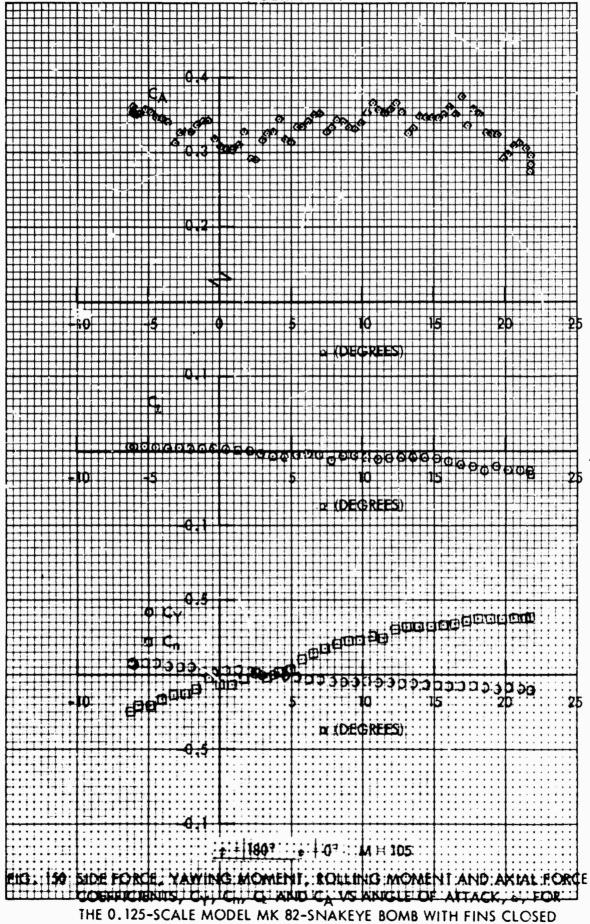


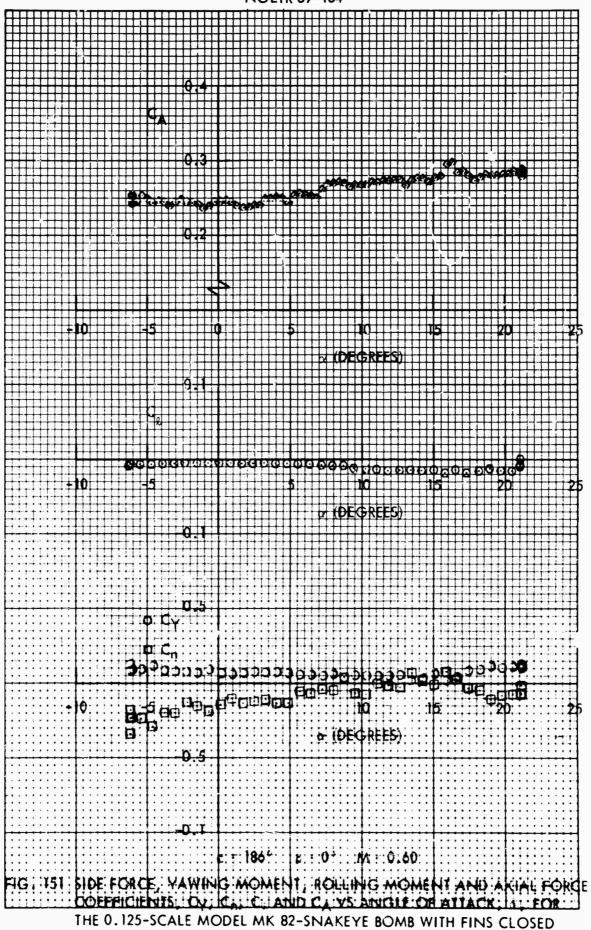


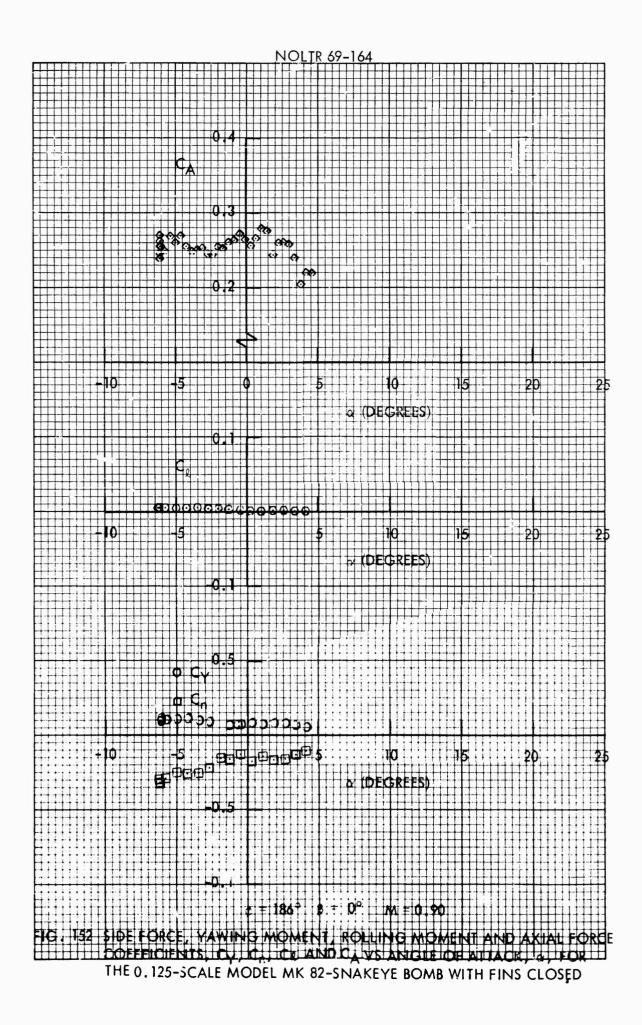
THE 0.125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

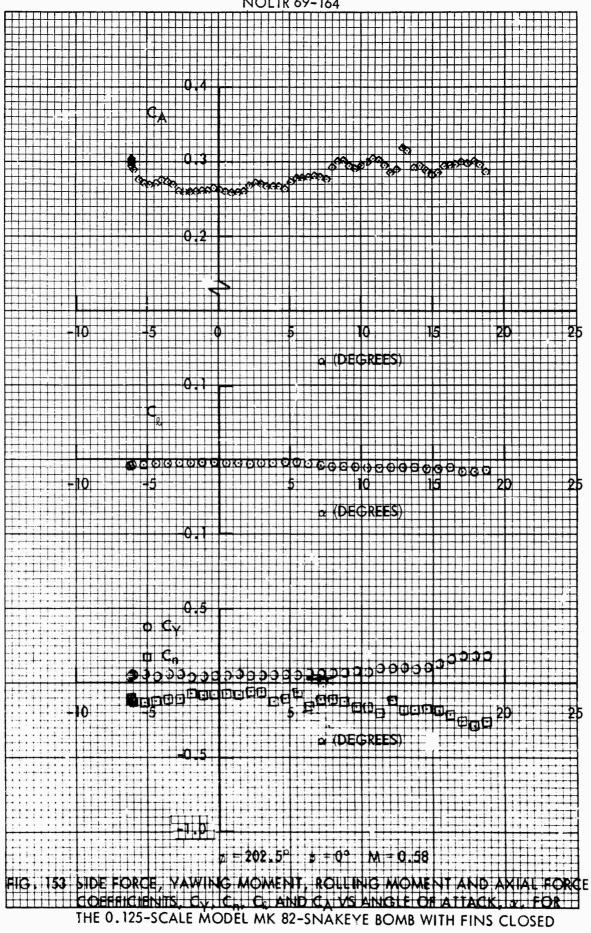


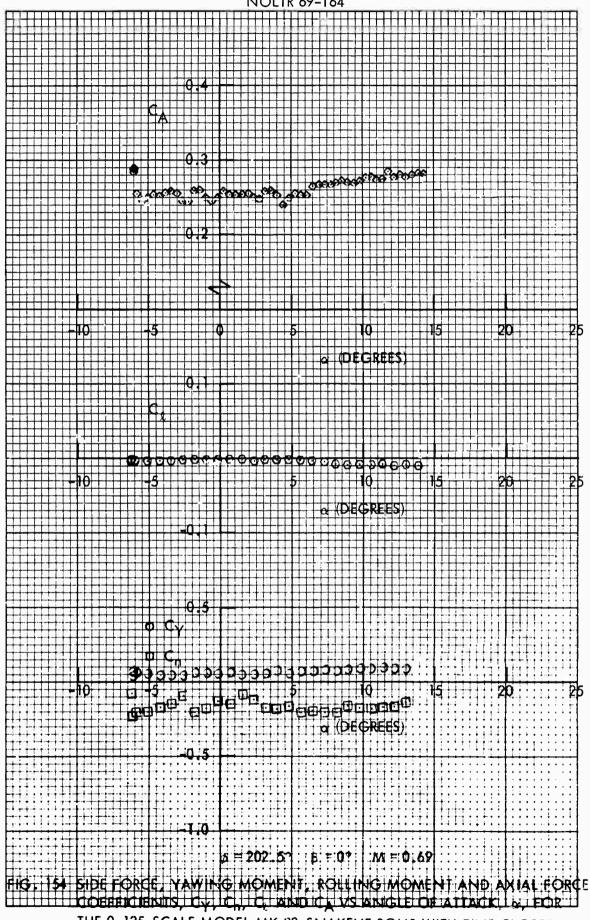




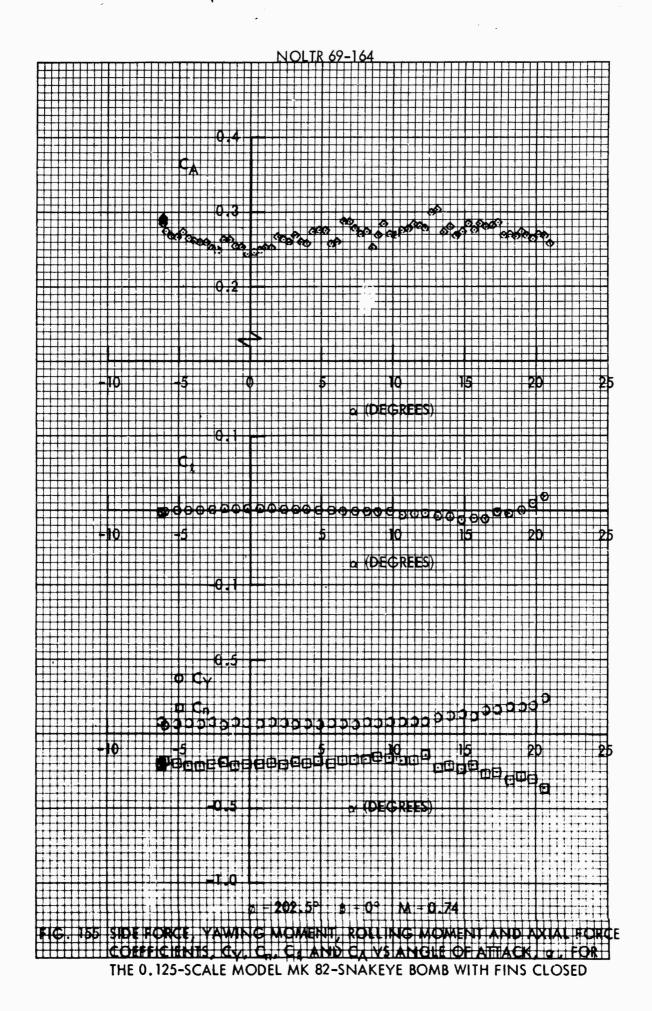


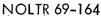


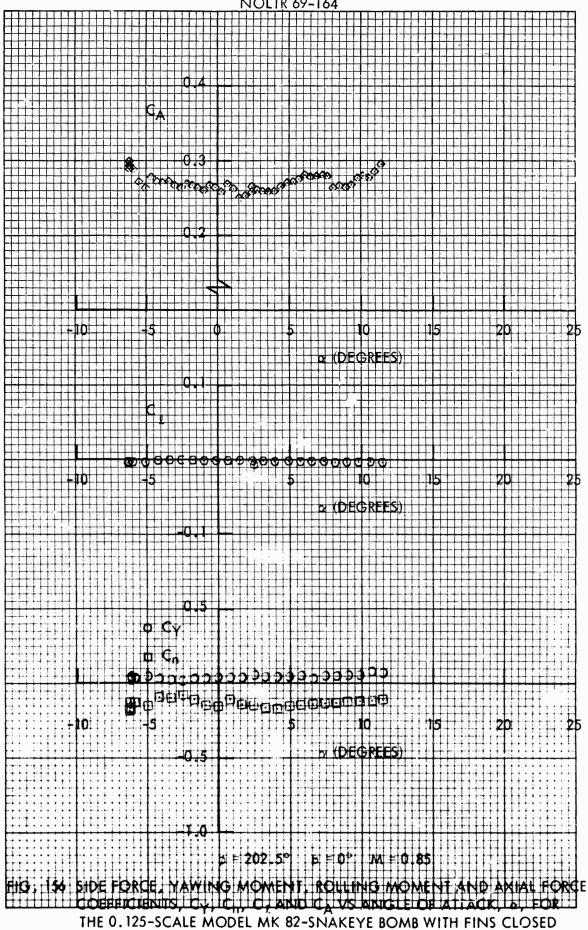


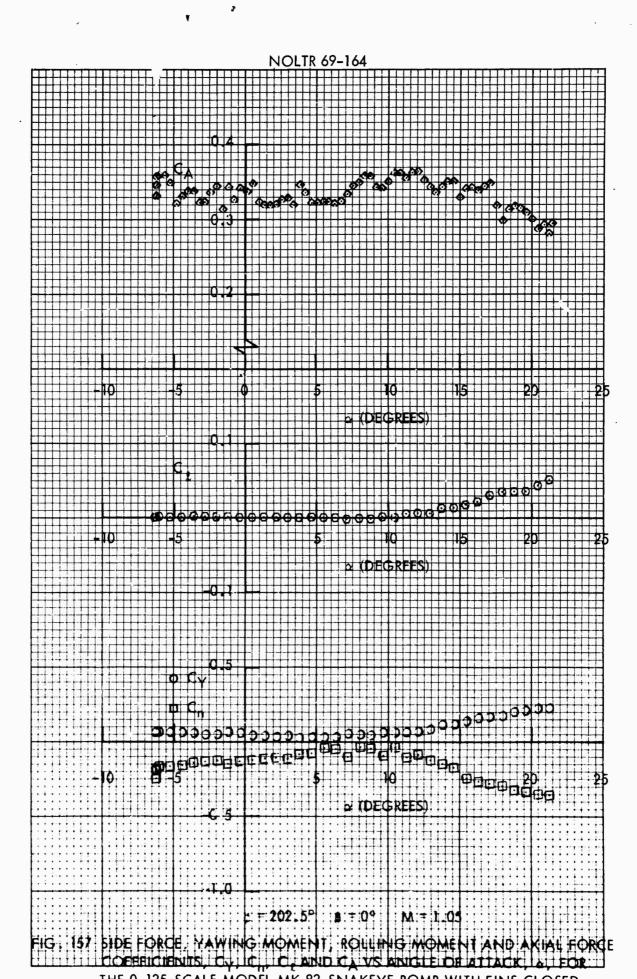


THE 0.125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

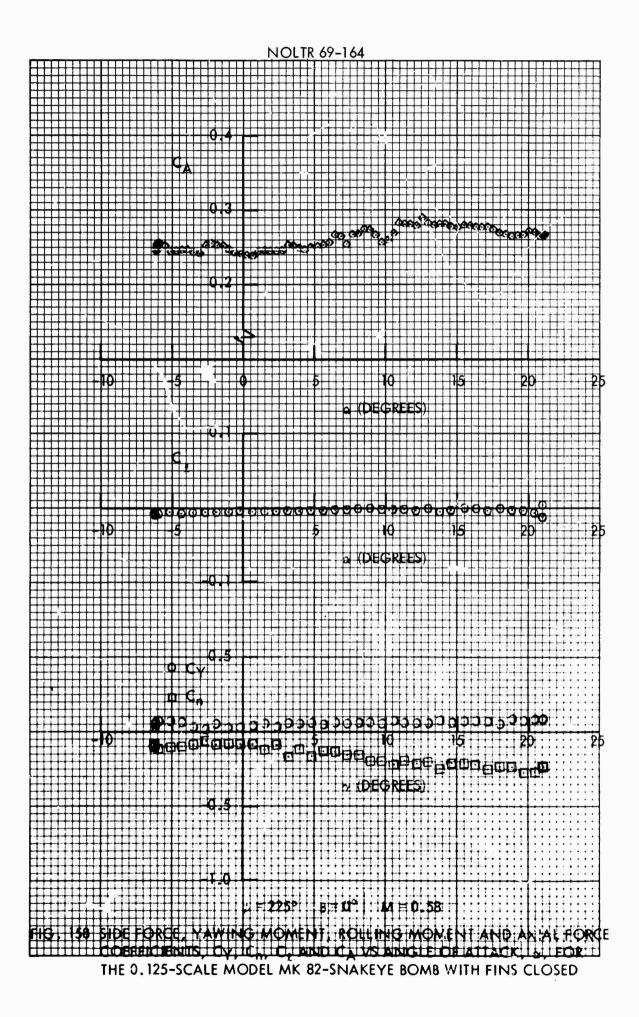




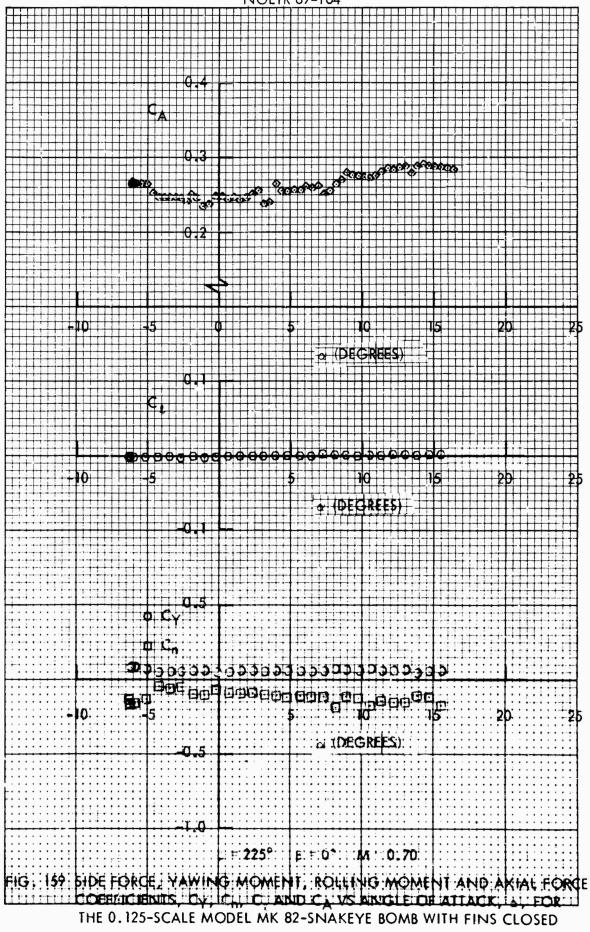


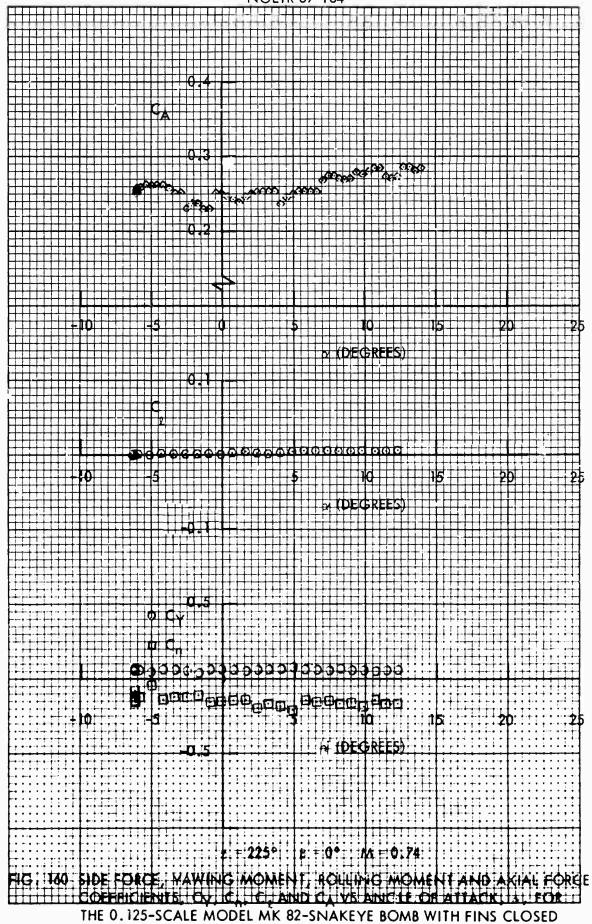


THE 0.125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

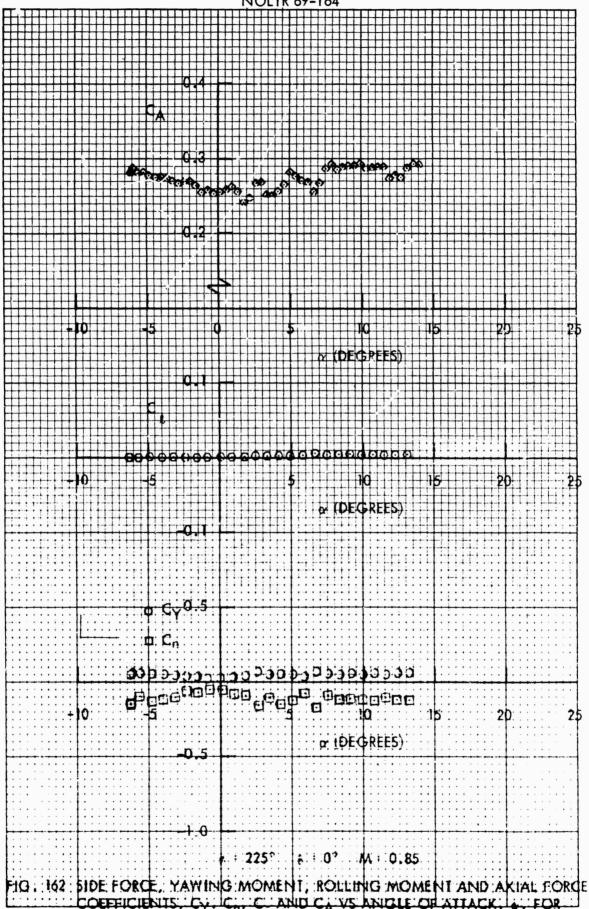




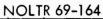


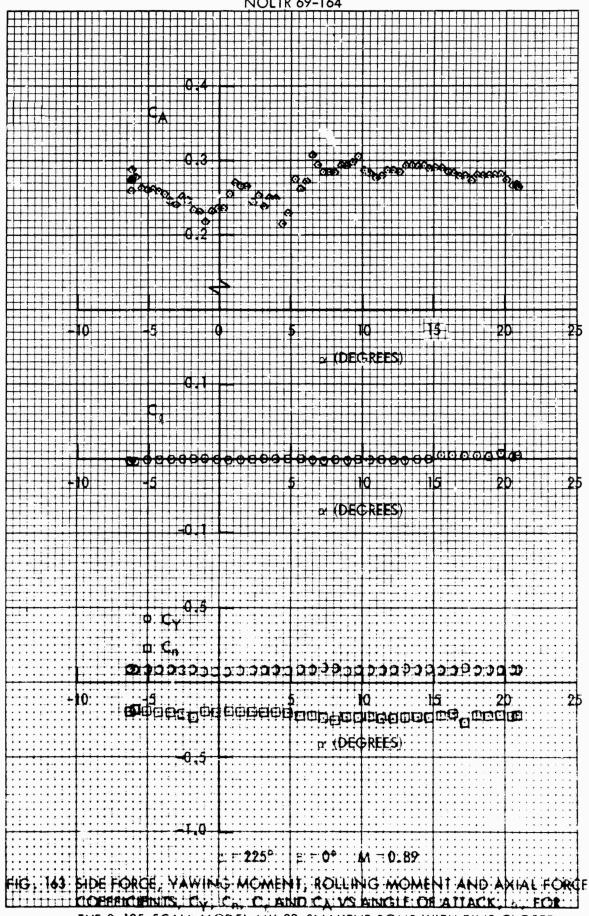




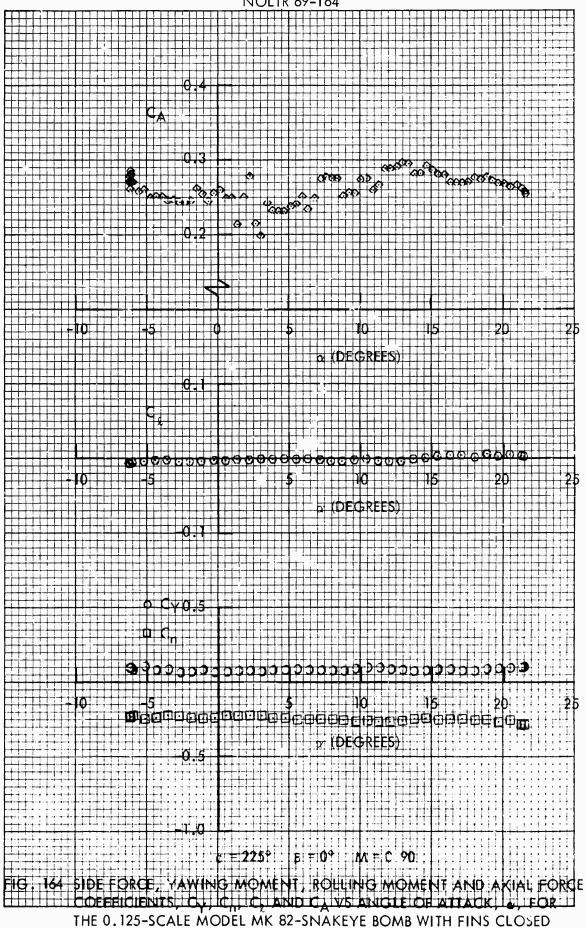


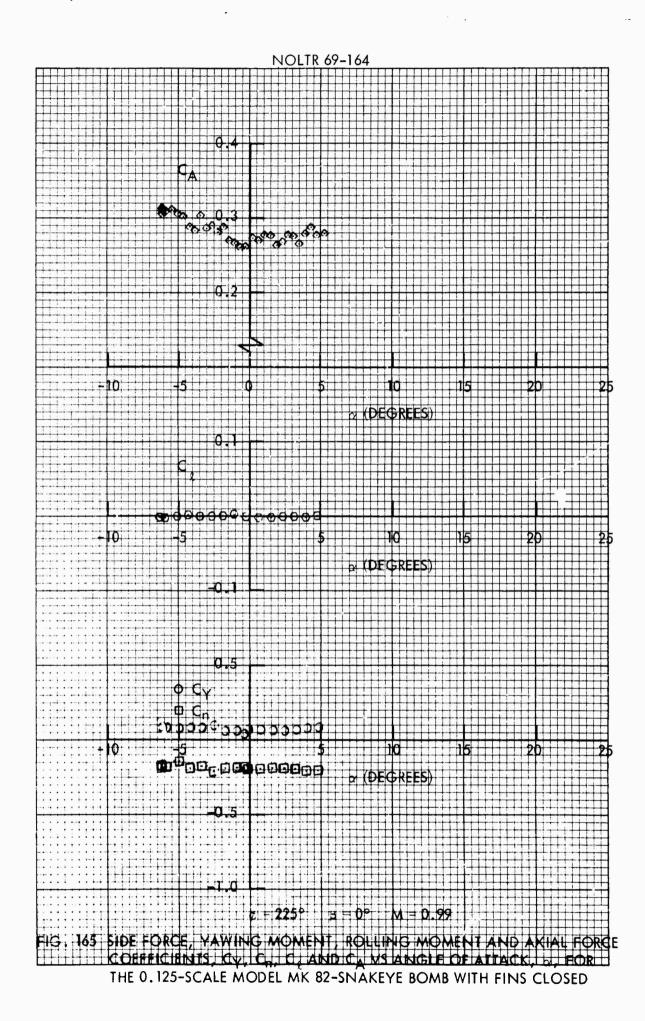
COEFFICIENTS; Cy; C;; C; AND CA:VS ANGLE OF ATTACK; L; FOR THE 0.125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED

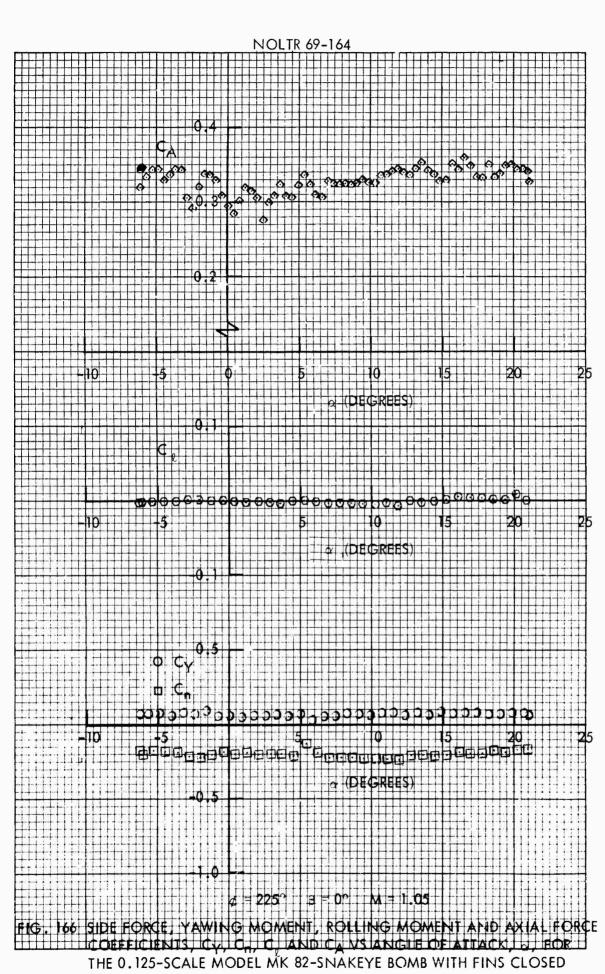


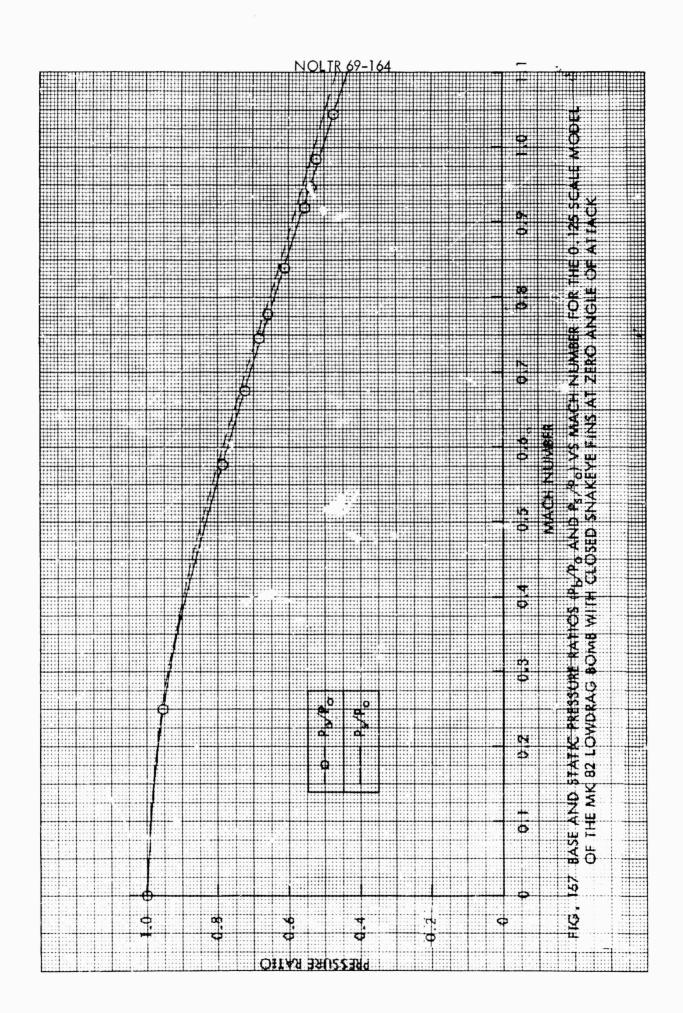


THE 0.125-SCALE MODEL MK 82-SNAKEYE BOMB WITH FINS CLOSED









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Security Classification					
DOCUMENT CONTI					
1 ORIGINATING ACTIVITY (Corporate author) U. S. Naval Ordnance Laboratory		28. REPORT SECURITY CLASSIFICATION			
White Oak, Silver Spring, Maryland		UNCLASSIFIED			
STATIC STABILITY AND AXIAL FORCE CO MODEL MARK 82 LOW DRAG BOMB WITH CL AND TRANSONIC SPEEDS	DEFFICIENTS	S FOR THE 0.125 SCALE EYE I FINS AT SUBSONIC			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)					
5. AUTHORISI (First name, middle initial, last nume)					
V. L. Schermerhorn					
6 REPORT DATE	78, TOTAL NO. O	OF PAGES 76. NO OF REFS			
17 September 1969	98. ORIGINATOR	none			
b. PROJECT NO.	NOLTR 69-164				
c NOL 795/NWL	সং. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)				
d.					
10. DISTRIBUTION STATEMENT		he consider of the II C			
Each transmittal of this document Government must have prior approva		ne agencies of the U.S.			
11 SUPPLEMENTARY NOTES	1	MILITARY ACTIVITY			
	Naval Weapons Laboratories				
	ngurgret	n, Virginia			
Static stability and axial force a function of angle of attack for Snakeye Fins in the closed position a Mach number range from 0.6 to 16 to +20 degrees; and, a roll anguithe NOL Supersonic Tunnel No. 1, us	ce coeffice the Mk 82 n. These l; an angl	cients are presented as Low Drag Bomb with data were obtained for le of attack range from from 0 to 225 degrees in			

DD FORM 1473 (F'Ass 1)

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14	LINK A		LINK B		LINK C	
KEY WORDS	ROLE	WΤ	ROLE	wr	ROLE	WΤ
force and moment coefficients						
low-drag bomb						
closed fins (unretarded mode)						
Cooper Land (united and another						
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DD FORM 1473 (BACK)
(PAGE 2)

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